TECHNICAL MANUAL

OPERATOR'S ORGANIZATIONAL, DIRECT SUPPORT, AND GENERAL SUPPORT

MAINTENANCE MANUAL
INCLUDING REPAIR PARTS AND
SPECIAL TOOLS LIST

FOR<br>ELECTROMAGNETIC INTERFERENCE/<br>FIELD INTENSITY METER<br>NM-37157 (NSN 6625-00-161-4176)

DEPARTMENTS OF THE ARMY
AND AIR FORCE
17 SEPTEMBER 1984


## ?



SAFETY STEPS TO FOLLOW IF SOMEONE IS THE VICTIM OF ELECTRICAL SHOCK


DO NOT TRY TO PULL OR GRAB THE INDIVIDUAL


IF POSSIBLE, TURN OFF THE ELECTRICAL POWER

4
IF YOU CANNOT TURN OFF THE ELECTRICAL
POWER, PULL, PUSH OR LIFT THE PERSON TO
SAFETY USING A DRY WOODEN POLE OR A DRY
ROPE OR SOME OTHER INSULATING MATERIAL
IF YOU CANNOT TURN OFF THE ELECTRICAL
POWER, PULL, PUSH OR LIFT THE PERSON TO
SAFETY USING A DRY WOODEN POLE OR A DRY
ROPE OR SOME OTHER INSULATING MATERIAL
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POWER, PULL, PUSH OR LIFT THE PERSON TO
SAFETY USING A DRY WOODEN POLE OR A DRY
ROPE OR SOME OTHER INSULATING MATERIAL

## 2

## WARNING

This instrument, while energized, contains dangerous voltages which can cause death on contact.

The NM-37/57 is designed for operation from a polarized, three-terminal power receptacle having one terminal connected to earth ground. When only a two-terminal power receptacle is available, eliminate shock hazard by using a three-prong to two-prong adapter and connect the adapter pigtail lead to the power receptacle ground.

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TECHNICAL MANUAL
NO. 11-6625-2827-14\&P
TECHNICAL ORDER
NO. 33A1-4-67-1

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TO 33A1-4-67-1
DEPARTMENTS OF THE ARMY AND
AIR FORCE
Washington, DC, 17 September 1984

OPERATOR'S, ORGANIZATIONAL, DIRECT SUPPORT
AND GENERAL SUPPORT MAINTENANCE MANUAL
INCLUDING REPAIR PARTS AND SPECIAL TOOLS LISTS
FOR
ELECTROMAGNETIC INTERFERENCE FIELD INTENSITY METER NM-37/57
(NSN 6625-00-161-4176)

## REPORTING ERRORS AND RECOMMENDING IMPROVEMENTS

You can help improve this manual. If you find any mistakes or if you know of a way to improve the procedures, please let us know. Mail your letter, DA Form 2028 (Recommended Changes to Publications and Blank Forms), or DA Form 2028-2 located in back of this manual direct to: Commander, US Army Communications-Electronics Command and Fort Monmouth, ATTN: AMSEL-ME-MP, Fort Monmouth, New Jersey 07703-5007.

For Air Force, submit AFTO Form 22 (Technical Order System Publication Improvement Report and Reply) in accordance with paragraph 6-5, Section VI, T.O. 00-5-1. Forward direct to prime ALC/MST.

In either case, a reply will be furnished direct to you.

This manual is an authentication of the manufacturer's commercial literature which, through usage, has been found to cover the data required to operate and maintain this equipment. The manual was not prepared in accordance with MIL-M-38784A; therefore, the format has not been structured to consider categories of maintenance.

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## SECTION 0

## INTRODUCTION

### 0.1. SCOPE OF MANUAL

This manual provides operation and maintenance information for the Model NM-37/57 Electromagnetic Interference/Field Intensity Meter (figure 0-1). The manual is divided into six sections containing a general description of the equipment and accessories, operating instructions and procedures, theory of operation, maintenance instructions, schematic diagrams, a repair parts list, part number, national stock number cross reference index, and a maintenance allocation chart (MAC).

### 0.2. CONSOLIDATED INDEX OF ARMY PUBLICATIONS AND BLANK FORMS

Refer to the latest issue of DA Pam 310-1 to determine whether there are new editions, changes, or additional publications pertaining to the equipment.

### 0.3. MAINTENANCE FORMS, RECORDS, AND REPORTS

a. Reports of Maintenance and Unsatisfactory Equipment. Department of the Army forms and procedures used for equipment maintenance will be those prescribed by DA Pam 738-750, The Army Maintenance Management System (TAMMS). Air Force personnel will use AFR 66-1 for maintenance reporting and TO-00-35D54 for unsatisfactory equipment reporting.
b. Report of Packaging and Handling Deficiencies. Fill out and forward SF 364 (Report of Discrepancy (ROD) as prescribed in AR 735-11-2/DLAR 4140.55/NAVMATINST 4355.73/AFR 400-54/MCO 4430.3F.
c. Discrepancy in Shipment Report (DISREP) (SF 361). Fill out and forward Discrepancy in Shipment Report (DISREP) (SF 361) as prescribed in AR 55-38/NAVSUPINST 4610.33C/AFR 75-18/MCO P4610.19D/DLAR 4500.15.

### 0.4 REPORTING EQUIPMENT IMPROVEMENT RECOMMENDATIONS (EIR)

a. Army. If your EMI FIELD INTENSITY METER-SINGER NM-37/57 needs improvement, let us know. Send us an EIR. You, the user, are the only one who can tell us what you don't like about your equipment. Let us know why you don't like the design. Put it on an SF 368 (Quality Deficiency Report). Mail it to Commander, US Army CommunicationsElectronics Command and Fort

## Monmouth, ATTN: AMSEL-ME-MP, Fort Monmouth, New Jersey 07703-5007. We'll send you a reply.

b. Air Force. Air Force personnel are encouraged to submit EIR's in accordance with AFR 900-4.

### 0.5 ADMINISTRATIVE STORAGE

Administrative Storage of equipment issued to and used by Army activities will have preventive maintenance performed in accordance with the PMCS chart before storing. When removing the equipment from administrative storage the PMCS should be performed to assure operational readiness.

Disassembly and repacking of equipment for shipment or limited storage are covered in paragraph 1.8.

### 0.6 DESTRUCTION OF ARMY ELECTRONICS MATERIEL

Destruction of Army electronics materiel to prevent enemy use shall be in accordance with TM 750-244-2.

### 0.7 EQUIPMENT DIFFERENCES DURING PRODUCTION

a. Basis and Annotation of Changes.

Components have been added and changes have been made in the equipment during production (i.e., serial number 339 and above) to improve equipment operation. These differences are shown on the equipment drawings (figure 5-1 thru 539) by a Serial Number Note on the applicable drawing and in the parts list (appendix) by asterisks keyed to a note or notes at the end of the applicable parts list assembly. Also, three figures (fig. 5-3-1, 5-12-1, and 5-27-1) have been added.
b. Maintenance Application.

During maintenance of the equipment it is important to note the serial number of the equipment being serviced. This will ensure that the correct circuitry and components are interacting during operation.

## SECTION I

## GENERAL INFORMATION

### 1.1. PURPOSE AND USE OF EQUIPMENT

The tNM-37/57 is a programmable, precision electromagnetic interference/field intensity (EMI/FI) meter for the measurement of conducted or radiated RF interference within the frequency range of 30 MHz to 1 GHz in accordance with standard military and commercial EMI test specifications. The instrument performs automatic and semiautomatic testing when supplied with appropriate command signals and provides outputs of signal amplitude and frequency that are suitable for input to a digital data processing system. Some typical applications of the NM-37/57 are:
a. Determining the presence, level, frequency, and characteristics of conducted or radiated RF signals within the frequency range of 30 MHz to 1 GHz .
b. Automatic and semiautomatic EMI testing in accordance with MIL-STD 461A and MIL-STD-826A.
c. Connected to an $\mathrm{X}-\mathrm{Y}$ plotter for spectrum signature recording.
d. Measurement of radiation from a component, system, or vehicle.
e. General laboratory applications as a tunable, programmable, two-terminal microvolntmeter.
f. RF current measurement in a conductor.
g. Antenna propagation studies, radiation pattern and field strength measurements.
h. Measuring the susceptibility of electronic equipment to an electromagnetic environment.
i. Analyzing bandpass, band rejection, and discriminating characteristics of electronic components, circuitry, and systems.
j. Determination of shielding effectiveness.

### 1.2 GENERAL DESCRIPTION

The instrument is all solid-state, rugged and portable, and operates from internal rechargeable batteries. It is an ideal unit for use in conjunction with a simple, lightweight computer and recorder to form a high-speed, high-volume mobile test station.

The instrument may be used to analyze narrowband or broadband signals in its frequency range. Average (field intensity) or direct peak detector functions may be used for measurements in addition to quasi-peak, slideback peak and BFO detection modes. AM, FM and PM signals may be detected and are available at the video output for oscilloscope display. When used in conjunction with an oscilloscope, the NM-37/57 becomes an improved spectrum analyzer with integral pre selection. Exceptional gain flatness is inherent in the design of the NM-37/57. This feature permits X-Y plotting of signal amplitude and frequency information without an extreme deviation of accurate calibration.

Electronic tuning permits remote tuning without mechanical drive. Activation of the internal electronic scan provision is by a front-panel pushbutton. Three IF bandwidths are provided, permitting quick identification of broadband or narrow-band signals:
a. The 1 MHz bandwidth provides greatest sensitivity for broadband signals and permits direct amplitude measurement in microvolts-per-megahertz.
b. The 100 kHz bandwidth can be used for broadband or narrowband signals.
c .. The 10 kHz bandwidth provides greatest sensitivity for narrowband signals and permits improved frequency resolution for closely-spaced channels. (A fine-tune control is provided for ease of tuning CW signals when this bandwidth is used. )

The frequency dial indicates operating frequency in all modes of operation: manual, automatic scan, remote and AFC. Adjustments to the fine-tune control are also indicated on the frequency dial. The primary detection circuitry of the NM37/57
uses a logarithmic amplifier which provides 60 dB of dynamic display range on the panel nieter. In conjunction with the four 20 dB RF attenuator steps (total of 80 dB attenuation) the overall measurement range is 140 dB (from one-tenth of one -nicrovolt to one volt).

## 1. 3 PROGRAMMABLE FUNCTIONS

In order to facilitate automated testing methods, the following critical control functions of the NM-37/57 are programmable by the application of voltage from a remote source:
a. Frequency band selection.
b. Bandwidth selection.
c. Frequency tuning.
d. Receiver gain (calibration).
e. Detector function selection.

### 1.4 SPECIFICATIONS

Table 1-1 contains specification data for the NM-37/57.

Table 1-1. Specifications

| Parameter | Characteristic |
| :---: | :---: |
| Frequency Range: | 30 to 1000 MHz in 8 bands. |
|  | Band 1: $\quad 30$ to 57 MHz . Band 5: 285 to 445 MHz . |
|  | Band 2: $\quad 55$ to 105 MHz . Band 6: 430 to 620 MHz . |
|  | Band 3: 101 to 192 MHz . Band 7: 600 to 825 MHz . |
|  | Band 4: 186 to 292 MHz . Band 8: 800 to 1000 MHz . |
| Receiver Type: | Superheterodyne. Single conversion on Bands 1 thru 3; dual conversion on Bands 4 thru 8. |
| Intermediate | Bands 1 thru 3: 20.5 MHz . |
| Frequencies: | Bands 4 thru 8: 160 MHz and 20.5 MHz. |
| RF Input Impedance: | 50 ohms (Type N coaxial connector). |
| RF Input VSWR: | Bands 1 thru 3: 1.25:1 typical, 1.5:1 maximum. |


| Parameter | Characteristic |
| :---: | :---: |
| Frequency Scale Accuracy: | True frequency is within $\pm 2 \%$ of indicated frequency |
| Voltage Measurement | + 2 dB for CW signals. |
| Accuracy: | +3 dB for impulse signals. |
| Gain Flatness: | $\begin{aligned} & \text { Typically }+2 \mathrm{~dB}\left(+25^{\circ} \mathrm{C}\right) \text {, maximum }+3 \mathrm{~dB} \\ & \left(-15^{\circ} \mathrm{C} \text { to }+500 \mathrm{C}\right) \text {. } \end{aligned}$ |
| Calibrator: | Internal solid-state impulse generator, fixed amplitude, 450 Hz repetition rate. |
| Voltage Measurement Range: | $140 \mathrm{~dB} ; 60 \mathrm{~dB}$ on meter scale plus $20,40,60$, and 80 dB attenuator steps. |
| Undesired Response Rejection: | Intermediate Frequency Rejection: 60dBminimum. Image Frequency Rejection: 60 dB minimum. Spurious Rejection: 60 dB minimum (except Band 1 at $2 \mathrm{X} 20.5 \mathrm{MHz} \mathrm{IF}, 40 \mathrm{~dB}$ minimum). |
| Local Oscillator Emission: | Less than 50 picowatts. |
| Shielding Effectiveness: | Typically greater than 100 dB , minimum 80 dB . |
| Automatic Frequency Control: | Typical Locking Range: <br> Greater than +100 kHz in 10 kHz bandwidth. <br> Greater than +1 MHz in 100 kHz bandwidth. <br> Greater than +2 MHz in 1 MHz bandwidth. |
| Signal Outputs (simultaneously available): | For a full scale CW signal: |
| IF ( 20.5 MHz ): | 20 mV RMS minimum across 50 ohms. BNC connector on rear panel |
| Log Video: | $300 \mathrm{mV}+10 \%$ peak across 50 ohms, DC to 500 kHz . BNC connector on rear panel. |
| Linear Video: | 100 mV minimum peak-to-peak across 50 ohms, 20 Hz to 200 kHz , for $30 \%$ amplitude modulation. BNC connector on rear panel. |
| FM Video: | $\pm 300 \mathrm{mV}$ minimum peak across 50 ohms, DC to 100 kHz , for +300 kHz deviation. BNC connector on rear panel. |
| Audio (AM or FM): | 100 mW typical, 50 mW minimum across 600 ohms, 300 to 4000 Hz , for $30 \%$ amplitude modulation. Phone jack on front panel. |
|  | 1-4 |

Table 1-1. Specifications (Continued)

| Parameter | Characteristic |
| :---: | :---: |
| LO Outputs (8) (optional): | Bands 1 thru 3: -33 dBm minimum. Bands 4 thru 8: -20 dBm minimum. |
| Data Outputs (simultaneously available): |  |
| X-Axis Output: | 0 to $1 \mathrm{~V}+5 \%$ across 1000 ohms, 0 to 2 V open circuit, for any frequency band. <br> BNC connector on rear panel. |
| Y-Axis Output: | 0 to $1 \mathrm{~V} \pm 5 \% 0$ across 1000 ohms, 0 to 2 V open circuit, for zero to full scale meter deflection. BNC connector on rear panel. |
| Frequency Readout: | 10 mV per MHz , 0.3 to 10.0 V for full frequency range. Accuracy $\pm+2 \%$. <br> From Programmer receptacle on rear panel. |
| dB Readout: | 1 mV per $\mathrm{dB},-20$ to +120 mV for full voltage measurement range. Accuracy +2 dB . From Programmer receptacle on rear panel. |
| Detector Functions: |  |
| Field Intensity (FI) (Average): | Average value of output of the 60 dB logarithmic detector. |
| Quasi-Peak: | Weighted average of output of the 60 dB logarithmic detector. Charge time is 1 millisecond; discharge time is 600 milliseconds. |
| Direct Peak: | Responds to true peak value. Calibrated in RMS of an equivalent sine wave. Selectable hold times of $0.05,0.3$, and 3 seconds. |
| Slideback Peak: | Manual slideback detector with aural null indication. |
| BFO: | Beat frequency oscillator for CW signal reception and tuning aid. |
| FM Discriminator: | $\pm 300 \mathrm{kHz}$ deviation. |
| Linear: | Video and audio outputs. |
| Selectable IF Bandwidth: | $\begin{aligned} & 10 \mathrm{kHz} \pm 10 \% \text { at }-3 \mathrm{~dB} \text {; } \\ & 100 \mathrm{kHz}+10 \% \text { at }-3 \mathrm{~dB} ; \end{aligned}$ <br> $1 \mathrm{MHz} \pm 10 \%$ at -6 dB (at low end of Band 1 the tolerance of the 1 MHz bandwidth is $+10 \%$ and $-30 \%$ ). |

Table 1-1. Specifications (Continued)

| Parameter | Characteristic |
| :---: | :---: |

Sensitivity (as a twoterminal RF voltmeter):

Narrowband, CW Signal:

Broadband, Impulse Signal:

Internal Frequency Scan:

Programmable Functions:
Frequency Band Selection:
Frequency Tuning:
Bandwidth Selection:
Detector Function Selection:

Receiver Gain (Calibrate Control):

Power Requirements:
AC Power:

To produce a 3 dB meter indication above noise:

Field Intensity function, 10 kHz bandwidth:

|  | $\underline{\mu V}$ | $\underline{\mathrm{~dB} \mu \mathrm{~V}}$ | $\underline{\mathrm{dBm}}$ |
| :--- | :--- | :--- | :--- |
| Bands 1 thru 3: | 0.14 | -17 | -124 |
| Bands 4 thru 8: | 0.316 | -10 | -117 |

Field Intensity function, 1 MHz bandwidth:

|  | $\frac{\mu \mathrm{V}}{1.4}$ | $\frac{\mathrm{~dB} \mu \mathrm{~V}}{+3}$ | $\frac{\mathrm{dBm}}{-104}$ |
| :--- | :--- | :--- | :--- |
| Bands 1 thru 3: | 3.16 | +10 | -97 |

Direct Peak function, 1 MHz bandwidth:

## $\mu \mathrm{V} / \mathrm{MHzdB} \mu \mathrm{V} / \mathrm{MHz}$

Bands 1 thru 3: $\quad 5.6+15$
Bands 4 thru 8: $\quad 10.0 \quad+20$
Electronically scans any band in one minute, providing outputs to $\mathrm{X}-\mathrm{Y}$ recorder. Pen Lift provided (isolated contact closure).

Electrical programming requirements:
-12 V, 50 mA maximum.
0 to +10 V sawtooth (input resistance of 2 kilohms).
+12 V, 14 mA maximum.
+12 V, 60 mA maximum.
+4.8 V to +7.2 V (input resistance of 50 kilohms).
$115 \pm 10 \mathrm{~V}$ or $230+20 \mathrm{~V}, 50$ to 400 Hz , approximately 30 watts.

Table 1-1. Specifications (Continued)

| Parameter | Characteristic |
| :---: | :---: |
| Battery: | Rechargeable nickle-cadmium cells provided in removeable battery pack. Eight (8) hours continuous operation. Internal charging circuits charge battery in 14 to 16 hours. Battery test indication is provided on front panel meter. <br> NOTE <br> Refer to Appendix Afor supplementary battery information. |
| Mechanical: Dimensions (including handles): | Height: 8-3/4 inches. <br> Width: 16-3/4 inches. <br> Depth: 18-1/2 inches. |
| Weight: Environmental: Temperature: | 65 pounds (including battery pack). <br> Operational -150C to $+50^{\circ \mathrm{C}}$. <br> Non-operational: $-50^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$. |
| Vibration: <br> Altitude: | Meets MIL-T-21200, Class 3 non-operating. <br> Operational to at least $15,000 \mathrm{ft}$. (mean sea level). |

### 1.5 SUPPLIED ACCESSORIES

The items listed in Table 1-2 are furnished with the NM-37/57 EMI/FI meter.

Table 1-2. Supplied Accessories

| Quantity | Description | Singer Part. No. |
| :---: | :--- | :--- |
| 1 | AC power cable, 6 ft. | $1-910166-001$ |
| 1 | Module extender cable | $2-004543-001$ |
| 1 | Calibration Chart <br> Connector (mates with PROGRAMMER input <br> receptacle) <br> Instruction manual | $1-403274-001$ |
| 1 | Rack mounting brackets | $1-910101-005$ |
| 2 | Flat-head screws, 10-32 X $1 / 2$ <br> (for rack mounting brackets) | $3-100783-234$ |
| 4 |  | $\mathbf{1 - 7}$ |

### 1.6 OPTIONAL ACCESSORIES

Accessories available for use with the NM-37/57 are listed in Table 1-3 and illustrated in Figure 1-2.

Table 1-3. Optional Accessories

| Index No. <br> (Fig. 1-2) | Description | Model No. |
| :---: | :---: | :---: |
| 1 | Meter transit case | 95207-2 |
| 2 | Biconical antenna ( 30 MHz 200 MHz ) | 94455-1 |
| 3 | Antenna mounting adapter | 91932-2 |
| 4 | Collapsible tripod | 91933-2 |
| 5 | Log spiral antenna ( 200 MHz 1 GHz ) | 93490-1 |
| 6 | Headphones | 10796 |
| 7 | RF current probe ( $1 \mathrm{MHz}-$ 1 GHz ) | 94111-1 |
| 8 | Loop antenna base | 90995-2 |
| 9 | Loop antenna | 90799-2 |
| 10 | RF probe cable | 90757-2 |
| 11 | Tripod bag | 92049-1 |
| 12 | Antenna mast | 90920-2 |
| 13 | Video output cable, X-output cable, or $Y$-output cable | 90071-1 |
| 14 | RF transmission line, 20 ft . | 90933-8 |
| 15 | Headphone extension cable, 20 ft . | 90074-1 |
| 16 | Cable bag | 91981-2 |



Figure 1-1. Optional Accessories

### 1.7. UNPACKING AND INSPECTION

If the shipping carton is damaged, ask that the carrier's agent be present when the instrument is unpacked. Inspect the equipment for damage (scratches, dents, broken knobs, etc.) If the instrument is damaged or fails to operate, notify the carrier and the nearest Singer Sales and Service Office immediately. Retain the shipping carton and padding material for the carrier's inspection.

### 1.8 STORAGE AND SHIPMENT

### 1.8.1 STORAGE

The NM-37/57 should be stored in a clean dry area in a temperature range of -500 to +750 C and a relative humidity of less than $95 \%$.

### 1.8.2. PACKAGING

The following general instructions should be used to package the NM-37/57 for shipment using commercial available materials.
a. Wrap the instrument in heavy paper or plastic. (If the instrument is being returned to Singer for repair, attach a tag indicating the type of service required, return address, model and serial number.)
b. Place the instrument in a strong shipping container (double roll carton made of 350 pound test material is adequate) and place a minimum of 1 inch of shock absorbent material around all sides of the instrument to provide a firm cushion and prevent movement within the carton. Mark the outside of the container FRAGILE to assure careful handling. Seal the shipping container securely.

## Section II

## OPERATING INSTRUCTIONS

### 2.1 GENERAL

Instructions and information for preparing the NM-37/57 for use, functional descriptions of controls and receptacles, instructions for using signal input devices available as accessories, operating instructions, and calibration instructions are presented in this section of the manual.

### 2.2 PREPARATION FOR USE

### 2.2.1 Bench Operation

The NM-37/57 is shipped ready for use as a bench-operated instrument. A folding support that is attached to the feet under the front of the instrument may be pulled down to elevate the front panel for ease of operation.

### 2.2.2 Rack Mounting

A set of adapter brackets and attaching screws are provided to permit mounting of the NM-37/57 in a standard 19-inch rack. To prepare the instrument for rack-mounting, proceed as follows:
a. Remove six screws attaching four feet and folding support to bottom of instrument. Retain screws, feet, and support for future use.
b. Attach one rack mounting bracket (Part No. 3-103317-001) to each side of instrument using two $10-32 \times 1 / 2$ screws (Part No. 1-964064-265) in each bracket.

### 2.3 OPERATING CONTROLS, INDICATORS, AND RECEPTACLES

All external operating controls, indicators, and receptacles of the NM-37/57 are located on the front panel Figure 2-1 and on the rear panel (Figure 2-2). Functional descriptions of the front panel features are given in Table 2-1, and the rear panel features in Table 2-2


Figure 2-1. Front Panel Features


Figure 2-2. Rear Panel Features

| Control, Indicator, or Receptacle | Index No. (Fig. 2-1) | Function |
| :---: | :---: | :---: |
| BANDWIDTH Switch | 1 | A three-position rotary switch that provides selection of three calibrated bandwidths of $10 \mathrm{kHz}, 100 \mathrm{kHz}$, and 1 MHz . |
| BAND Switch | 2 | An eight-position rotary switch that selects the appropriate tuner and IF circuit, for the frequency band desired. Also causes the red indicators on the selected band scale of the frequency meter to illuminate. |
| Frequency Meter | 3 | Indicates operating frequency in all modes. Eight scales are provided to cover the frequency range of 30 MHz to 1 GHz . A pair of red indicators are illuminated on the scale in use. |
| ATTENUATOR Switch | 4 | A five-position pull-turn-push switch which allows 80 dB attenuation to be inserted in 20 dB steps. |
| RF INPUT Connector | 5 | Type N coaxial RF signal input connector. |
| CONTROL MODE Switch | 6 | A three-position rotary switch which permits selection of local or remote control of band selection, frequency tuning, bandwidth selection, detector function, and receiver gain. In the SCAN position the internal frequency scanning circuits are enabled. |
| SINGLE Switch | 7 | Pushbutton switch which triggers a single 60 -second scan of the frequency band in use when CONTROL MODE switch is at SCAN position. |
| TUNE Control | 8 | Tunes the receiver in the selected band. |
| CALIBRATE Control | 9 | Adjusts IF gain of receiver. |
| FINE TUNE Control | 10 | Controls fine tuning of receiver when AFC switch is at OFF position. |

Table 2-1. Front Panel Features (Continued)

| Control, Indicator, or Receptacle | $\begin{aligned} & \text { Index No. } \\ & \text { (Fig. 2-1) } \end{aligned}$ | Function |
| :---: | :---: | :---: |
| AFC Switch | 11 | Two-position ON/OFF rotary switch which activates or disables AFC circuit. |
| FUNCTION Switch | 12 | An eight-position rotary switch that selects measurement functions as follows: |
|  |  | CALIBRATE - Disconnects RF input and energizes impulse generator to standardize receiver gain. FIELD INTENSITY - Weights signal to permit measurement of average carrier values. |
|  |  | QUASI-PEAK - Weights signal to permit measurement near the peak value of input signals. |
|  |  | PEAK - Responds to peak value of signal. Three positions provide selectable hold times of 0.05 , 0.3 , and 3.0 seconds. |
|  |  | SLIDEBACK PEAK - Applies manually controlled reverse bias to detector for slideback peak signal measurements with aural null indication. |
|  |  | BFO - Activates beat frequency oscillator to permit audible reception of CW signals. |
| SLIDEBACK PEAK Control | 13 | Adjust the voltage to the slideback peak detector for an aural null indication. |
| AUDIO Jack | 14 | Headphone output receptacle. |
| GAIN Control | 15 | Adjusts level of audio output. |
| AUDIO Switch | 16 | Two-position rotary switch selects AM or FM audio for output at AUDIO jack. |
|  |  |  |

Table 2-1. Front Panel Features (Continued)


Table 2-2. Rear Panel Features

| Control or Receptacle | $\begin{aligned} & \text { Index No. } \\ & \text { (Fia. 2-2) } \end{aligned}$ | Function |
| :---: | :---: | :---: |
| 115/230V Switch | 1 | A two-position slide switch set according to the power line voltage available. |
| $\begin{aligned} & 115 / 230 \mathrm{~V} 50-400 \mathrm{~Hz} \\ & \text { Receptacle } \end{aligned}$ | 2 | AC power input receptacle. |
| PROGRAMMER Receptacle | 3 | Remote control input receptacle for programmable functions. |
| RECORDER <br> PENLIFT Jack | 4 | Phone jack for connecting X-Y recorder pen lift control; used in conjunction with electronic scanning of frequency band. |
| IF OUTPUT Connector | 5 | Type BNC receptacle which provides 20.5 MHz IF output for application to auxiliary signal processing equipment. |
| LINEAR VIDEO Connector | 6 | Type BNC receptacle which provides detected video output of linear IF amplifie $r$. |
| FM VIDEO Connector | 7 | Type BNC receptacle which provides detected video output of FM discriminator. |
| LOG VIDEO <br> Connector | 8 | Type BNC receptacle which provides detected video output of log IF amplifier. |
| X OUTPUT <br> Connector each band. | 9 | Type BNC receptacle which provides a DC voltage representing frequency in |
| Y OUTPUT <br> Connector | 10 | Type BNC receptacle which provides a DC voltage representing signal level. |
| EXTERNAL SCAN Jack | 11 | Phone jack for frequency scan voltage input from external source when CONTROL MODE switch is at SCANposition. |
| Circuit Breakers | 12 | Protects batteries from overload. Press to reset. |

### 2.4 PROGRAMMABLE FUNCTIONS

The interconnection requirements of remote controls via the PROGRAMMER receptacle on the rear panel of the NM-37/57 are described in the following paragraphs. Functional schematic diagrams (Figures 2-3 through 2-7) that illustrate typical remote controls and a PROGRAMMER receptacle pin data list (Table 2-3) are included. Refer to the appropriate schematic diagrams in Section V for circuit details within the NM-37/5.

### 2.4.1 Frequency Band Selection

A total of eight mutually exclusive contact closures is required for remote selection of the eight frequency bands covered by the NM-37/57. Switching potential is -12 V at 50 mnA maximum current. Refer to Figure 2-3

### 2.4.2 Bandwidth Selection

Remote selection of any of three bandwidths requires three mutually exclusive contact closures. Switching potential is +12 V at 15 mA maximum current. See Figure 2-4.

### 2.4.3 Frequency Tuning

Remote tuning of the receiver is accomplished by the application of a linear ramp voltage to the tuning circuit of the NM-37/57 as shown in Figure 2-5. Scan time over the frequency band in use is determined by remote programming requirements. The remote ramp generator circuits must provide a sawtooth from 0 to +10 volts to an input resistance of approximately 2 kilohms.

### 2.4.4 Receiver Gain (Calibrate)

Remote adjustment of receiver IF gain for calibration purposes requires a potentiometer capable of supplying a continuously variable DC voltage ranging from +4.8 V to +7.2 V to an input resistance of 50 kilohms . See Figure 26.

### 2.4.5 Detector Function Selection

Remote selection of detector functions requires six mutually exclusive contact closures. Refer to Figure 2-7. Switching potential is +12 V at 60 mA maximum current.


Figure 2-3. Remote Frequency Band Selection,
Functional Schematic Diagram


Figure 2-4. Remote Bandwidth Selection, Functional Schematic Diagram


EL2RP045
Figure 2-5. Remote Frequency Tuning, Functional Schematic Diagram


Figure 2-6. Remote Receiver Gain,
Functional Schematic Diagram


Figure 2-7. Remote Function Selection, Functional Schematic Diagram

### 2.4.6 PROGRAMMER Receptacle Pin Data

Signals at the PROGRAMMER receptacle on the rear panel are listed in Table 2-3.
Table 2-3. PROGRAMMER Receptacle Pin Data


Table 2-3. PROGRAMMER Receptacle Pin Data (Continued)

| Pin | Signal Description |
| :--- | :--- |
| g | Calibrate function select input $(+12 \mathrm{~V})$ |
| h | Spare |
| i | Spar e |
| k | Calibrate control voltage input $(+4.8$ to $+7.2 \mathrm{~V})$ |
| m | Simultaneous FI output $(0$ to $+2 \mathrm{~V})($ See Note 2$)$ |
| n | Tuning voltage monitor $(0$ to $+10 \mathrm{~V})$ |
| E | X-axis output $(0$ to $+2 \mathrm{~V})$ |
| q | Spare |
| r | Spare |
| s | Spare |
| t | -12 V regulated supply output |
|  | +12 V regulated supply output |

Note 1: This pin is connected to the RC integrator in Internal Sweep A33. Connecting an external capacitor from pin R to ground will increase the duration of the internal sweep at a rate of one minute per 100 microfarads. A low-leakage tantalum capacitor should be used, positive terminal to pin R.

Note 2: When the direct peak function is selected, this output simultaneously provides an average (FI) indication of the received signal.

### 2.5 PRELIMINARY OPERATING PROCEDURES

The following procedures are to be accomplished as a preliminary to all other operating procedures.

### 2.5.1 Operation From an AC Power Source

The NM-37/57 requires AC power of 105 to 125 volts, or 210 to 250 volts, 50 to 400 Hz , approximately 30 watts.
a. Set the $115 / 230 \mathrm{~V}$ slide switch on the rear panel to the position corresponding to the AC power line voltage.

## CAUTION

The NM-37/57 is designed for operation from a polarized, threeterminal power receptacle having one terminal connected to earth ground. When only a two-terminal power receptacle is available, to eliminate shock hazard, use a three-prong to twoprong adapter and connect the adapter pigtail lead to the power receptacle ground.
b. Connect the female end of the 6 -foot power cable to the AC power receptacle on the rear panel of the instrument. Connect the male end of the cable to the AC power source.
c. Set the POWER switch on the front panel at ON AC. The frequency meter scale lights should come on.

### 2.5.2 Operation from Internal Batteries

The NM-37/57 can be operated from the internal rechargeable batteries for a period of 8 hours when the batteries are fully charged.
a. To operate from the internal batteries, set the POWER switch at ON BATT.
b. To check the condition of the internal batteries, set the POWER switch at BATT TEST. Set the BATT TEST toggle switch at + and thereafter at -.In both positions the dB meter should indicate above the RECHARGE zone of the BATTERY scale.
c. If either the + or - battery test causes the dB meter to indicate in the RECHARGE zone of the BATTERY scale, the equipment should be switched OFF, operated from an AC power source, or the batteries charged.

## NOTE

The NM-37/57 is fully capable of normal operation from an AC power source when the internal batteries are completely discharged or if the battery pack is removed from the instrument. When operated from an AC power source (POWER switch at the ON AC position), the battery trickle charger will require approximately 30 hours to recharge fully discharged batteries.

### 2.5.3_ Battery Charging

Refer to Appendix B for supplementary battery information.
To charge the fully or partially discharged internal batteries, set the POWER switch to CHARGE position. With fully discharged batteries, the charge starts slightly higher than the 10 hours charge rate current of the batteries, and the batteries are fully charged in 12 to 14 hours. At the end of the charge time, the charge current is automatically tapered down to such a level that overcharging the batteries for any length of time will not damage the battery cells. The fully charged batteries should operate the instrument continuously for eight hours without recharging. If the operating time is considerably shorter, then the battery pack is defective and should be replaced.

## NOTE

When a number of cells are operated in series, charge imbalance occurs. To reduce the possibility of one or more cells going into reverse charge towards the end of the discharge cycle, charge balancing is recommended. The recommended method of charge balancing is to deliberately charge for a longer period of time than is necessary to reach maximum ampere hour rating. In other words, overcharge the battery. Balancing is recommended once a month or every 15 charge/discharge cycles by charging for about $50 \%$ longer than the normally recommended time.

### 2.6 BASIC OPERATING TECHNIQUES

Specific operational procedures for detecting and measuring RF signals with the NM-37/57 will vary depending upon the purpose of measurement, the signal pickup device used, and the type of signal being measured. Military and commercial EMI test specifications generally include detailed requirements and instructions for performing measurements of conducted or radiated interference. However, the following basic operating procedures will generally apply for all measurement conditions:
a. Determination and adjustment of an appropriate signal pickup device.
b. Determination of the type of signal to be measured (narrowband or broadband).
c. Calibration of instrument gain.
d. Signal measurement.
e. Calculation of the measured signal level in the required units of measurement.

## NOTE

This equipment is calibrated in terms of RMS of a sine wave ( 0.707 of true peak of sine wave). Peak values are therefore in terms of RMS of a sine wave which would have the same peak amplitude as the signal that appears at the second detector input.

### 2.7 SIGNAL PICKUP DEVICES

Various accessories are available for use with the NM-37/57 as signal pickup devices. Typical among these are the three antennas and RF current probe described in the paragraphs that follow. The antennas consist of a biconical, a log spiral, and a loop antenna and are used for radiated signal measurements. The RF current probe is used for conducted signal measurements. Direct connections to a signal source may be made using an RF probe cable.

### 2.7.1_ Biconical Antenna, Model 94455-1

The biconical antenna is a broadband, balanced antenna designed to cover the frequency range of 25 to 200 MHz and is calibrated for a 50 -ohm load. The biconical antenna is specifically designed for measurement of radiated emissions and meets the requirements of MIL-STD-461A.

The biconical antenna is normally mounted on a tripod and located remotely from the NM-37/57 with the signal coupled by a 50 -ohm coaxial cable. The antenna is inherently broadband and requires no adjustment of length of the antenna elements. However, it has a radiation pattern similar to that of a tuned dipole and must be positioned broadside to the signal source for maximum response. In addition, the antenna must be rotated to obtain maximum response to signal polarization.

Each biconical antenna is furnished with an antenna correction factor (ACF) chart which provides ACF's in dB values across the full frequency range of the antenna. The ACF's are to be added to the EMI/FI meter readings when calculating signal strength in terms of dB referred to $1 \mu \mathrm{~V} /$ meter.

### 2.7.2 Conical Log Spiral Antenna, Model 93490-1

The conical log spiral antenna is a broadband antenna operating over the frequency range of 200 MHz to 1 GHz . The log spiral antenna has a nominal 50 -ohm impedance and meets the requirements of MIL-STD-461A for EMI testing.

The log spiral antenna is circularly polarized, assuring equal response to signals radiated in either the horizontal or vertical plane. The antenna has a high front to-back ratio with excellent back lobe suppression. It is normally mounted on a standard Singer tripod and connects to the NM- $37 / 57$ with a 50 -ohm coaxial cable. A calibration chart providing ACF's in dB values over the operating frequency range is provided with the antenna.

### 2.7.3 Loop Antenna, Model 90799-2

The loop antenna is used primarily in localizing electromagnetic leakage and may be used over the full frequency range of the NM-37/57. Its main advantage is that it can be used in areas where limited accessibility prevents the use of other signal pickup devices. Since the loop antenna housing is insulated, it may be used as a hand-held probe in close proximity to the signal source. Tripod mounting is generally used for determining the direction of a distant signal source. The maximum signal intensity pickup for vertically polarized signals is obtained when the plane of the loop is in line with the signal source. The antenna is coupled to the NM-37/57 by a 50 -ohm coaxial cable.

Calibration figures are not usually given for the loop antenna because it is intended for relative indications, rather than actual signal measurement.

### 2.7.4 RF Current Probe, Model 94111-1

The RF current probe is a clamp-on type of RF current transformer useable over the full frequency range of the NM-37/57. The probe may be clamped around a conductor (or group of conductors) having a maximum diameter of $1-1 / 4$ inches. The probe signal is coupled to the EMI/FI meter by a 50 -ohm coaxial cable.

The total current (AC or DC) in the circuit under investigation must not exceed 350 amperes, otherwise core saturation in the probe negates the calibration. Calibration curves of transfer impedance over the frequency range and full instructions for use are provided with each RF current probe.

### 2.7.5 RF Probe Cable, Model 90757-2

The RF probe cable is an adapter cable for use in making direct connections to a signal source. Two alligator clips are provided for attachment.

## CAUTION

Do not connect the RF INPUT receptacle of the NM-37/57 to signal sources exceeding the limits specified in Table 2-4

### 2.8 MAXIMUM SAFE INPUT LEVELS

To avoid possible damage to the input circuits of the NM-37/57, the input signal level measured at the RF INPUT receptacle must not exceed the limits set forth in Table 2-4.

Table 2-4. Maximum Safe Input Levels

| Signal Type | ATTENUATOR <br> Switch Position | Limit at RF INPUT <br> Receptacle |
| :--- | :--- | :--- |
| DC or Peak | Any $\pm 400 \mathrm{~V}$ |  |
| AC (to 400 Hz ) | Any | 230 V RMS |
| Impulsive | $+20,+40,+60 \mathrm{~dB}$ | $1 \mathrm{~V} / \mathrm{MHz}(+120 \mathrm{~dB} \mu \mathrm{~V} / \mathrm{MHz})$ |
| Impulsive | $-20,0 \mathrm{~dB}$ | $0.1 \mathrm{~V} / \mathrm{MHz}(+100 \mathrm{~dB} \mu \mathrm{~V} / \mathrm{MHz})$ |
| CW | $+20,+40,+60 \mathrm{~dB}$ | $0.5 \mathrm{watt}(+27 \mathrm{dBm})$ |
| CW | $-20,0 \mathrm{~dB}$ | $0.02 \mathrm{watt}(+13 \mathrm{dBm})$ |

### 2.9 GAIN CALIBRATION

The NM-37/57 is calibrated (gain standardized) at the desired measurement frequency as follows:
a. Set the FUNCTION switch to CALIBRATE and the CONTROL MODE switch to LOCAL.

## NOTE

When the FUNCTION switch is at the CALIBRATE position, the ATTENUATOR switch and the BANDWIDTH switch are automatically overridden and may be left in any position.
b. Obtain the proper calibration figure for the specific frequency in use from the calibration chart (Figure 2-8) for the NM-37/57.

## NOTE

The following nominal calibration figures are within $\pm 1 \mathrm{~dB}$ of the calibration chart values:
Bands 1 thru 4: 30 dB
Bands 5 and 6: 29 dB
Bands 7 and 8: 28 dB
c. Adjust the CALIBRATE control so the dB meter indicates the correct calibration figure on the dB referred to 1 $\mu \mathrm{V}$ scale.
d. Return the FUNCTION switch to its original position.

### 2.10 NARROWBAND SIGNAL MEASUREMENTS

A narrowband (NB) signal is defined as a signal having a spectral power distribution that is narrow compared to the 6 dB bandwidth of the receiver. The following signals are classified as NB:
a. Continuous wave (CW) or unmodulated carrier.

## NOTE

For unmodulated RF carriers the FIELD INTENSITY (FI), QUASI-PEAK (QP), DIRECT PEAK (DP), and SLIDEBACK PEAK (SP) detector functions will provide identical dB meter readings.

## SINGER <br> INSTRUMENTATION

The Singer Company, Los Angetes Operation
211 South La Clenmga eiva., Los Angeles, Ca. 90016

EMI/FIELD INTENSITY METER MODEL NM-37/57

SERIAL NO. $\qquad$

## CALIBRATING ENGINEER:

$\qquad$ DATE $\qquad$


Figure 2-8. Calibration Chart
2-18
b. Amplitude modulated (AM) or single sideband (SSB) modulated carrier.
c. Frequency modulated (FM) carrier.

## NOTE

Theoretically, an FM signal produces an infinite number of sidebands and would not qualify as an NB signal. The bandwidth of the significant sidebands, however, is approximately $2\left(\Delta f+f_{m}\right)$, where $\Delta f=$ peak frequency deviation and $\mathrm{fm}=$ modulation frequency. If $2\left(\Delta f+f_{m}\right)$ is less than the 6 dB bandwidth of the receiver in use, for measurement purposes the FM signal may be considered as NB.

### 2.10.1 Selection of Bandwidth

In the examples for narrowband signal measurement outlined in the following paragraphs, a 0.1 MHz bandwidth is recommended for ease of tuning. However, any of the three bandwidths may be used for narrowband signal measurement at the discretion of the operator. Use of a narrower bandwidth provides greater CW signal sensitivity. For example, using the 10 kHz bandwidth, the NM-37/57 CW signal sensitivity is approximately 10 dB better than with the 0.1 MHz bandwidth, and approximately 20 dB better than with the 1 MHz bandwidth. When using the 10 kHz bandwidth, use of AFC is recommended for tuning a narrowband signal for maximum meter deflection.

### 2.10.2 Field Intensity (Average Value) Measurements

Conducted or radiated NB signals may be measured in terms of the RMS value of the average carrier levels. Perform the measurements in the following steps:
a. Using the proper signal pickup device, connect the signal to be measured to the RF INPUT receptacle of the equipment.
b. Calibrate the instrument as described in Paragraph 2.9.
c. Set the FUNCTION switch to FIELD INTENSITY, the BANDWIDTH switch to 0.1 MHz , and the AFC switch to the OFF position.
d. Tune the receiver for maximum response to the signal indicated by the panel meter and adjust the ATTENUATOR as necessary to maintain on- scale meter deflection. Rotate the TUNE control back and forth and also
use FINE TUNE to maximize the meter indication. Readjust the ATTENUATOR if necessary to keep meter indication in upper portion of the scale. Switch AFC to ON, if desired, to lock the instrument to the signal received.
e. Note the dB meter indication on the scale of the units of measurement desired (microvolts, dB referred to 1 F V , or dBm).
f. Multiply the meter indication noted in Step e in microvolts by the ATTENUATOR factor (X 0.1 to X 1000 ) for a measurement in terms of microvolts across 50 ohms. Add the meter indication in $d B$ to the ATTENUATOR setting in $\mathrm{dB}(-20$ to $+60 \mathrm{~dB})$ to obtain the input signal level in terms of dB referred to 1 I V across 50 ohms. Subtract the meter indication in dBm from the ATTENUATOR setting in dB to obtain the input signal level in terms of dB referred to one milliwatt.
g. Note the signal frequency on the dial scale of the band in use.
h. Refer to Paragraph 2.13for calculation of signal levels.

### 2.10.3 Quasi-Peak Measurements

Conducted or radiated NB signals having a relatively fast repetition frequency may be measured in terms of weighted RMS values in the following steps.
a. Perform steps $a$ and $b$ of Paragraph 2.10.2
b. Set the FUNCTION switch to QUASI-PEAK, the BANDWIDTH switch to 0.1 MHz , and the AFC switch to the OFF position.
c. Perform steps d through h o Paragraph 2.10.2

### 2.10.4 Direct Peak Measurements

Conducted or radiated NB signals may be measured in RMS values in the following steps.

## NOTE

The DP function is the best detector to use in the search of the presence of signals because of its extremely fast response time. In the absence of signals the dB meter will smoothly fluctuate with the rotation of the TUNE control. Interception of a signal, however, will cause the dB meter to rise sharply.
a. Perform steps $a$ and $b$ or Paragraph 2.10.2
b. Set the FUNCTION switch to PEAK/0.05 SEC HOLD, the BANDWIDTH switch to 0.1 MHz , and the AFC switch to the OFF position.
c. Perform steps d through h o Paragraph 2.10.2

### 2.10.5 Slideback Peak Measurements

Conducted or radiated NB signals may be measured in RMS values using an aural null indication in the following steps:
a. Perform steps a through do Paragraph 2.10.2
b. Set the FUNCTION switch to SLIDEBACK PEAK and rotate the SLIDEBACK PEAK control fully counterclockwise.
c. Connect a set of headphones to the AUDIO jack. Set the AUDIO switch to AM, and adjust the AUDIO GAIN control to a convenient sound level.
d. Rotate the SLIDEBACK PEAK control slowly clockwise until the signal in the headphones is cut off. Note the dB meter indication at this threshold level.
e. Perform steps $f$ through h of Paragraph 2.10.2

### 2.11 BROADBAND SIGNAL MEASUREMENTS

Broadband signals are defined as those having a spectral power distribution that is broad compared to the impulse bandwidth of the receiver. Broadband interference can be considered as being composed of short pulses, the pulse repetition frequency determining the character of the interference.

If the pulses are clearly separated, the interference is termed impulsive. Such interference is generated by motor brush sparking and by combustion engine ignition circuits. If the pulses are not clearly distinguishable and overlap, then the interference is termed random. A good example of this is thermal noise. Other signals, not always broadband, have been assigned this classification for measurement purposes. These are pulse modulated CW signals. The spectrum of a pulse modulated carrier consists of lines spaced at intervals of the repetition frequency. If the impulse bandwidth of the receiver is much wider than the pulse repetition frequency then many spectral lines fall in the receiver passband and the signal is broadband related to the receiver.

Following is a list of signals, classified as Broadband:
a. Pulse modulated CW.
b. Random noise.
c. Impulsive noise from motor brushes.
d. Impulsive noise from combustion engine ignition circuits.
e. Corona discharge.

### 2.11.1 Selection of Bandwidth

In the examples for broadband signal measurement outlined in the following paragraphs, use of the 1 MHz bandwidth is recommended to permit the measurement of signal strength directly in units of microvolts-per- $\mathrm{MHz}(\mu \mathrm{V} / \mathrm{MHz}$ ), or in units of dB referred to $1 \mu \mathrm{~V} / \mathrm{MHz}(\mathrm{dB} \mu \mathrm{V} / \mathrm{MHz})$. However, any of the three bandwidths may be used for broadband signal measurement at the discretion of the operator.

## NOTE

Use of the 10 kHz bandwidth is not recommended for the measurement of broadband signals. If its use is required for special measurements, extreme care must be exercised to prevent overload of the receiver.

Use of a narrower bandwidth reduces the broadband signal sensitivity. For example, using the 0.1 MHz bandwidth, the broadband signal sensitivity of the NM-37/57 is approximately 10 dB less than with the 1 MHz bandwidth, and approximately 20 dB less when using the 10 kHz bandwidth.

### 2.11.2 Direct Peak Measurements

Measure the peak value of conducted or radiated BB signals in terms of RMS in the following steps:
a. Using the proper signal input device, connect the signal to be measured to the RF INPUT receptacle of the equipment.
b. Calibrate the instrument as described in paragraph 2.9.
c. Set the FUNCTION switch to PEAK/0.3 SEC HOLD, the BANDWIDTH switch to 1.0 MHz , and the AFC switch to the OFF position.
d. Tune the receiver to the carrier frequency of a pulse modulated CW signal, indicated by maximum deflection of the dB meter. Adjust the ATTENUATOR for a reading in the upper portion of the scale. Precise tuning is not possible for random or impulsive signals, but the interference level can be measured at any frequency within the spectrum range of the signal.
e. Multiply the meter indication in microvolts by the ATTENUATOR factor ( X 0.1 to $>1000$ ) to obtain the signal level in microvolts per $\mathrm{MHz}(\mu \mathrm{V} / \mathrm{MHz})$. Add the meter indication in dB to the ATTENUATOR setting in dB to obtain the signal level in dB referred to $1 \mu \mathrm{~V} / \mathrm{MHz}(\mathrm{dB} \mu \mathrm{V} / \mathrm{MHz})$.

## NOTE

If the 0.1 MHz bandwidth is used, multiply the $\mu \mathrm{V} / \mathrm{MHz}$ value obtained in step e by 10 , or add 20 dB to the $\mathrm{dB} \mu \mathrm{V} / \mathrm{MHz}$ value. If the 10 kHz bandwidth is used, multiply the $\mu \mathrm{V} / \mathrm{MHz}$ value from step e by 100 , or add 40 dB to the $\mathrm{dB} \mu \mathrm{V} / \mathrm{MHz}$ figure.
f. Note the signal frequency on the dial of the band in use.
g. Refer to paragraph 2.13for calculation of signal levels.

### 2.11.3 Quasi -Peak Measurements

Measure the weighted value of conducted or radiated BB signals in terms of RMS as follows:
a. Perform steps $a$ and $b$ of Paragraph 2.11.2.
b. Set the FUNCTION switch to QUASI-PEAK, the BANDWIDTH switch to 1.0 MHz , and the AFC switch to OFF.
c. Perform steps $d$ through $g$ of Paragraph 2.11.2.

### 2.11.4 Slideback Peak Measurements

Measure the peak value of conducted or radiated BB signals in terms of RMS using an aural null indication as follows:
a. Perform steps a through o o Paragraph 2.11.2
b. Set the FUNCTION switch to SLIDEBACK PEAK and rotate the SLIDEBACK control fully counterclockwise.
c. Connect a set of headphones to the AUDIO jack. Set the AUDIO switch to AM, and adjust the AUDIO GAIN control to desired sound level.
d. Rotate the SLIDEBACK PEAK control slowly clockwise until the signal in the headphones is cut off. Note the dB meter indication at this threshold level.
e. Perform steps e through g of Paragraph 2.11.2

### 2.12 SIGNAL TYPE DETERMINATION

To determine if the signal is narrowband or random noise or impulse interference, change the BANDWIDTH switch from 1.0 MHz to 0.1 MHz . If the signal is narrowband the meter deflection remains unchanged when the receiver is accurately tuned to the signal frequency. If the signal is random noise the meter deflection will decrease by approximately 10 dB . If the signal is random but not "white" noise, the signal decrease will be somewhat less than 10 dB . If the signal is impulsive the meter deflection will decrease by approximately 20 dB .

A signal type of special interest is pulsed CW. Although classified as a broadband signal in Military interference specifications, a pulsed CW signal has some characteristics that resemble narrowband signals. For example, a CW pulse may be thought of as having a distinct carrier frequency much as an AM signal has. The spectral power distribution of a carrier modulated with a rectangular pulse in principle extends from the carrier frequency to infinity and to zero. The frequencies of the components are given by $f=f_{c}+n f_{r}$, where $f_{c}=$ carrier frequency, $f_{r}=$ pulse repetition frequency and $n=$ $\sin 2 \pi \mathrm{fT}$
$0,1,2,3 \ldots$. The relative amplitude of the components is given by $2 \pi f \mathrm{~T}$ where $\mathrm{T}=$ pulse width.
Since the detector of the usual receiver ignores phase information, the actual spectrum information available will show the absolute amplitudes of the various components. A CW pulse train will have a wide spectral distribution with the first zero $\underline{l} \frac{1}{T}$
at $\overline{\mathrm{T}}$ on each side of the carrier frequency and zero recurring at $\overline{\mathrm{T}}$ intervals as far on each side of the carrier as the power is detectable. Actual pulses are never rectangular and the spectral distribution is somewhat different than the ideal case, the exact spectral envelope being determined by the nature of the pulse shape.

An oscilloscope can also be used to determine if the signal is random or impulsive by connecting the LINEAR VIDEO output to the oscilloscope. In the case of random noise, "grass" will be observed on the oscilloscope. In the case of an impulsive signal, individual pulses will be seen on the oscilloscope.

The audio output available in the headphones helps also to determine the nature of the interference. Random noise yields a hissing sound, and impulsive interference results in a popping sound.

### 2.13 SIGNAL LEVEL CALCULATIONS

Typical methods of calculating signal levels of radiated and conducted RF interference in various units of measurement are described in the following paragraphs.

## NOTE

If a coaxial cable of such length that insertion losses are significant is used to connect a signal pickup device to the NM-37/57 during measurements, the loss factor of the cable should be determined at the test frequency and included in the following calculations.

### 2.13.1 Calculation of Conducted NB Interference (50-Ohm Direct Connection)

When the NM-37/57 is used as a two-terminal RF microvoltmeter and connected across a 50 -ohm signal source, the measurement procedures given in Paragraphs 2.10.2 through 2.10 .5 yield signal levels in microvolts or in dB referred to 1 $\mu \mathrm{V}$ and no further calculations are necessary.

### 2.13.2 Calculation of Radiated NB Interference

To obtain the RF field strength in dB referred to one microvolt per meter ( $\mu \mathrm{V} / \mathrm{m}$ ), the antenna correction factor (ACF) in dB for the particular antenna used in making the measurement must be added to the input signal level in dB obtained in Paragraphs 2.10.2 through 2.10.5.

Perform the calculation as follows:
a. Determine the RF signal input level in dB referred to $1 \mu \mathrm{~V}$ as described in Paragraphs 2.10.2 through 2.10.5.
b. Determine the ACF in dB from the calibration chart for the antenna used at the test frequency.
c. Add the results of steps $a$ and $b$ to obtain the RF field strength of the radiated NB interference in $d B$ referred to $1 \mu \mathrm{~V} / \mathrm{m}$.
d. To convert the signal level in dB referred to $1 \mathrm{FV} / \mathrm{m}$ into microvolts or millivolts per meter, refer to Table 2-5.

### 2.13.3 Calculation of Conducted NB Interference Measured with RF Current Probe

Signal levels of conducted NB interference can be computed in terms of dB referred to one microampere ( $\mu \mathrm{A}$ ) when the RF current probe is employed as a signal pickup device. The transfer impedance in dB above or below one ohm must be subtracted from the input signal level in dB obtained in Paragraphs 2.10.2 through2.10.5.

Perform the calculation as follows:
a. Determine the RF signal input level in dB referred to $1 \mu \mathrm{~V}$ as described in Paragraphs 2.10.2 through 2.10.5.
b. Determine the transfer impedance of the current probe in dB at the test frequency from the chart furnished with the current probe.
c. Subtract the transfer impedance figure obtained in step b. from the measured signal level in dB determined in step a. to obtain the value of the conducted NB interference in terms of dB referred to $1 \mu \mathrm{~A}$ in the test sample conductor.

## NOTE

The transfer impedance in dB may have a positive or negative sign, depending on being above (positive) or below (negative) the one ohm reference. Observe the sign when subtracting in step c.
d. To convert the signal level in dB referred to 1 A into microamperes or milliamperes, refer to Table 2-5 and substitute "ampere" for "volt" in the units given in the table headings.

### 2.13.4 Calculation of Conducted BB Interference (50-Ohm Direct Connection)

When the NM-37/57 is used as a two-terminal RF microvoltmeter and connected across a $50-\mathrm{ohm}$ signal source, the procedures given in Paragraphs 2.11 .2 through 2.11.4 provide signal levels in $\mu \mathrm{V} / \mathrm{MHz}$ or in dB referred to $1 \mu \mathrm{~V} / \mathrm{MHz}$ and no further calculations are necessary.

Table 2-5. Conversion of Units

| dB Referred to $1 \mu \mathrm{~V}$ | $\mu \mathrm{~V}$ |
| :---: | :---: |
| -20 | 0.100 |
| -19 | 0.112 |
| -18 | 0.126 |
| -17 | 0.141 |
| -16 | 0.159 |
| -15 | 0.178 |
| -14 | 0.200 |
| -13 | 0.224 |
| -12 | 0.251 |
| -11 | 0.382 |
| -10 | 0.355 |
| -9 | 0.398 |
| -8 | 0.447 |
| -7 |  |
| -6 | 0.562 |
|  | 0.631 |
| -5 | 0.708 |
| -4 | 0.894 |
| -3 |  |
| -2 | 1.00 |
| -1 | 1.12 |
|  | 1.26 |
| 0 | 1.41 |
| 1 | 1.59 |
| 2 | 1.78 |
| 3 |  |
| 4 | 2.00 |
| 5 | 2.24 |
| 6 | 2.51 |
| 7 | 2.82 |
| 8 | 3.16 |
| 9 | 3.55 |
| 10 | 3.98 |
|  | 5.47 |
| 11 | 5.62 |
| 13 |  |
| 14 |  |
| 15 |  |
|  |  |
|  |  |
|  |  |
|  |  |


| dB Referred to $1 \mu \mathrm{~V}$ | $\mu \mathrm{~V}$ |
| :---: | :---: |
| 16 | 6.31 |
| 17 | 7.08 |
| 18 | 7.94 |
| 19 | 8.91 |
| 20 | 10.00 |
| 21 | 11.20 |
| 22 | 12.60 |
| 23 | 14.30 |
| 24 | 15.90 |
| 25 | 17.80 |
|  |  |
| 26 | 20.00 |
| 27 | 22.40 |
| 28 | 25.10 |
| 29 | 38.20 |
| 30 | 31.60 |
| 31 | 35.50 |
| 32 | 39.80 |
| 33 | 44.70 |
| 34 | 50.10 |
| 35 | 56.20 |
| 36 | 63.10 |
| 37 | 70.80 |
| 38 | 79.40 |
| 39 | 89.10 |
| 40 | 100.00 |
|  |  |
| 46 | mV |
| 47 | 0.112 |
| 48 | 0.126 |
| 43 | 0.141 |
| 43 | 0.159 |
|  | 0.200 |
| 43 | 0.251 |
|  |  |

Table 2-5. Conversion of Units (Continued)

| dB Referred to $1 \mu \mathrm{~V}$ | mV |
| :---: | :---: |
|  |  |
| 49 | 0.282 |
| 50 | 0.316 |
|  |  |
| 51 | 0.355 |
| 52 | 0.398 |
| 53 | 0.447 |
| 54 | 0.501 |
| 55 | 0.562 |
|  | 0.631 |
| 56 | 0.708 |
| 57 | 0.794 |
| 58 | 0.891 |
| 59 | 1.00 |
| 60 | 1.12 |
|  | 1.26 |
| 61 | 1.41 |
| 62 | 1.59 |
| 63 | 1.78 |
| 64 | 2.00 |
| 65 | 2.24 |
|  | 26 |
| 67 | 2.51 |
| 68 | 3.16 |
| 69 | 3.55 |
| 70 | 3.98 |
| 71 | 4.47 |
| 72 | 5.01 |
| 73 | 5.82 |
| 74 | 5.82 |
| 75 | 6.31 |
| 75 | 7.08 |
| 76 | 8.94 |
| 77 | 10.00 |
| 78 | 11.20 |
| 80 | 12.60 |
|  | 15.10 |
| 82 |  |
| 83 |  |
| 84 |  |
|  |  |


| dB Referred to $1 \mu \mathrm{~V}$ | mV |
| :---: | :---: |
| 85 | 17.80 |
| 86 | 20.00 |
| 87 | 22.40 |
| 88 | 25.10 |
| 89 | 28.20 |
| 90 | 31.60 |
|  |  |
| 91 | 35.50 |
| 92 | 39.80 |
| 93 | 44.70 |
| 94 | 50.10 |
| 95 | 56.20 |
|  |  |
| 96 | 63.10 |
| 97 | 70.80 |
| 98 | 79.80 |
| 99 | 89.10 |
| 100 | 100.00 |
| dB Referred to $1 \mu \mathrm{~V}$ | Volts |
| 101 | 0.112 |
| 102 | 0.126 |
| 103 | 0.141 |
| 104 | 0.159 |
| 105 | 0.178 |
| 106 | 0.200 |
| 107 | 0.224 |
| 108 | 0.251 |
| 109 | 0.282 |
| 109 | 0.282 |
| 110 | 0.316 |
| 111 |  |
| 112 | 0.355 |
| 113 | 0.398 |
| 114 | 0.447 |
| 115 | 0.501 |
| 116 | 0.562 |
| 117 | 0.631 |
| 118 | 0.708 |
| 119 | 0.994 |
| 120 | 0.811 |
|  | 1.000 |
|  |  |

### 2.13.5 Calculation of Radiated BB Interference

To obtain the RF field strength in dB referred to $1 \mu \mathrm{~V} / \mathrm{m} / \mathrm{MHz}$, the ACF in dB for the antenna used must be added to the input signal level in dB obtained in Para- graphs 2.11.2 through 2.11.4.

Perform the calculation as follows:
a. Determine the RF signal input level in dB referred to $1 \mathrm{RV} / \mathrm{MHz}$ as described ir Paragraphs 2.11.2 through 2.11.4.
b. Determine the ACF in dB from the calibration chart for the antenna used at the test frequency.
c. Add the results of steps $a$ and $b$ to obtain the RF field strength of the radiated $B B$ interference in $d B$ referred to $1 \mu \mathrm{~V} / \mathrm{m} / \mathrm{MHz}$.
d. To convert the signal level in dB referred to $1 \mu \mathrm{~V} / \mathrm{m} / \mathrm{MHz}$ directly into microvolts $/ \mathrm{m} / \mathrm{MHz}$ or millivolts $/ \mathrm{m} / \mathrm{MHz}$, refer to Table 2-5.

### 2.13.6 Calculation of Conducted BB Interference Measured with RF Current Probe

Signal levels of conducted BB interference as measured with the RF current probe can be computed in terms of dB referred to 1 microampere per $\mathrm{MHz}(\mu \mathrm{A} / \mathrm{MHz})$. The transfer impedance in dB above or below one ohm must be subtracted from the input signal level in dB obtained in Paragraphs 2.11.2 through 2.11.4.

Perform the calculation as follows:
a. Determine the RF signal input level in dB referred to $1 \mu \mathrm{~V} / \mathrm{MHz}$ as described in Paragraphs 2.11.2 through 2.11.4.
b. Determine the transfer impedance of the current probe in dB at the test frequency from the chart furnished with the current probe.
c. Subtract the transfer impedance figure obtained in step b . from the measured signal level in dB determined in step a. to obtain the value of the conducted BB interference in terms of dB referred to $1 \mathrm{IA} / \mathrm{MHz}$ in the test sample conductor.

## NOTE

The transfer impedance in dB may have a positive or negative sign, depending on being above (positive) or below (negative) the one ohm reference. Observe the sign when subtracting in step c .
d. To convert the signal level in dB referred to $1 \mu \mathrm{~A} / \mathrm{MHz}$ into $\mu \mathrm{A} / \mathrm{MHz}$ or milliamperes $/ \mathrm{MHz}$, refer to Table 2-5 and substitute "ampere" for "volt" in the units given in the table headings.

### 2.13.7 Calculation of Conducted Signal Levels in Picowatts

The methods described in Paragraphs 2.10.2through 2.10.5 are used to measure conducted NB signals in terms of 4 V or dB referred to $1 \mu \mathrm{~V}$. Signal levels may also be expressed in picowatts, considering the 50 ohm input impedance of the $N M-37 / 57$. If $E$ is the $R F$ signal level in $\mu V$, then the input power $P$ in picowatts is: $P=\frac{E^{2}}{50}$ Figure 2-9 is a graphical presentation of this equation giving the input signal in picowatts for any signal voltage from 1 to $1000 \mu \mathrm{~V}$.

Conducted NB signal levels may be also expressed in terms of dBm , or dB referred to 1 milliwatt. The RF signal level for 1 mW across 50 ohms is $(10-3 \mathrm{X} 50) / 2=0.223 \mathrm{~V}=107 \mathrm{~dB}$ above $1 \mu \mathrm{~V}$. To obtain the dBm value of a signal subtract 107 dB from the signal measured in dB above $1 \mu \mathrm{~V}$. (This may be read directly from the dBm scale on the dB meter of the NM-37/57.)

### 2.14 OPERATION WITH X-Y RECORDER

Signal amplitude may be plotted against frequency, as in spectrum signature studies, by connecting an $\mathrm{X}-\mathrm{Y}$ recorder to the NM-37/57. Any suitable X-Y plotter can be used that is compatible with the $\mathrm{X}-\mathrm{Y}$ output characteristics of the NM-37/57. (Refer to the specifications in Table 1-1.) The X-output voltage of the NM-37/57 is proportional to the indicated frequency throughout each band, and the Y -output volt- age is proportional to the signal level as indicated on the dB meter.

The internal scan feature of the NM-37/57 provides semiautomatic frequency tuning over each band in one minute, and also provides a contact closure during the scan period for use as a recorder pen lift control.

The instructions that follow are general and are intended as a guide for the particular test setup and $X-Y$ recorder used.
Proceed as follows:
a. Connect the X-Y cables (Model 90071-1) to the X-Y OUTPUT receptacles on the rear panel of the NM-37/57 and the corresponding input receptacles of the recorder.


Figure 2-9. Signal Power Conversion Chart (Picowatts - Microvolts)
b. Connect a suitable cable between the RECORDER PENLIFT phone jack on the rear panel of the NM-37/57 and the appropriate receptacle on the recorder. A three-conductor phone plug (Military type PJ-068 or equivalent) is required for the RECORDER PENLIFT connection.
c. Turn on the NM-37/57 and set the BAND switch to the desired frequency range. Set the CONTROL MODE switch to LOCAL, the AFC switch to OFF, the BANDWIDTH switch at 1 MHz , and the FUNCTION switch at SLIDEBACK PEAK.
d. Turn on and prepare the $X-Y$ recorder for operation.
e. Rotate the TUNE control on the NM-37/57 to the low frequency end of the band in use and zero the recorder pen on the X -axis.
f. Temporarily disconnect the Y -axis cable to the recorder, and zero the recorder pen on the Y -axis. Re-connect cable.
g. Rotate the TUNE control on the NM-37/57 to the high frequency end of the band in use. Adjust the recorder pen for full scale on the X-axis, then turn the TUNE control back to the low frequency end of the band.
h. Adjust the SLIDEBACK PEAK control on the NM-37/57 to obtain full-scale deflection of the dB meter. Adjust the recorder pen for full scale on the Y-axis, then turn the SLIDEBACK PEAK control back to the counterclock- wise position.
i. Calibrate the NM-37/57 as described in Paragraph 2.9.
j. Connect the proper signal pickup device to the RF INPUT receptacle of the NM-37/57. Set the FUNCTION switch to PEAK/0.3 SEC HOLD.
k. Tune the NM-37/57 slowly across the band in use and observe the dB meter deflection. Adjust the ATTENUATOR control to maintain an on- scale deflection for the strongest signal encountered. Turn the TUNE control back to the low frequency end of the band.
I. To record a spectrum signature of the band, set the CONTROL MODE switch on the NM-37/57 to SCAN and press the SINGLE switch. The receiver will automatically sweep the full frequency range of the band in use in one minute, and will then return to the low frequency end of the band.
m. Repeat steps $\mathrm{i}, \mathrm{k}$, and 1 to record a spectrum signature of each band selected.

### 2.15 OPERATION WITH EXTERNAL SCAN INPUT

The frequency tuning of the NM-37/57 may be remotely controlled independently front remote programming of other functions by using the EXTERNAL SCAN input. This feature should be employed when the application requires a scan time other than one minute for $\mathrm{X}-\mathrm{Y}$ recording, or when a spectrum display is desired. For example, a low frequency function generator may be used as a tuning voltage source. It could be adjusted to produce a 0 to +10 volt ramp function with a scan time of 1000 seconds. This would allow a finely detailed X-Y plot. For spectrum display on an oscilloscope, scan times as fast as 30 milliseconds can be employed.

For $\mathrm{X}-\mathrm{Y}$ recording with external scan, the following general procedure is recommended:
a. Connect and calibrate the equipment as directed in paragraph 2.14
b. Provide a tuning voltage source capable of delivering 0 to +10 volts across 2000 ohms with a scan time suitable for the application.

## CAUTION

Do not exceed +l 5 volts at the EXTERNAL SCAN input jack of the NM-37/57.
c. Connect the tuning voltage source to the EXTERNAL SCAN jack on the NM-37/57 rear panel. Use a standard phone plug (Military type PJ-055 or equivalent) and shielded cable.
d. Set the CONTROL MODE switch to SCAN.

NOTE
Insertion of the phone plug into the EXTERNAL SCAN jack automatically disables the internal sweep circuit.
e. Proceed with the $X-Y$ recording.

## 2-33/(2-34 blank)

## Section III

## THEORY OF OPERATION

The NM-37/57 EMI/FI meter consists of five primary circuit groups: RF, tuning control, IF, detection and display, and power supply. The function and operation of each of these circuits are described in the following paragraphs.

### 3.1 RF CIRCUITS

The RF circuits consist of the turret attenuator switch assembly A45, 2-position RF switch (calibrate switch) A17, impulse calibrator A9, 8-position RF switch A10 and tuners Al thru A8. Refer to Figure 3-1.

### 3.1.1 Turret Attenuator Switch Assembly A45

The turret attenuator switch assembly provides for a maximum of 80 dB attenuation of the RF input signal in 20 dB steps. The turret attenuator provides $0,20,40$, and 60 dB attenuation of the RF input signal. An additional 20 dB attenuation is provided in the IF circuits and is controlled by A45.

In the 0 and -20 positions, the attenuator connects the RF input to calibration switch A17 without attenuation. In the 420, +40 , and +60 positions a coaxial attenuator is connected in series with the input RF signal and attenuates the input the selected amount. The attenuated RF signal is supplied to calibration switch A17. In the IF circuits, an additional 20 dB attenuation is provided when the switch is in any position other than -20 .

### 3.1.2. Calibration Switch A17

Calibration switch A17 is a 2-position RF switch that selects one of two inputs and routes the selected input to the 8position RF switch.

The calibration switch consists of three coaxial reed switches. Two reed switches, one normally open and one normally closed, are connected in series with the RF input and the calibration switch output. The third reed switch is normally open and is between the input from impulse calibrator A9 and the output. Operation of these reed switches is controlled by the FUNCTION switch or the remote function selector A25.


EL2RP050

Figure 3- 1. Simplified Block Diagram, Model NM-37/57

When the calibrate function is selected, the normally closed reed switch in 6crie s with the RF input and the normally open reed switch in series with the calibrate input are energized. This opens the RF input path and closes the calibration input path, supplying the calibration input to the 8-position RF switch A10.

When any function other than calibrate is selected, the normally open reed switch in series with the RF input is energized and the two remaining reed switches are de-energized. This closes the RF input path and opens the calibrate input path, supplying the RF input to 8-position RF switch A] 0.

### 3.1.3 Impulse Calibrator A9

Impulse calibrator A9 generates a short-duration broadband pulse of fixed amplitude. Operation of impulse calibrator A25 is initiated when calibrate is selected at the FUNCTION switch or by remote function selector A25.

In A9, a free-running multivibrator generates a 450 Hz square-wave signal that is applied to a buffer amplifier. The buffer amplifier applies the square-wave signal to a pulse shaping network. The square-wave signal is differentiated in the input of this network to produce a positive pulse with a fast rise time. This pulse is amplified and applied across a tunnel diode to an amplifier. The tunnel diode sharpens the leading edge of the pulse (decreases rise time) so that the output of the amplifier is a short-duration positive pulse with a very fast rise time. This pulse is amplified and applied via a broad-band transformer to a transistor current switch. The input pulse turns the current switch on, resulting in a high-amplitude positive pulse. This pulse is applied to a diode pulse forming network. The diode pulse forming network contains two step recovery diodes. These step recovery diodes shape the pulse to produce an output pulse of very short duration (less than 1 nanosecond) with extremely short rise and fall times.

### 3.1.4 8-Position RF Switch A10

The 8-position RF switch connects the output of the calibration switch to one of eight tuners. The 8-position RF switch consists of eight coaxial reed switches connected to a common input. Each reed switch is normally open and is controlled by the BAND switch or from a remote programmer when the CONTROL switch is positioned at REMOTE. When a band is selected, energizing voltage is supplied to the appropriate reed switch, causing the switch to close. The closed reed switch supplies the input to the appropriate tuner. The remaining reed switches are open, isolating the remaining tuners from the input.

### 3.1.5 Tuners Al Through A8

Tuners Al through A8 are voltage tuned mixer-oscillator stages that convert the RF input to a fixed IF output. Tuners AI through A3 provide a 20.5 MHz IF output and A4 through A8 provide a 160 MHz IF output. Operation of all tuners is similar.

Each tuner contains a preselector, a mixer, and a local oscillator that are voltage tuned. Tuning is controlled by the tuning control circuits, which supply a variable tuning voltage to the tuner. When properly tuned, the local oscillator produces a frequency that is 20.5 MHz (Al through A3) or 160 MHz (A4 through A8) above the RF input signal. The oscillator output is applied to the mixer, which receives the output of the preselector. The preselector is a tuned RF amplifier. The output of the mixer is a 20.5 MHz (Al through A3) or 160 MHz (A4 through A8) signal containing any modulation present on the RF input signal. The output of the tuner is applied to 5 -position and 3 -position IF switch All. As an option, the output of the local oscillator can be routed to LOCAL OSCILLATOR jacks on the rear panel to permit monitoring by external equipment.

### 3.2 TUNING CONTROL CIRCUITS

The tuning control circuits tune the RF and local oscillator circuits to the desired frequency. The tuning control circuits are band selector A30, tuning control A29, shapers A26 and A27, frequency meter A47, internal sweep A33, and frequency readout A34.

### 3.2.1 Band Selector A30

Band selector A30, under control of the BAND switch or remote selection inputs, selects the tuning band of the EMI/FI meter by applying energizing voltage to the tuner for the selected band, applying electronic tuning signals to the selected tuner, and applying switching signals to the IF circuits.

When the CONTROL MODE switch is set at the LOCAL or SCAN position, a -12 V signal is applied to the BAND switch. Setting the BAND switch to the desired frequency band routes the - 12 V signal to band selector A30, 8 -position RF switch A10, and 5 -position and 3 -position RF switch All in the IF circuits. The -12 V signal to switches A10 and All cause the switches to select the input and output of the tuner for the desired band. The -12 V signal to band selector A30
energizes a relay corresponding to the selected band. This relay applies a -12 V signal to the appropriate tuner to energize the tuner and to frequency meter A47 to light the band indicators corresponding to the selected band. This relay also connects electronic tuning signals from shaper I or 2 to the energized tuner. The band select relays in A30 also route -12 V switching signals to the IF circuits to select proper IF signal processing for the selected frequency band.

When the CONTROL MODE switch is set at the REMOTE position, band selection is accomplished in the same manner as in the LOCAL mode except that band select signals are supplied to band selector A30 from an external source via the PROGRAMMER connector on the rear panel.

### 3.2.2 Tuning Control A29

Tuning to a precise frequency within a selected band is accomplished by tuning control A29 under control of the TUNE and FINE TUNE controls or a signal from an external source.

When the CONTROL MODE switch is set at the LOCAL position, tuning control A29 generates a precise voltage output under control of the TUNE and FINE TUNE controls. A precise voltage control circuit in A29 responds to the tuning controls by providing a 0 V to +10 VDC output. This precise voltage output is routed to frequency meter A47, the X OUTPUT jack on the rear panel, frequency readout A34, and via shaper select relays to shaper A26 or A27. The shaper select relays operate under control of band selector A30.

When band 1,2 , or 3 is selected, the precise voltage output is applied to shaper A26. When band 4 thru 8 is selected, the precise voltage output is applied to shaper A27.

When the automatic frequency control (AFC) function is turned on at the AFC switch, A29 receives an AFC signal from FM discriminator A18 in the detection and display circuits. As the RF input frequency varies around the tuned frequency, the voltage of the AFC signal varies. In A29, the AFC signal is applied to the voltage control circuit. As the AFC signal varies, the voltage control circuit varies the precise voltage output. This causes the selected tuner to follow the drift of the RF input signal.

When the CONTROL MODE switch is set at the SCAN position, A29 applies the output of internal sweep A33 to the proper shaper for the selected band.

When the CONTROL MODE switch is set at the REMOTE position, AZ9 applies tuning control voltage from an external source to the proper shaper for the selected band. Tuning control at the front panel is disabled.

### 3.2.3. Shapers A26 and A27

Shapers A26 and A27 generate output voltages that control tuning devices in the tuners. Shaper A26 controls tuners AI, AZ, and A3 and shaper A27 controls tuners A4 thru A8. As the TUNE and FINE TUNE controls are changed from minimum to maximum settings, the voltage output of tuning control A29 is a linear voltage change from 0 to +10 volts. This linear voltage change is applied to the shaper, which produces a nonlinear voltage change that is applied to the tuning devices in the tuners.

Tuning is accomplished by varactor diodes in the tuners. Varactor diodes are solid-state devices whose capacitance is controlled by the voltage applied to the varactor. Varactors are nonlinear devices; i.e., a linear change in voltage will not cause a linear change in capacitance. Shapers A26 and A27 compensate for this nonlinearity by producing a nonlinear output voltage that produces a change of capacitance in the varactors that causes a linear change in the tuned frequency. As the output of tuning control A29 changes linearly from 0 V to +10 V , the output of AZ6 or A27 is nonlinear to produce a linear change in frequency from the low end to the high end of each band.

The voltage output of the shaper is routed through the band select relays in A30 to the selected tuner, where it is applied to the varactors. Each tuner has three varactor tuned circuits: preselector, mixer, and local oscillator. The voltage applied to the varactor determines the capacitance of the varactor, which determines the resonant frequency of the circuit containing the varactor. In this manner the tuners are electronically tuned to a desired frequency.

### 3.2.4 Frequency Meter A47

The frequency meter monitors the tuning control voltage output from A29 and indicates the frequency to which the NM$37 / 57$ is tuned. Frequency is displayed on eight linearly graduated scales which correspond to the eight tuning bands of the receiver. Light emitting diodes (LED) are used to indicate the selected frequency band.

### 3.2.5 Internal Sweep A33

When the CONTROL MODE switch is set at SCAN and the SINGLE pushbutton is pressed, interanl sweep A33 generates a sawtooth voltage that rises from 0 to 10 volts in 60 seconds. This sawtooth voltage is applied to shaper A26 or A27 via tuner control A29, and causes the selected tuner to sweep the band from the low end to the high end in 60 seconds.

To generate the sawtooth voltage, A33 contains a ramp generator, a comparator, a relay driver, and a relay. When the SINGLE pushbutton is pressed, the relay driver causes the relay to energize and initiate operation of the ramp generator. The ramp generator produces the sawtooth voltage that rises from 0 to 10 volts in 60 seconds. The comparator monitors the output of the sweep generator and applies a pulse to the relay driver when the output reaches 10 volts. This pulse causes the relay driver to de-energize the relay, stopping operation of the ramp generator. A second set of contacts on the relay provide an isolated closure across the RECORDER PEN LIFT jack on the rear panel.

### 3.2.6 Frequency Readout A34

The frequency readout circuits provide a scaled voltage output of $10 \mathrm{mV}, / \mathrm{MHz}$ that is representative of the tuned frequency of the NM-37,/57. This output is available at the PROGRAMMER receptacle and may be applied to a digital voltmeter to obtain a digital readout of received frequency.

The scaling is accomplished by combining the tuning control voltage from A29 with a bandswitched voltage which is proportional to the minimum frequency of the selected band. The voltage combining circuitry employs operational amplifiers and resistive scaling networks selected by reed relays.

The voltage output of A34 is an electrical analog of the tuned frequency as follows: band $1,300 \mathrm{mV}$ to 570 mV ; band 2,550 mV to 1050 mV ; band 3, 1010 mV to 1920 mV ; band $4,1860 \mathrm{mV}$ to 2920 mV ; band $5,2850 \mathrm{mV}$ to 4450 mV ; band 6, 4300 mV to 6200 mV ; band $7,6000 \mathrm{mV}$ to 8250 mV ; and band $8,8000 \mathrm{mV}$ to $10,000 \mathrm{mV}$.

### 3.3 IF CIRCUITS

The IF circuits amplify the output of the tuners to obtain a signal level that is useable in the detection and display circuits. The IF circuits also provide signal attenuation when desired and video signals for display on external equipment.

The IF circuits consist of 5 -position and 3-position IF switch All, 160/20. 5 MHz IF converter A12, IF preamplifier A13, voltage controlled attenuator A48, bandwidth selector A14, linear IF amplifier and BFO A15, and logarithmic IF amplifier A41.

### 3.3.1 $\quad 5$-Position and 3 -Position IF Switch All

The 5-position and 3-position IF switch connects the IF output of the selected tuner to the proper IF module. It consists of two coaxial reed switch sets in one module. One coaxial reed switch set contains five normally open coaxial reed switches with a common output. This switch set connects the output of tuners A4 thru A8 to $160 / 20.5 \mathrm{MHz}$ converter A12. The remaining switch set contains three normally - open coaxial reed switches with a common output. This set connects the output of AI, AZ, or A3 to IF preamplifier A13.

The 5-position and 3-position IF switch is controlled by band select signals from the BAND switch. When a band is selected, a band select signal is applied to the coaxial reed switch connected to the output of the tuner for the selected band. The band select signal causes the coaxial reed switch to close and connect the IF output of the tuner to the proper IF circuit.

### 3.3.2 $\quad 160 / 20.5 \mathrm{MHz}$ IF Converter A12

The 160 MHz IF output of selected tuner A4 thru A8 is routed through a bandpass filter to 160/20.5 IF converter A12 by 5position and 3 -position IF switch All. The converter changes the 160 MHz input signal to a 20.5 MHz signal for compatability with the remainder of the IF circuits. To accomplish the 160 MHz to 20.5 MHz conversion, A12 contains an oscillator, a frequency doubler, a mixer, and a 20. 5 MHz amplifier.

The oscillator is crystal controlled at 69.75 MHz , and its output is applied to the frequency doubler. The frequency doubler is basically an RF amplifier tuned to 139.5 MHz , which is the second harmonic of the 69.75 MHz output of the oscillator. The 139.5 MHz output of the frequency doubler is applied to the mixer. The mixer also receives the 160 MHz input from the tuner. The output of the mixer is the difference between the two inputs: 160 MHz 139.5 MHz , which is 20 . 5 MHz . The 20. 5 MHz output of the mixer is applied to 20.5 MHz amplifier. This amplifier increases the amplitude of the 20.5 MHz signal and suppresses other frequency
outputs of the mixer. The 20. 5 MHz IF signal output of A12 is routed to IF preamplifier A13.
The converter only operates when one of bands 4 thru 8 is selected. When one of these bands is selected, a -12 V signal is applied to A12 by band selector A30. This -12 V signal signal initiates operation of the four stages in A12. When band 1,2 , or 3 is selected, A12 does not operate.

### 3.3.3 $\quad$ 20.5 MHz IF Preamplifier A13

The IF preamplifier performs three functions: IF switching, IF amplification, and IF attenuation.
IF switching is controlled by frequency band selection and determines if the IF amplifier circuits in A13 are used. The IF switching is accomplished by a relay. When band 1,2 , or 3 is selected, a band 1 thru 3 select signal ( -12 V ) is received from band selector A30 and 20. 5 MHz input is received from tuner AI, A2, or A3 via All. The band 1 thru 3 select signal energizes the IF switching relay and energizes the IF preamplifier circuits. The energized IF switching relay connects the output of the IF preamplifier circuits to the IF attenuation circuit. When a band other than 1, 2, or 3 is selected, the IF switching relay is de-energized and the IF amplifier circuits are not energized. In the de-energized condition, the IF switching relay connects the 20.5 MHz signal received from A12 to the IF attenuation circuit and disconnects the output of the IF amplifier circuits.

When energized (band 1, 2, or 3 selected), the IF amplifier circuits provide increased signal amplitude and undesired frequency rejection. These circuits consist of two 20.5 MHz amplifier stages.

The IF attenuator circuit contains two relays and a 20 dB resistive attenuator. The attenuator is switched into or out of the 20.5 MHz IF signal path by the two relays under control of the ATTENUATOR switch. When the ATTENUATOR switch is at any position other than -20 dB , the relays switch the attenuator into the signal path and any signal passing through A13 is attenuated 20 dB . When the switch is positioned to -20 dB , the relays switch the attenuator out of the signal path and no attenuation occurs.

### 3.3.4 Voltage Controlled Attenuator A48

The voltage controlled attenuator provides compensation for changes in gain in the EMI/FI meter circuits. When the FUNCTION switch is positioned to CALIBRATE,
a fixed-value broadband signal is applied to the tuner selected by the BAND switch. This known input should cause a specific display on the dB meter. If the dB meter display is not as specified, minor gain changes have occurred in the circuits. Operation of a CALIBRATE control on the voltage controlled attenuator causes an increase or decrease in attenuation of the 20. 5 MHz IF signal. The change in signal attenuation results in a change in the dB meter indication. This permits the overall gain of the NM-37/57 to be adjusted so that a know input results in a specific dB meter display.

Voltage controlled attenuator A48 permits IF signal attenuation of up to $20+2 \mathrm{~dB}$. Attenuation of the IF signal is accomplished by a bridged-T resistive attenuator network that contains two PIN diodes as variable resistors.

The amount of attenuation provided is controlled by varying the bias applied to the PIN diodes. This bias is provided by two operational amplifiers. The CALIBRATE control provides an input signal to the two operational amplifiers. This signal determines the bias voltages which are applied to the PIN diodes to control resistance. Operation of the CALIBRATE control causes the operational amplifiers to change the PIN diode bias, resulting in a proportional change in signal attenuation.

### 3.3.5 Bandwidth Selector A14

The bandwidth selector permits the operator to select either a $10 \mathrm{kHz}, 100 \mathrm{kHz}$, or a 1 MHz bandwidth of the 20.5 MHz IF signal. Bandwidth selection is controlled by the BANDWIDTH switch and accomplished by bandpass filters in A14. Positioning the BANDWIDTH switch to the desired bandwidth causes one of three sets of input and output relays in A14 to energize The energized relays connect the 20.5 MHz IF signal to the bandpass filter with the desired bandwidth, and connect the output of that filter to the output of A14. Each bandpass filter has a center frequency of 20.5 MHz .

### 3.3.6 Linear IF Amplifier and BFO A15

The linear IF amplifier and BFO provides IF signal amplification and signal detection to produce audio and video outputs. Four stages of IF amplification, a diode detector, a video amplifier, and a BFO are included in A15.

Three IF amplifier stages, connected in cascade, amplify the 20.5 MHz IF signal. The amplified IF signal is applied to the diode detector circuit. The diode detector
circuit rectifies and filters the 20.5 MHz signal to detect any amplitude modulation present on the input. The output of the detector is applied to an AGC circuit and to the video amplifier. The AGC circuit monitors signal amplitude and routes a signal to the first IF amplifier to control gain. The common-collector video amplifier provides isolation of output and impedance matching of the output to the load. This amplifier has two outputs. One output, audio, is routed through the FUNCTION and CONTROL MODE switches to the AUDIO switch. When the AUDIO switch is in the AM position, this audio signal is routed through the AUDIO GAIN control to dB readout and audio amplifier A24. The second output of the common-collector amplifier is routed to the LINEAR VIDEO connector on the rear panel. This output is provided so that the output of A15 can be displayed on an oscilloscope.

The BFO is controlled by the FUNCTION switch and is normally used when a CW signal is being monitored. When the FUNCTION switch is set at BFO, a +12 V signal is supplied to the BFO to initiate operation. The BFO is a 20.501 MHz crystal-controlled oscillator. The 20. 501 MHz output of the BFO is applied to the input of the detector circuit. In the detector circuit, the 20.5 MHz IF signal is mixed with the 20.501 MHz BFO signal and the result is detected. The deviation of the audio signal above or below 1 kHz is the inverse representative of the change of frequency of the IF signal about 20.5 MHz .

The fourth IF amplifier in A1 5 provides a buffered 20.5 MHz IF signal to the IF OUTPUT jack on the rear panel.

### 3.3.7 Logarithmic IF Amplifier A41

Instantaneous logarithmic compression and detection of the IF signal is accomplished by A41. Logarithmic compression results in maximum amplification of small amplitude input signals and minimum amplification of large amplitude input signals. The amplitude of the output of A41 is a logarithmic function of the amplitude of the input signal. A 1 dB increase in input signal amplitude results in a 50 mV increase in output signal amplitude.

Logarithmic IF amplifier A41 contains seven stages of IF amplification, each containing a detector. The seven IF amplifiers are connected in cascade; the detector outputs of the seven stages are connected in parallel. At minimum input signal amplitude, the IF signal is amplified by all seven stages. However, only the detected output of the seventh stage is significant. As input signal amplitude increases, the seventh IF amplifier saturates and the detected output of the sixth
stage becomes significant. The detected output of the sixth stage is summed with the detected output of the seventh stage. This action continues from sixth stage to first stage as input signal amplitude is increased. The detected outputs of the seven stages are summed and applied to an emitter follower. This action results in sequential detection of the IF signal as a result of input signal amplitude and the gain of the stages is such that the output amplitude is a logarithmic function of input amplitude. Because of this logarithmic response, any modulation present on the IF signal will be distorted in the output.

Two outputs are provided by the emitter follower that receives the detected outputs of the seven IF stages. One output is routed through a buffer network to the LOG VIDEO jack on the rear panel. The other output of the emitter follower is routed via the LOCAL and SCAN positions of the CONTROL MODE switch to the FUNCTION switch. Depending on the selected function, this output of A41 is routed to weighting and meter amplifier A21, direct peak detector A22, or slideback peak detector A23.

The IF signal output of the seventh IF stage in A41 is routed to FM discriminator A18. The amplitude of this IF output is limited by saturation of the seventh (and possibly preceding stages) and is not representative of the input IF signal amplitude.

### 3.4 DETECTION AND DISPLAY CIRCUITS

The detection and display circuits perform the desired signal detection and processing, and display the results. The detection and display circuits are FM discriminator A18, slideback peak circuit A23, weighting and meter amplifier A21, direct peak circuit $A Z Z 2$, $d B$ readout and audio amplifier $A 24$, dB meter $A 46$, and remote function selector $A 25$. The functions performed and the circuits used are selected by the FUNCTION switch or by the remote function selector A25 when a remote programmer is used.

### 3.4.1 FM Discriminator A18

Any change in the frequency of the 20. 5 MHz IF signal is detected by FM discriminator A18, which provides voltage outputs representative of the change. The FM discriminator contains a driver amplifier, an FM discriminator, and an output amplifier.

The driver amplifier amplifies the IF signal received from A41 and applies the signal to the FM discriminator. The FM discriminator detects any change of
frequency in the input signal and generates a DC output voltage whose polarity is representative of the direction of change and amplitude represents the amount of change. The discriminator contains two half-wave rectifiers with tuned inputs.

One rectifier has an input circuit tuned to 20.2 MHz and produces a positive output signal. The other rectifier has an input circuit tuned to 20.8 MHz and produces a negative output. The outputs of the two rectifiers are summed and applied to the output amplifier. With a 20.5 MHz input the outputs of the two rectifiers are of equal amplitude and opposite polarity; thus the input to the amplifier is 0 volts. When the input frequency is above or below 20.5 MHz , the output of one rectifier is greater than the output of the other and the input to the amplifier is a positive or negative signal. The output amplifier amplifies the output of the discriminator to provide three outputs. One output is routed through a low-pass filter in A18 to the FM VIDEO jack on the rear panel. The second output of the amplifier is routed to the AUDIO switch. When this switch is at the FM position, the signal is routed through the GAIN control dB readout and audio amplifier A24. The third output of the amplifier is routed to the AFC switch as an automatic frequency control signal. When the AFC switch is set at ON, the signal is routed to tuning control A29.

### 3.4.2 Slideback Peak Circuit A23

The slideback peak circuit provides a means of determining the peak value of any signal detected by logarithmic IF amplifier A41. When a CW signal is applied to the input of the NM-37,/57, the detected signal is DC. When a AM signal is applied to the input of the NM-37/57, the detected signal contains the modulation superimposed on the DC level. When a short pulse is applied to the input of the NM-37/ 57, the detected signal is a pulse having a width that is inversely proportional to the bandwidth. Such short pulses can not be indicated directly by the dB meter. The slideback peak method substitutes an equivalent DC voltage which can be measured by the meter amplifier and displayed on the dB meter.

Slideback peak circuit A23 contains a comparator, a pulse stretcher, a gate, and a free running multivibrator. The comparator compares the detected signal with a manually-controlled slideback peak voltage. When the peak of the detected signal exceeds the slideback voltage, the comparator opens the gate, which turns on the multivibrator. The constant tone of the multivibrator is connected via the FUNCTION switch, the AUDIO switch, and the AUDIO GAIN control to the audio
amplifier circuit on A24. When the manually-controlled slideback voltage equals or exceeds the peak of the detected signal, the comparator closes the gate and cuts off the multivibrator. By slowly increasing the slideback voltage until the tone in the headphone just stops, a precise aural monitoring of the detected peak level is obtained. The slideback voltage is connected via the FUNCTION switch to the meter amplifier and is displayed on the dB meter. The stretcher between comparator and gate serves to stretch short pulses to the risetime of the gate.

In addition to the components described above, slideback peak circuit A23 contains a rectifier and adder circuit which are connected via the FUNCTION switch to the Y OUTPUT jack. When the detected signal exceeds the slideback voltage, the Y output is the sum of the slideback voltage ( 0 to 1 V ) and rectified multivibrator output (about 100 mV ). When the slideback voltage equals or exceeds the detected signal level, the Y output equals the slideback peak voltage displayed on the dB meter. This circuit enables the NM-37/57 to indicate and plot any signal above a selected threshold level.

### 3.4.3 Weighting and Meter Amplifier AZ1

The weighting and meter amplifier performs signal weighting and meter scaling of signals to be displayed on the dB meter. The weighting and meter amplifier contains a field intensity (FI) weighting amplifier, a quasi-peak (QP) weighting amplifier, and a meter amplifier. The FI amplifier is used in the field intensity and BFO modes. The QP amplifier is used in the quasi-peak and calibrate modes. The meter amplifier operates in all modes. The FI amplifier provides an output voltage that is the average of the input voltage. The input circuit of the FI amplifier contains a resistor and capacitor network with a charge time and a discharge time of approximately 0.6 second. The voltage across the capacitor at any given time is the average of the input voltage. This voltage is applied to the amplifier, which has unity gain. The output of the FI amplifier is routed through the function selector to the input of the meter amplifier.

The QP amplifier provides an output that is the quasi-peak value of the input signal. The input circuit of this amplifier contains a diode and a resistor-capacitor network. When an input is applied, the capacitor is charged through the diode to the positive value of the input signal. Each time the input voltage rises above the charge level of the capacitor, the diode conducts and charges the capacitor to the new peak value. The charge time is relatively short, approximately one microsecond. The discharge time of the capacitor is relatively long approximately 600 milliseconds, and
therefore the voltage charge on the capacitor at any time is the quasi-peak value of the input signal. This voltage is applied to the amplifier, which has unity gain The output of the QP amplifier is routed through the function selector to the meter amplifier. The output voltage swing of the detector circuits is from 0.6 to 3.6 volts. The meter amplifier shifts this voltage swing to from 0 to 3.0 volts and provides current amplification to drive the following circuitry. The 0 to 3 -volt output is applied to two resistive divider networks and to dB readout and audio amplifier A24. The two divider networks produce 0 to 1 volt outputs: one is applied to dB meter A46 and the other is routed to the Y OUTPUT jack on the rear panel during all functions except slideback peak.

### 3.4.4 Direct Peak Circuit AZZ

The direct peak circuit enables measurement of the peak value of signals. To enable peak measurement, the direct peak circuit detects and holds the peak value of the input signal. The amount of time that the peak value is held is selectable. The direct peak circuit contains two pulse stretchers and a dump circuit.

The first pulse stretcher is very sensitive and fast-reacting, and performs a small degree of stretching. This pulse stretcher receives the input signal and consists of a differential comparator, a switching transistor, an RC network, and an FET follower. The differential comparator compares the peak amplitude of a received pulse against the peak value stored in the pulse stretcher. When the input amplitude is greater than the stored amplitude, the comparator is unbalanced and produces an output that causes the switching transistor to turn on. The biasing of the switching transistor is such that the transistor reacts very rapidly to a small input. Thus, a short duration pulse with an amplitude only slightly greater than the stored amplitude will turn on the switching transistor. The switching transistor provides a rapid charge path for the capacitor in the RC network. The charge on the capacitor is transferred via the FET follower to the differential comparator. When the capacitor charge equals the input peak value, the comparator is balanced and the switching transistor is turned off. The capacitor now begins to discharge. The discharge time of the capacitor is long so that the input pulse is stretched. As long as no input occurs with a peak value greater than the present charge, the capacitor will continue to discharge. If an input occurs with an amplitude greater than the capacitor charge, the capacitor is charged to this new value. The output of the FET follower is also applied to the second pulse stretcher.

The second pulse stretcher has a slower response than the first and holds the peak amplitude until dumped by the dump circuit (up to 3 seconds hold time). This pulse i stretcher consists of a comparator, a switching diode, a RC network, and an FET follower. Operation of the second pulse stretcher is similiar to operation of the first in that the comparator causes the capacitor to be charged when the input is greater than the stored amplitude. Response time of the second pulse stretcher is slower than the first because a larger storage capacitor is used. The requirement for fast response time is reduced because of the pulse stretching accomplished in the first pulse stretcher. The most significant difference between the first and second pulse stretcher is that no discharge path is provided for the capacitor in the second pulse stretcher. Therefore, the capacitor maintains its charge, holding the peak amplitude. The capacitor charge is applied to the FET follower, whose output is applied to the comparator and is the peak amplitude output of the direct peak circuit.

The time that the peak amplitude is held in the second pulse stretcher is selectable at $0.05,0.3$ or 3 seconds. Discharging of the capacitor in the second pulse strecher after the selected time interval is accomplished by the dump circuit. The dump circuit consists of a differential comparator, two switching transistors, an RC network, and two relays. The differential comparator monitors the voltage levels stored in the two pulse stretchers. As long as the input signal remains constant or is increasing in amplitude, the voltage level in the first pulse stretcher is equal to or greater than the voltage level in the second pulse stretcher. With this condition, the dump circuit comparator produces an output that turns on a switching transistor. This turned on switching transistor prevents charging of the capacitor in the RC network. When the input signal decreases in peak amplitude, the voltage in the first pulse stretcher decreases. With this condition the dump circuit comparator causes the switching transistor to turn off and permit the capacitor to charge. The charge on the capacitor is coupled via a unijunction transistor to the second switching transistor. When the capacitor charge reaches a certain value, the unijunction transistor causes the second switching transistor to turn on. When turned on, the second switching transistor provides a very rapid discharge path for the capacitor in the second pulse stretcher. Discharge of this capacitor reduces the voltage level stored in the second pulse stretcher. When the voltage level in the second pulse stretcher is reduced to a point that is equal to the voltage level in the first pulse stretcher, the dump circuit comparator turns on the first switching transistor.

This switching transistor discharges the capacitor in the dump circuit causing the second switching transistors to turn off. Discharge of the second pulse stretcher capacitor is stopped and the voltage stored is equal to the input peak value. The time interval between the reduction of the input peak value and dumping of the second pulse stretcher is determined by the charge time of the capacitor in the dump circuit. The two relays in the dump circuit select the resistance in the capacitor charge path to control charge time. When the selected hold time is 3 seconds, both relays are de-energized. In the 0.05 and 0.3 second positions, a relay is energized to select a decreased resistance to decrease capacitor charge time from 3 seconds to either 0.05 or 0.3 seconds.

During the time the dump circuit capacitor is charging, an input with a peak amplitude equal to or greater than the level stored in the second pulse stretcher will stop operation of the dump circuit.

### 3.4.5 DB Readout and Audio Amplifier A24

The dB readout and audio amplifier provides an electrical analog of measured signal strength in dB and amplification of audio signals to drive headsets.

The dB readout is accomplished by adding a voltage which is proportional to the RF ATTENUATOR setting to a voltage which is proportional to the dB meter reading. The addition is performed by a summing network controlled by relays. The relays are energized by the ATTENUATOR switch and add a fixed voltage corresponding to the ATTENUATOR setting. The 0 to 3volt output of weighting and meter Amplifier circuit A21 is also applied to the summing network which scales both inputs to a 1 -millivolt-per-dB output. The output of the summing network is routed to the PROGRAMMER connector on the rear panel to enable readout of measured signal strength to external equipment.

The dB readout and audio amplifier alos contains a diode logic circuit. This circuit controls relays in the IF attenuator in IF preamplifier A13. When the ATTENUATOR switch is set at any position other than -20, the diode logic circuit routes a signal to A13 that causes the IF attenuator to be in the IF signal path. With the ATTENUATOR switch set at -20, the diode logic circuit removes the signal causing the IF attenuator to be removed from the IF signal path run-in. The audio amplifier consists of an integrated -circuit audio driver and a push-pull power amplifier.

### 3.4.6 DB Meter A46

The dB meter displays measured signal strength or battery condition. When the POWER switch is at the ON AC or ON BATT position, the dB meter displays signal strength. With the switch at the CHARGE or BATT TEST position, the dB meter indicates battery condition. The meter has full scale deflection with a I V DC input and has a microvolt, a dB referred to 1 microvolt, a -dBm, and a battery condition scale.

### 3.4.7 Remote Function Selector A25

The remote function selector enables control of the EMI/FI meter function from an external programmer. The remote function selector operates only when the CONTROLI, NODE switch is set at REMOTE. With the remote control mode selected, all inputs to the FUNCTION switch are removed and the output of logarithmic IF amplifier A41 is applied to the remote function selector. The field intensity (FT), quasi-peak (QP), direct peak, or calibrate functions can now be selected by a remote programmer.

To select a function, the remote programmer applies +12 volts to the appropriate A25 input via the PROGRAMMER connector. Selection of the Ft, QP, or direct peak mode energizes an appropriate relay in A25. The energized relay routes the output of the logarithmic IF amplifier to the FI or QP weighting circuit in A21 or to direct peak circuit A22. The output of the selected FI, QP, or direct peak circuit is routed through the energized relay to the meter amplifier in AZ1. Normal signal strength display and readout is performed by A21 and A24. The direct peak is selected by the remote programmer by applying -12 volts to one of three lines. Voltage on any of the three causes the proper DPk relay in A25 to energize, and the hold time ( $0.05,0.3$, or 3 seconds) of the direct peak circuit is determined by the line to which the -12 volts is applied.

When selected by the remote programmer, the calibrate function operates in the same manner as when selected at the FUNCTION switch. Usually the calibrate function is selected at the remote programmer to permit calibration of the device that is recording or displaying the dB output from dB readout and audio amplifier A 24 . If the $\mathrm{NNI}-37 / 57$ requires calibration it is accomplished in the same manner as in the local mode (operation of CALIBRATE control).

The remote function selector enables the remote programmer to perform simultaneous direct peak and FI measurements. The remote function selector contains
an FI amplifier that operates in the same manner as the FI amplifier in A21. When the direct peak mode is selected, the logarithmic IF amplifier output is applied to this FI amplifier and A22. The NM-37/57 performs a normal direct peak measurement and the FI amplifier in A25 provides a simultaneous FI measurement output to the remote programmer.

### 3.5 POWER SUPPLY

The power supply provides the +12 VDC and +100 VDC necessary for operation of the NM-37/57. The power supply accepts 100 V or 220 V 50 to 400 Hz input power to develop the necessary voltages. It also contains a battery package to permit up to 8 hours operation without external power. The power supply contains power transformer A42, rectifier-charge regulator A32, voltage regulator A31, DC/DC converter A16, and battery assembly A44.

### 3.5.1 Power Transformer A42

The power transformer has two primary windings. With the $115 / 230 \mathrm{~V}$ switch on the rear panel at the 115 position, the two primaries are connected in parallel. With the switch at the 230 V position, the primaries are connected in series. Both secondaries produce an output of approximately 22 volts. The secondaries outputs are applied to rectifier-charge regulator A32.

### 3.5.2 Rectifier-Charge Regulator A32

The rectifier-charge regulator contains two rectifiers and two battery charge regulators. The two rectifiers produce outputs of approximately $\pm 27$ volts. This is applied to the battery charge regulators and via the ON AC position of the POWER switch to A31 and A16. The battery charge regulators monitor battery voltage levels and supply charging current to the batteries. With the POWER switch set to ON AC, trickle charge current is applied to the batteries. With the POWER switch at CHARGE, full charging current is applied.

### 3.5.3 Voltage Regulator A31

Voltage regulator A31 receives the output of the rectifiers or batteries and produces outputs of $\pm 12$ VDC. The voltage regulator contains an overload protection circuit which limits the output current to 600 mA .

### 3.5.4 DC/DC Converter A16

The DC-to-DC converter employs an electronic chopper and rectifier to convert the input from the rectifiers or batteries to a +100 VDC output. To keep the 100 -volt output constant at varying battery levels, a pre-regulator is applied before the chopper circuit.

### 3.5.5 Battery Assembly A44

The battery assembly contains 2 groups of nickle-cadium batteries rated at 17.5 volts.

## NOTE

Refer to Appendix Afor supplementary battery information.

## Section IV.

## MAINTENANCE

### 4.1 INTRODUCTION

This section of the manual contains minimum performance test procedures, disassembly procedures, and alignment procedures for the NM-37/57. The mini-mum performance test procedures are intended for verification that the NM-37/57 is functioning in accordance with the specification requirements listed in Section I. Disassembly procedures are presented as necessary for ordinary maintenance requirements. Disassembly of the NM-37/57 beyond the extent provided in this section is not recommended.

The maintenance and alignment procedures presented in this section of the manual are intended for use only by skilled personnel, well-qualified and experienced in the calibration and maintenance of laboratory test equipment. Alignment of the NM-37/57 should not be attempted unless proper test equipment is available and unless the instructions given in this manual are clearly understood and realignment is definitely required. The alignment procedures progress from the output circuits back through the instrument to the RF input section. The procedures for each functional section of the NM-37/57 should be performed in the sequence given, and satisfactory results obtained in each section before proceeding to the next section.

No scheduled, periodic maintenance of the NM-37/57 is required. The test procedures should be used to establish the operational performance capability of the instrument, and to assist in isolating a possible malfunction to a specific section. Use normal troubleshooting techniques to further isolate the fault to the component level. Replace the faulty component, then test and realign the unit as necessary.

### 4.2 MINIMUM PERFORMANCE TEST PROCEDURES

The test procedures contained in Table 4-1 may be used to establish the performance of the NM-37/57 within acceptable limits. The test equipment required is listed in Paragraph 4.2.1.

Perform the preliminary procedures in Paragraph 2.5to apply power and check battery condition, then set the controls of the NM-37/57 to be tested in accordance with the initial settings given in Paragraph 4.2.2 and proceed to Table 4-1. Follow the sequence of the tests as given in the table.

## 4. 2. 1 Test Equipment Required

The following test equipment (or equivalent) is required for conducting the minimum performance test of the NM-37/57:
Signal Generator, HP 608E
Signal Generator, HP 612A
Sweep Generator, Wavetek Model 2001
Oscilloscope, Tektronix 535A
Digital Voltmeter, HP 3440A
RF Millivoltmeter, HP 411A
Impulse Generator, Singer Model 91263-1
Step Attenuator (10 dB per step), HP 355D
VSWR Bridge, Telonic TRB-3

### 4.2.2 Initial Control Settings

Set the following controls of the NM-37/57 to the position indicated before beginning the tests given in Table 4-1

Control
BAND switch
BANDWIDTH switch
ATTENUATOR switch
CONTROL MODE switch
TUNE control
AFC switch
FINE TUNE control
FUNCTION switch
POWER switch

Position
$30-57 \mathrm{MHz}$
0.1 MHz

0 dB
LOCAL
Fully ccw
OFF
Fully ccw
PEAK/0.3 SEC HOLD
ON AC

## Table 4-1. Minimum Performance Test Procedures

| Procedure | Acceptable Indication |
| :---: | :---: |

## A. FREQUENCY RANGE AND ACCURACY TEST

Connect the horizontal and vertical outputs of Sweep Generator (Wavetek Model 2001) to the corresponding inputs of Oscilloscope (Tektronix 535A). Connect the RF output of the Sweep Generator to the RF INPUT receptacle of the NM-37/57. Connect the LOG VIDEO output receptacle (rear panel) of the NM-37/57 to the video input of the Sweep Generator. Adjust the Sweep Generator for a sweep range from 30 to 60 MHz at an output level of -67 dBm and turn on the 10 MHz and 50 MHz markers. Adjust the Oscilloscope vertical and horizontal gain to display the full sweep range. Set the NM-37/57 controls as specified in Paragraph 4.2.2.

## Band 1

Tune the NM-37/57 sequentially to exactly 30,40 , and 50 MHz as indicated on the Oscilloscope using the markers as reference. Use the TUNE control only -- leave FINE TUNE control fully ccw. Record the frequency indicated on the front panel frequency meter at each test frequency.

## Band 2

Set the NM-37/57 BAND switch to $55-105 \mathrm{MHz}$ (Band 2) and adjust the Sweep Generator for a sweep from 50 to 110 MHz . Tune the NM-37/57 to 60 , 80 , and 100 MHz and record the frequency meter indication.

## Band 3

Set the NM-37/57 BAND switch to $101-192 \mathrm{MHz}$ (Band 3) and adjust the Sweep Generator for a sweep from 100 to 200 MHz . Tune the NM-37/57 to 110 , 130,160 , and 190 MHz and record the frequency meter indication.

The NM-37/57 frequency meter indication is within $\pm 2 \%$ of all test frequencies.

Same as for Band 1.

Same as for Band 1.

Table 4-1. Minimum Performance Test Procedures (Continued)

| Procedure | Acceptable Indication |
| :---: | :---: |
| Band 4 |  |
| Set the NM-37/57 BAND switch to $186-292 \mathrm{MHz}$ (Band 4) and adjust the Sweep Generator for a sweep from 180 to 300 MHz . <br> 220,260 , and 290 MHz and record the frequency meter indication. | Same as for Band 1. Tune the NM-37/57 to 190, |
| Band 5 |  |
| Set the NM-37/57 BAND switch to $285-445 \mathrm{MHz}$ (Band 5) and adjust the Sweep Generator for a sweep from 280 to 450 MHz . Tune the NM-37/57 to 290, 340,390 , and 440 MHz and record the frequency meter indication. | Same as for Band 1. |
| Band 6 |  |
| Set the NM-37/57 BAND switch to $430-620 \mathrm{MHz}$ (Band 6) and adjust the Sweep Generator for a sweep from 430 to 630 MHz . <br> 500,560 , and 620 MHz and record the frequency meter indication. | Same as for Band 1. Tune the NM-37/57 to 440, |
| Band 7 |  |
| Set the NM-37/57 BAND switch to $600-825 \mathrm{MHz}$ (Band 7) and adjust the Sweep Generator for a sweep from 590 to 830 MHz . Tune the NM-37/57 to 600, $660,720,780$, and 820 MHz and record the frequency meter indication. | Same as for Band 1. |
| Band 8 |  |
| Set the NM-37/57 BAND switch to $800-1000 \mathrm{MHz}$ (Band 8) and adjust the Sweep Generator for a sweep from 800 to 1000 MHz . Tune the NM-37/57 to 800, 850, 900,950 , and 1000 MHz and record the frequency meter indication. | Same as for Band 1. |

Table 4-1. Minimum Performance Test Procedures (Continued)

|  | Procedure | Acceptable Indication |
| :---: | :---: | :---: |
| B. | NARROWBAND (CW) SIGNAL LEVEL |  |
|  | TRACKING ACCURACY TEST |  |
|  | Connect the output of Signal Generator (HP 608E) via Step Attenuator (HP 355D) to the RF INPUT receptacle of the NM-37/57. Set the Step Attenuator for 40 dB . Adjust the Signal Generator for a CW signal at 150 MHz at an output level of -27 dBm , yielding an RF input to the NM-37/57 of -67 dBm. Set the NM-37/57 BAND switch to Band 3, BANDWIDTH to 1.0 MHz , ATTENUATOR to 0 dB , AFC to OFF, and FUNCTION switch to FIELD INTENSITY. |  |
|  | Function Tracking Accuracy |  |
|  | Tune the NM-37/57 for maximum signal indication on the dB meter. Adjust the CALIBRATE control for a reference indication of 40 dB on the dB referred to $1 \mu \mathrm{~V}$ scale of the meter. | The dB meter indicates 40 $\pm 0.5 \mathrm{~dB}$ on the dB referred to $1 \mu \mathrm{~V}$ scale at each position of the FUNCTION Set the switch. | FUNCTION switch to QUASI-PEAK, then to each of the three PEAK positions, and record the dB meter indication at each position. Set the FUNCTION switch to SLIDEBACK PEAK. Rotate the SLIDEBACK PEAK control fully counterclockwise. Connect headphones to AUDIO jack, set AUDIO switch to AM, and adjust AUDIO GAIN control for sound level desired. Rotate SLIDEBACK PEAK control slowly clockwise until signal cuts off. Record the dB meter indication at this threshold level.

## Bandwidth Tracking Accuracy

Set the NM-37/57 FUNCTION switch to FIELD INTENSITY and BANDWIDTH to .01 MHz . Tune the receiver for maximum deflection on the dB meter using the FINE TUNE control, then set AFC switch ON. Set the BANDWIDTH switch to 0.1 MHz and 1.0 MHz . Record the dB meter indication on the dB referred to $1 \mu$ scale for each of the three bandwidths.

The dB meter indicates 40 $\pm 0.5 \mathrm{~dB}$ on the dB referred to $1 \mu \mathrm{~V}$ scale at each position of the BANDWIDTH switch.

Table 4-1. Minimum Performance Test Procedures (Continued)

| Procedure | Acceptable Indication |
| :---: | :---: |
| Attenuator Tracking Accuracy <br> Set the BANDWIDTH switch to 1.0 MHz . Adjust the Signal Generator and Step Attenuator as necessary to obtain the following signal levels at the RF INPUT connector of the NM-37/57. Set the NM-37/57 ATTENUATOR switch as given for each input signal level and record the dB meter indication. | The dB meter indicates 40 $\pm 0.5 \mathrm{~dB}$ on the dB referred to $1 \mu$ scale at each input signal level. |
| RF INPUT <br> Signal Level (dBm) ATTENUATOR <br> Switch Setting (dB) <br> -87 -20 <br> -67 0 <br> -47 +20 <br> -27 +40 <br> -7 +60 |  |
| Log IF Amplifier Tracking Accuracy |  |
| Set the NM-37/57 BANDWIDTH switch to 0 . 1 MHz and ATTENUATOR switch to +40 dB . Adjust the Signal Generator output to -7 dBm and set the Step Attenuator for 0 dB . Adjust the NM-37/57 CALIBRATE control to obtain full scale deflection ( 60 dB ) of the dB meter. Decrease the RF input level in 10 dB steps (use the Step Attenuator) to obtain the following input signal levels. Record the dB meter indication at each signal level. | The dB meter indicates the following values within $\pm 2$ dB at each signal level: |
| $\begin{gathered} \text { RF INPUT } \\ \text { Signal Level (dBm) } \end{gathered}$ | Meter Indication (dB Referred to $1 \mu \mathrm{~V}$ ) |
| $\begin{aligned} & -760 \\ & -17 \\ & -27 \\ & -37 \\ & -47 \\ & -57 \\ & -67 \end{aligned}$ | $\begin{aligned} & 50 \\ & 40 \\ & 30 \\ & 20 \\ & 10 \\ & 0 \end{aligned}$ |

Table 4-1. Minimum Performance Test Procedures (Continued)

|  | Procedure | Acceptable Indication |
| :---: | :---: | :---: |
| C. | BROADBAND (IMPULSE) SIGNAL LEVEL TRACKING ACCURACY TEST |  |
|  | Terminate the output of Impulse Generator (Singer Model 91263-1) with 10 dB Attenuator (Singer Model 90530-10) furnished with the Impulse Generator. |  |
|  | CAUTION |  |
|  | The Impulse Generator output may damage external low-power attenuators if Attenuator Model 90530-10 is not used. |  |
|  | Connect output of 10 dB Attenuator via Step Attenuator (HP 355D) to the RF INPUT receptacle of the NM-37/57. Set the Step Attenuator for 20 dB . Set the NM-37/57 BAND switch to Band 3, BANDWIDTH to 1.0 MHz , AFC to OFF, and ATTENUATOR to 0 dB . Tune receiver near center of frequency band. |  |
|  | Function Tracking Accuracy |  |
|  | Adjust the spectral output of the Impulse Generator to obtain the signal levels listed below at the RF INPUT connector of the NM-37/57, compensating for loss | The dB meter indicates the RF input signal level within +3 dB on the dB referred to $1 \mu \mathrm{~V}$ scale. |

Table 4-1. Minimum Performance Test Procedures (Continued)


## D. CALIBRATION DATA ACCURACY TEST

Connect the output of Signal Generator (HP 608E) via Step Attenuator (HP 355D) to the NM-37/57 RF INPUT receptacle. Set the Step Attenuator for 20 dB . Adjust the Signal Generator for a CW signal at 31 MHz at an output level of -27 dBm , yielding a signal level of -47 dBm at the NM-37/57 input. Set the NM-37/57 ATTENUATOR switch at 0 dB , BANDWIDTH to 1.0 MHz . AFC to OFF, and FUNCTION switch to FIELD INTENSITY.

The dB meter indicates within +3 dB of the values given for each bandwidth in either DP or SP function:

40
.01

Table 4-1. Minimum Performance Test Procedures (Continued)


Table 4-1. Minimum Performance Test Procedures (Continued)


Table 4-1. Minimum Performance Test Procedures (Continued)


Table 4-1. Minimum Performance Test Procedures (Continued)

| Procedure | Acceptable Indication |
| :--- | :---: |

Turn on the Impulse Generator and adjust for minimum output, then increase the output to obtain an indication on the dB meter 3 dB above the receiver noise level. Record the impulse signal amplitude at the RF INPUT jack (Impulse Generator output less attenuators) as the impulse sensitivity in $\mathrm{dB} \mu \mathrm{V} / \mathrm{MHz}$.

## Bands 2 through 8

Follow the procedure given for Band 1 and test Bands 2 through 8, selecting a test frequency near the low end of each band. Determine and record the impulse sensitivity for each band.

## H. UNDESIRED RESPONSE REJECTION TEST

Connect and adjust Sweep Generator, Oscilloscope, and the NM-37/57 as described in Test A. Adjust the Sweep Generator to obtain a signal level at the RF INPUT connector of the NM-37/57 that is 60 dB above the narrowband sensitivity figure for Band 1 (recorded in Test F).

Spurious Response Rejection Slowly tune the receiver across Band 1 and observe any spurious responses on the Oscilloscope. If a spurious response occurs, measure the narrowband (CW) sensitivity of the NM-37/57 (as instructed in Test $F$ ) at the frequency to which the receiver is tuned. Then, set the CW Signal Generator to the spurious response frequency and increase the signal output until the dB meter indicates 3 dB above the receiver noise level. Note the signal level (at the spurious response frequency) in dBm at the RF INPUT jack. Record the difference between this signal level and the narrowband sensitivity figure as the spurious response rejection figure in dB .

The broadband (impulse) sensitivity is equal to or greater than the following:

Bands 1 thru 3: $+15 \mathrm{~dB} \mu \mathrm{~V} / \mathrm{MHz}$
Bands 4 thru 8: $+20 \mathrm{~dB} \mu \mathrm{~V} / \mathrm{MHz}$

The optimum indication is that no undesired responses are observed when sweeping each band with a signal that is 60 dB above the narrowband sensitivity figure for that band. For observed responses, the measured spurious rejection shall be 60 dB minimum, except in Band 1 from 39 to 43 MHz (near twice the 20.5 MHz IF). In this region the spurious response rejection shall be 40 dB minimum.

Table 4-1. Minimum Performance Test Procedures (Continued)

| Procedure | Acceptable Indication |
| :---: | :---: |

Repeat the procedure for Bands 2 through 8 , adjusting the frequency range of the Sweep Generator as necessary to cover each band. Set the sweep signal level at the RF INPUT connector for 60 dB above the narrowband sensitivity figure (recorded in Test F) for the band selected.

## IF Rejection

Set the NM-37/57 BAND switch to Band 1. Adjust the Sweep Generator to cover Band 1, but extend the sweep range down to 20 MHz . Tune the NM-37/57 at the low end of the band and observe the 20.5 MHz IF response on the Oscilloscope.

Set the BAND switch to Band 4. Adjust the Sweep Generator to sweep Band 4, but extend the sweep range down to 150 MHz . Tune the NM-37/57 at the low end of the band and observe the 160 MHz IF response on the Oscilloscope.

Follow the same procedure as for measuring spurious response rejection and determine the IF rejection on Bands 1 and 4. (The maximum IF response occurs on Bands 1 and 4.)

## Image Rejection

Set the NM-37/57 BAND switch to Band 3. Adjust the Sweep Generator to cover Band 3 , but extend the sweep range up to 240 MHz . Tune the NM-37/57 at the high end of the band and observe the image response on the Oscilloscope.

Set the BAND switch to Band 8. Adjust the Sweep Generator to sweep Band 8, but extend the frequency range up to 1400 MHz . Tune the NM-37/57 at the high end of the band and observe the image response on the Oscilloscope.
Follow the same procedure as for measuring spurious response rejection and determine the image rejection on Bands 3 and 8 .

The rejection of the 20.5 MHz IF and the 160 MHz IF shall be 60 dB minimum.

The image rejection shall be 60 dB minimum.

Table 4-1. Minimum Performance Test Procedures (Continued)

| Procedure | Acceptable Indication |
| :---: | :---: |

## I. INPUT VSWR TEST

Connect the horizontal and vertical outputs of Sweep Generator (Wavetek Model 2001) to the corresponding inputs of Oscilloscope (Tektronix 535A). Connect the RF output of the Sweep Generator to the RF IN jack of VSWR Bridge (Telonic TRB-3). Terminate the Z 1 jack of the VSWR Bridge with 50 ohms. Connect the Z2 jack of the VSWR Bridge to the RF INPUT connector on the NM-37/57. Connect the DETECTOR OUTPUT jack of the VSWR Bridge to the DEMOD IN jack of the Sweep Generator. Adjust the Sweep Generator for sweep range from 30 to 60 MHz at an output level of 0 dBm and turn on the 10 MHz and 50 MHz markers. Adjust the Oscilloscope horizontal gain to display the full sweep range, and the vertical gain for $5 \mathrm{mV} / \mathrm{cm}$. Set the NM-37/57 controls as specified in Paragraph 4.2. 2

## $B$ and 1

Establish references on the Oscilloscope by disconnecting the NM-37/57 from the VSWR Bridge at jack Z2 and terminating Z2 with 1.2:1 and then 1.5:1 standard mismatches. Remove the mismatch and reconnect the NM-37/57 to Z2. Slowly tune the NM-37/57 across the band and observe the VSWR on the Oscilloscope.

## Bands 2 and 3

Follow the procedure given for Band 1 and test Bands 2 and 3 , adjusting the Sweep Generator frequency range as necessary to cover each band.

## Bands 4 through 8

Follow the procedure given for Band 1 and test Bands 4 through 8, except establish references on the Oscilloscope using 1.2:1 and 2.0:1 standard mismatches. Adjust the Sweep Generator frequency range as necessary to cover each band.

The maximum RF input VSWR shall be as follows:

Bands 1 thru 3: 1.5:1
Bands 4 thru 8: 2.0:1

Table 4-1. Minimum Performance Test Procedures (Continued)

|  | Procedure |  |
| :--- | :--- | :---: |
| J. | FM VIDEO OUTPUT AND AFC OPERATION |  |
|  | $\underline{\text { TEST }}$ |  |

Connect and adjust Sweep Generator, Oscilloscope, and NM-37/57 as described in Test A. Adjust the Sweep Generator for an output signal level of -47 dBm at a center frequency of 150 MHz . Set the sweep width for 2 MHz (from 149 to 151 MHz ) using the 1 MHz markers. Set the NM-37/57 BAND switch to Band 3, BANDWIDTH to 1.0 MHz , ATTENUATOR to 0 dB, AFC to OFF, and FUNCTION selector to PEAK/. 05 SEC HOLD.

## FM Video Output

Tune the NM-37/57 to obtain maximum indication on the dB meter. Adjust the horizontal gain of the Oscilloscope for $200 \mathrm{kHz} / \mathrm{cm}$ and the vertical gain for $0.2 \mathrm{~V} / \mathrm{cm}$. Adjust the NM-37/57 FINE TUNE control to obtain IF response curve in the center of the display. Change the video input to the Sweep Generator from the NM-37/57 LOG VIDEO output connector to the FM VIDEO output connector. Set the vertical gain of the Oscilloscope for $0.5 \mathrm{~V} / \mathrm{cm}$ and observe the amplitude of the FM discriminator curve. Reduce the RF input signal level to the NM-37/57 from -47 dBm to -97 dBm and note any change in the discriminator curve amplitude.

Adjust the Sweep Generator for an output signal level of -67 dBm . Set the NM-37/57 BANDWIDTH switch to 0.1 MHz and observe the change in amplitude of the FM discriminator curve.

## AFC Operation

Adjust the Sweep Generator for a 150 MHz CW signal at an input level of -67 dBm to the RF INPUT receptacle of the NM-37/57. Set the NM-37/57 BANDWIDTH switch to 0.1 MHz , AFC to OFF, and FUNCTION

The peak-to-peak amplitude of the discriminator curve output at the FM VIDEO connector does not change when the FM input signal level is varied from -47 dBm to -97 dBm . Nominal peak-to-peak amplitude of the discriminator curve is 2 volts (from -1 to +1 volt).

The peak-to-peak amplitude of the FM discriminator curve drops to one-half of the previous value.

Table 4-1. Minimum Performance Test Procedures (Continued)

| Procedure | Acceptable Indication |
| :--- | :--- |
| switch to QUASI-PEAK. Tune the receiver |  |
| for maximum indication on the dB meter. |  |
| Set the AFC switch to ON and observe that | The dB meter indication |
| the dB meter indication does not change. | remains peaked when AFC |
| Rotate the FINE TUNE control approxi- | is switched on and does not |
| mately $1 / 4$ turn in each direction and | change when FINE TUNE |
| observe the dB meter indication. | control is rotated. |
| Set the AFC switch OFF and readjust the | The dB meter indication |
| FINE TUNE control for peak dB meter | does not change when |
| indication. Set the AFC switch ON and | receiver bandwidth is |
| observe that the dB meter indication does | reduced to 10 kHz. |

## K. SIGNAL OUTPUT TEST

Connect the RF output of Sweep Generator (Wavetek Model 2001) via Step Attenuator (HP 355D) to the RF INPUT receptacle of the NM-37/57. Set the Step Attenuator for 40 dB . Connect the LINEAR VIDEO output receptacle (rear panel) of the NM-37/57 to the vertical input of Oscilloscope. Adjust the Sweep Generator for a 150 MHz CW signal with 1 kHz square wave modulation at a signal level of -47 dBm at the RF input of the NM-37/57. Set the NM-37/57 ATTENUATOR switch to 0 dB , BAND switch to Band 3, BANDWIDTH to 0. 1 $\mathrm{MHz}, \mathrm{AFC}$ to OFF, and FUNCTION selector to QUASI-PEAK.

## Linear Video and Audio Output

Tune the NM-37/57 for full-scale deflection of the dB meter. Note the amplitude of the demodulated 1 kHz square wave displayed on the Oscilloscope. Connect a set of headphones to the AUDIO jack of the NM-37/57 and adjust the AUDIO GAIN control for desired sound level of the 1 kHz tone.

Table 4-1. Minimum Performance Test Procedures (Continued)

| Procedure | Acceptable Indication |
| :---: | :---: |

Decrease the signal level at the RF input of the NM-37/57 from - 47 dBm to -87 dBm and note the amplitude change of the linear video output on the oscilloscope and the sound volume in the headphones.

Cut off the 1 kHz square wave modulation at the Sweep Generator and adjust the signal level at the RF input of the NM-37/57 to -47 dBm . Set the FUNCTION switch to BFO and note that tone is audible in headphones. Rotate FINE TUNE control and note change in the audio tone. Decrease the RF input level to -87 dBm and note change in the audio output level.

## IF Output

Adjust the level of the 150 MHz CW signal at the RF input of the NM-37/57 to -47 dBm . Set the FUNCTION switch to QUASIPEAK and tune the receiver for full-scale deflection of the dB meter. Connect a 50 -ohm load to the IF OUTPUT receptacle (rear panel). Connect an RF Millivoltmeter (HP 411A) across the 50 -ohm load and measure the amplitude of the IF output.

## Log Video Output

Remove the 50 -ohm load from the IF OUTPUT receptacle and connect to the LOG VIDEO output receptacle on the NM-37/57 rear panel. Connect a Digital Voltmeter (HP 3440A) across the 50 ohm load and measure the DC amplitude of the log video output.

## Y Output

Connect a 1 kilohm load to the Y OUTPUT receptacle on the rear panel of the NM-37/57. Connect the Digital Voltmeter across the 1 kilohm load and measure the DC amplitude of the Y output.

The amplitude of the square wave at the LINEAR VIDEO output receptacle and the sound volume of the 1 kHz audio output does not decrease more than 6 dB .

The BFO tone is approximately 1 kHz with the pitch changing as the FINE TUNE control is rotated. The BFO tone does not drop out when signal level is reduced to -87 dBm .

The voltage at the IF OUTPUT receptacle is at least 20 millivolts RMS across 50 ohms.

The voltage at the LOG VIDEO receptacle is +300 $\pm 10 \mathrm{mV}$ DC across 50 ohms.

The voltage at the Y OUT-
PUT receptacle is +1 V $\pm 10 \mathrm{mV}$ DC.

Table 4-1. Minimum Performance Test Procedures (Continued)

|  | Procedure | Acceptable Indication |
| :---: | :---: | :---: |
|  | X Output |  |
|  | Remove the 1 kilohm load from the $Y$ OUTPUT receptacle and connect to the X OUTPUT receptacle on the NM-37/57 rear panel. Rotate the TUNE control fully clockwise to obtain full-scale indication on the frequency meter. Connect the Digital Voltmeter across the 1 kilohm load and measure the DC amplitude of the X output. | The voltage at the X OUTPUT receptacle is +1 V $\pm 10 \mathrm{mV}$ DC. |
| L. | REMOTE CONTROL AND AUTOMATIC SCAN OPERATION TEST |  |
|  | Use the same equipment setup as in previous test (Test K). Connect a Remote Controller to the PROGRAMMER receptacle on the rear panel of the NM-37/57 and set the CONTROL MODE switch to REMOTE. |  |
|  | Remote Control Operation |  |
|  | Check the operation of remote band selection, bandwidth selection, receiver tuning, function selection, and adjustment of receiver gain (calibration). same as local operation. | The remote control of band selection, bandwidth selection, tuning, function selection, and calibration is the |
|  | Automatic Scan Operation |  |
|  | Set the NM-37/57 CONTROL MODE switch to the SCAN position. Momentarily press the SINGLE switch and observe the indication on the frequency meter. | The frequency meter indicates a smooth scan from low end to full scale in approximately one minute, then returns to low end of scale. |
|  | Connect an ohmmeter across the RECORDER PENLIFT connector on the rear panel of the NM-37/57. Momentarily press the SINGLE switch and observe the ohmmeter indication. | The ohmmeter initially indicates an open circuit, then indicates a short circuit during the one-minute scan period, then again indicates an open circuit. |

Table 4-1. Minimum Performance Test Procedures (Continued)

|  | Procedure | Acceptable Indication |
| :---: | :---: | :---: |
| M. | BATTERY OPERATION TEST |  |
|  | Use the same equipment setup as in previous test (Test L). Set the NM-37/57 FUNCTION switch to FIELD INTENSITY, CONTROL MODE to LOCAL, ATTENUATOR to 0 dB , BAND switch to Band 3, BANDWIDTH to 0.1 MHz , and AFC to OFF. |  |
|  | Set the POWER switch to BATT TEST. Set the BATT TEST switch to each polarity and check condition of batteries. | Fully charged batteries cause dB meter to indicate in FULL zone of BATTERY scale. |
|  | Set the POWER switch back to ON AC and tune receiver for maximum indication on the dB meter. Set the POWER switch to ON BATT and observe dB meter indication. | The signal level indication on the dB meter remains unchanged. |
|  | Check the operation of all controls using the internal batteries as power source, or repeat Tests A through K with POWER switch set at ON BATT. | Performance of the NM-37/57 when operating with internal batteries is the same as when using an AC power source. |

### 4.3 DISASSEMBLY PROCEDURES

Removal of four cover panels from the NM-37/57 provides across to the sub-assemblies for alignment and maintenance. The battery pack located at the rear of the instrument may be removed without removing the cover panels. Refer to the illustrations in Section VI for identification of subassemblies.

## 4. 3.1 Removal of Cover Panels

Each of the two side cover panels is held by four No. 4 flat-head screws that are externally accessible. The top and bottom cover panels are each held by ten No. 10 socket-head cap screws that are accessible after removal of the side cover panels.

Proceed as follows:
a. Remove four 4-40 $\times 3 / 8$ flat-head screws that secure each side cover panel.
b. Remove the side cover panels, exposing the side frames. The socket-head cap screws holding the top and bottom cover panels are now accessible.
c. Remove twenty $10-32 \times 3 / 4$ socket-head cap screws that secure the top and bottom cover panels to the side frames.
d. Remove the top and bottom cover panels from the NM-37/57. Use care not to damage the RF gaskets mounted in recesses on the interior surface of the panels.

### 4.3. 2 Removal of Battery Pack

The battery pack is mounted above the rear connector panel and is removed as follows:
a. Remove four $8-32 \times 1 / 4$ screws and lockwashers that secure the battery pack to the side frames.
b. Support the battery pack and pull out from the rear far enough to gain access to the battery pack cable connector.
c. Disconnect the battery pack cable and remove battery pack from the instrument.

### 4.3.3 Removal of Subassemblies

The plug-in shielded modules are held in place by two retaining brackets mounted across the top of the modules. Remove the eight screws that secure the brackets and the modules may then be pulled out from the chassis connectors and the coaxial cable disconnected.

The remainder of the subassemblies are accessible from the top or bottom of the instrument and require no special instructions for removal.

## CAUTION

If a fault has been isolated to the turret attenuator assembly, DO NOT attempt to remove the entire turret assembly. The only repairable components are the removable attenuators.

For turret attenuator assembly attenuator removal, proceed as follows:

1. Position the instrument to make the underside easily accessible.
2. Locate A45 (Turret Attenuator). (See Page 6-3.)
3. Rotate the attenuator switch until a small Phillip' s-head screw is visible.
4. Loosen the screw.
5. Rotate the attenuator switch until a second Phillip's-head screw is visible.
6. Loosen the screw.
7. Rotate the attenuator switch until the faulty attenuator is on the bottom of the attenuator assembly.
8. Slide the attenuator collar as far forward as possible.
9. Slide the bottom of the attenuators retainer spring forward until the spring is free of the faulty attenuator.
10. Slide the faulty attenuator down and away from the turret attenuator assembly.
11. For reassembly, perform Steps 1 thru 10 in the reverse order.

### 4.4 MAINTENANCE AND ALIGNMENT OF POWER SUPPLY SECTION

The following test equipment (or equivalent) is required for maintenance and alignment of the power supply section:
AC Voltmeter, HP 3400A
Clip-On Milliammeter, HP 428B
Digital Voltmeter, HP 3440A
Oscilloscope, Tektronix 535A

### 4.4. 1 Check and Alignment of Rectifier-Charge Regulator A32

a. Set the $115 / 230 \mathrm{~V}$ switch on the rear panel of the NM-37/57 to 115 V .
b. Connect the NM-37/57 to $115+2 \mathrm{~V}, 60 \mathrm{~Hz}$ power source and set the POWER switch to ON AC.
c. Measure the secondary voltage from the power transformer between pins 6 and 7, and between pins 12 and 13 of rectifier-charge regulator A32 with an AC Voltmeter. The voltage should be 23 to 24 volts RMS with the line voltage specified in step b applied to the NM-37/57.
d. Measure the positive rectifier output voltage from A32 pin 5 to ground with a Digital Voltmeter. The voltage should be +27 to +28 V . Measure the negative rectifier output voltage from A32 pin 14 to ground. The voltage should be -27 to -28 V .
e. Measure the positive unregulated output voltage from A32 pin 4 to ground with the Digital Voltmeter. The voltage should be $+20+1 \mathrm{~V}$. Measure the negative unregulated output voltage from A32 pin 15 to ground. The volt-age should be $-20+1 \mathrm{~V}$.
f. Connect a Clip-On Milliammeter over the red wire connected to A32 pin 1 and measure the trickle charge current to the positive battery. The trickle charge current should be $120+12$ milliamperes.
g. Set the POWER switch to CHARGE and measure the charge current to the positive battery. Adjust R9 on A32 as necessary to obtain $300 \pm 30$ milliamperes.
h. Connect the Clip-On Milliammeter over the white wire connected to A32 pin 18 and measure the charge current to the negative battery. Adjust R10 on A32 to obtain $300+30$ milliamperes.
i. Set the POWER switch to ON AC and check that the trickle charge current to the negative battery is $120 \pm 12$ milliamperes.
j. Set the POWER switch to CHARGE and the BATT TEST switch to +. Connect the Digital Voltmeter to A32 pin 1 and measure the positive battery charge voltage. With fully charged batteries, the voltage at pin 1 should be 19.5 to 20.2 V and the dB meter should indicate in the FULL zone of the battery scale (full scale $=$ 20.2 V ). Adjust R14 on A32 as necessary to obtain FULL indication on the dB meter.
k. Set the BATT TEST switch at -. Connect the Digital Voltmeter to A32 pin 18 and measure the negative battery charge voltage. With fully charged batteries the voltage at pin 18 should be -19.5 to -20.2 V and the dB meter should indicate in the FULL zone of the battery scale.

### 4.4. 2 Battery Maintenance

## NOTE

Refer to Appendix A for supplementary battery information.
a. Set the POWER switch to BATT TEST. Set the BATT TEST toggle switch to + and - , observing the dB meter indication on the battery scale. The meter indicates the battery condition during discharge with a test load.
b. If there is no indication on the dB meter for either the positive or negative battery test in step a, press the appropriate circuit breaker button on the rear panel to reset. If there is still no indication, remove the battery pack as instructed in Paragraph 4.3.2 and check the battery cable and connector.
c. If the batteries are discharged and the NM-37/57 is not required to operate, connect the instrument to an AC power source and set the POWER switch to CHARGE. Completely discharged batteries will be fully charged in approximately 12 hours.
d. If the batteries are discharged but the NM-37/57 is required for use, the trickle charge during AC operation will require approximately 30 hours to charge completely discharged batteries.

## 4. 4.3 Alignment of Voltage Regulator A31

a. Set the POWER switch at ON AC.
b. Using the Digital Voltmeter, check that the positive unregulated input volt-age at A31 pin 3 is $+20+1 \mathrm{~V}$ and the negative unregulated input voltage at A31 pin 16 is $-20 \pm 1 \mathrm{~V}$.
c. Measure the positive regulated voltage output at A31 pin 1 with the Digital Voltmeter and adjust R18 as necessary to obtain $+12 \mathrm{~V}+10 \mathrm{mV}$.
d. Measure the negative regulated voltage output at A 31 pin 18 and adjust R 19 to obtain $-12 \mathrm{~V}+10 \mathrm{mV}$.

## NOTE

There is interaction between adjustments of R18 and R19. Repeat steps c and d as necessary to obtain correct values without further adjustment.
e. The nominal DC voltage levels of the voltage regulator integrated circuits and transistors as measured to ground with the Digital Voltmeter under normal operating conditions are listed for reference (values are in volts):

|  |  | Pins 1 and 2 |  | Pin 3 |  | Pin 4 |  | Pin 5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AR1: |  | +6.4 |  | +12.0 |  | 0 |  | +5.6 |
| AR2: |  | -6.0 |  | 0 |  | -12.0 |  | -7.3 |
|  | Q1 | Q2 | Q3 | Q4 | Q5 | Q6 | Q7 | Q8 |
| $\begin{aligned} & \mathrm{V}_{\mathrm{E}} \\ & \mathrm{~V}_{\mathrm{B}} \\ & \mathrm{~V}_{\mathrm{C}} \end{aligned}$ | +12.3 | -12.3 | +12.9 | -13.0 | +4.6 | -8.3 | +12.0 | -12.0 |
|  | +12.9 | -13.0 | +13.5 | -13.6 | +5.3 | -7.6 | +12.3 | -12.3 |
|  | +20.0 | -20.0 | +20.0 | -20.0 | +12.9 | 0 | +13.5 | -13.6 |

### 4.4.4 Adjustment and Maintenance of DC/DC Converter A16.

Use extender cable and remove module cover for access to test points.
a. Measure the output voltage of the DC/DC converter at feedthrough capacitor C1 (accessible from the bottom of the power supply section) with a Digital Voltmeter. Adjust R4 on A16 to obtain $+100 \pm 5 \mathrm{~V}$.
b. Observe the square wave at TP3 of A16 with an Oscilloscope. The nominal peak-to-peak amplitude of the square wave is 50 V , and the frequency should be approximately 5 kHz .
c. The nominal DC voltage levels of the DC/DC converter transistors as measured to ground with the Digital Voltmeter under normal operating conditions are listed for reference (values are in volts):

|  | $\underline{\text { Q1 }}$ | $\underline{\text { Q2 }}$ | $\underline{\text { Q3 }}$ | $\underline{\text { Q4 and Q5 }}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{E}:}$ | +6.3 | -12.8 | +6.0 | -19.0 |
| $\mathrm{~V}_{\mathrm{B}:}$ | +6.9 | -12.2 | +6.3 | -18.3 |
| $\mathrm{~V}_{\mathrm{C}:}$ | +19.0 | +6.9 | +6.9 | +6.0 |

### 4.5 MAINTENANCE AND ALIGNMENT OF VIDEO SECTION

The following test equipment (or equivalent) is required for maintenance and alignment of the video section of the NM37/57:

Signal Generator, HP 608E
Digital Voltmeter, HP 3440A
Step Attenuator (1 dB per step), HP 355C
Oscilloscope, Tektronix 535A
VTVM, Ballentine 861

### 4.5.1 Preliminary Procedures

Refer to Figure 4-1 and proceed as follows:
a. Disconnect the T-adapter at OUTPUT connector J2 of bandwidth selector A14, leaving cables W32 and W33 connected to the T -adapter.
b. Connect a BNC T-adapter to IF INPUT connector J1 of log IF amplifier A41. Reconnect cable W33 to the Tadapter, and connect the output of Signal Generator (HP 608E) to the T-adapter via Step Attenuator (HP 355C).


Figure 4-1. Test Equipment Setup for Video Section Alignment
c. Connect a BNC T-adapter to VIDEO OUT connector J3 of log IF amplifier A41. Reconnect cable W19 to the T-adapter, and connect Digital Voltmeter (HP 3440A) to the T-adapter.
d. Set the Step Attenuator for 0 dB .
e. Adjust the Signal Generator for an output level of 50 mV at 20.5 MHz . The Digital Voltmeter should indicate approximately +3.6 V at the video output of the log IF amplifier. Readjust the Signal Generator output level until the Digital Voltmeter indicates $+3.60+0.01 \mathrm{~V}$.

### 4.5.2 Check and Alignment of Direct Peak Circuit A22

Perform the preliminary procedures given in Paragraph 4.5.1 and proceed as follows:

## Signal Response Test

a. Set the FUNCTION switch at PEAK/. 05 SEC HOLD. Measure the DC signal level at TP1 and TP4 of direct peak circuit A22 with the Digital Volt-meter. The signal level should be $+3.60 \pm 0$. 02 V at both test points.
b. Check that the signal level at A22 TP1 and TP4 is +3.600 .02 V with the FUNCTION switch set at PEAK/0. 3 SEC HOLD and PEAK/3. 0 SEC HOLD positions.

## Hold-and-Dump Circuit Check

c. Set the FUNCTION switch to PEAK/. 05 SEC HOLD. Adjust output of the Signal Generator to obtain approximately mid-scale deflection of the dB meter.
d. Remove input signal by disconnecting Signal Generator output cable and observe that the dB meter indication drops immediately (within 50 milliseconds) to zero.
e. Set the FUNCTION switch to PEAK/0. 3 SEC HOLD. Reconnect the Signal Generator to obtain mid-scale deflection of the dB meter.
f. Repeat step d , observing that the dB meter indication drops to zero after 0.3 seconds.
g. Repeat step e, but set the FUNCTION switch at PEAK/3. 0 SEC HOLD.
h. Repeat step d , observing that the dB meter drops to zero after 3 seconds.
i. Reconnect the Signal Generator to obtain mid-scale deflection of the dB meter and note the value on the dB scale.

## Dumping Sensitivity

j. Set the Step Attenuator for 2 dB and observe that the dB meter indication drops 2 dB after the selected hold time has elapsed.
k. Set the Step Attenuator back to 0 dB and note that the dB meter indication increases 2 dB .
I. Set the Step Attenuator for 1 dB insertion loss and observe that the Db meter indication remains the same after the selected hold time has elapsed
m . Meeting the requirements of steps $\mathrm{j}, \mathrm{k}$, and 1 determines that the dumping sensitivity is greater than 1 dB but less than 2 dB . If not, adjust R16 on A22 until the requirements are satisfied.
n. The nominal DC voltage levels of the integrated circuits and transistors on A22 as measured to ground with the Digital Voltmeter are listed for reference (values are in volts). Set the FUNCTION switch at PEAK/. 03 SEC HOLD and remove signal input.

| Pin 2 |  | Pin 3 | Pin 4 | Pin 6 | Pin 7 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR1: AR2: | $\begin{gathered} 0 \\ -0.15 \end{gathered}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & -12 \\ & -12 \end{aligned}$ | $\begin{array}{r} -10 \\ +11 \end{array}$ | $\begin{aligned} & +12 \\ & +12 \end{aligned}$ |
|  | Q1 | Q2 | Q3 | Q5 | Q7 |
| $V_{E}$ | -0.7 | -0.7 | +9.1 | 0 | 0 |
| B: | 0 | 0 | +8.8 | 0 | +0.65 |
| ${ }^{\text {C }}$ | +8.8 | +11.7 | 0 | +0.15 | 0 |
|  |  |  |  |  | Q8 |
| $\mathrm{V}_{\mathrm{s}}$ |  |  |  | $V_{E}$ | 0 |
| $\mathrm{V}_{\mathrm{G}}$ : |  |  |  | $V_{B 1}$ | 0 |
| $V_{\mathrm{D}}$ |  |  |  | $V_{B}$ : | +12 |

### 4.5.3 Check and Alignment of Slideback Peak Circuit A23

Perform the preliminary procedures given in Paragraph 4.5.1, ełcept in step d set the Step Attenuator for 1 dB . Proceed as follows:
a. Set the FUNCTION switch to SLIDEBACK PEAK, the AUDIO switch to AM, and rotate the AUDIO GAIN control to mid-position.
b. Connect a set of headphones to the AUDIO jack and rotate the SLIDEBACK PEAK control fully counterclockwise. An 800 Hz tone will be audible in the headphones. Adjust the AUDIO GAIN control as necessary to obtain a convenient sound level.
c. Observe the signal at TP3 on slideback peak circuit A23 with an Oscilloscope. The multivibrator output should be a square wave with a nominal peak-to-peak amplitude of 10 V at a frequency of approximately 800 Hz .
d. Connect the Digital Voltmeter to TP1 of slideback peak circuit A23. Rotate the SLIDEBACK PEAK control slowly clockwise until the audio tone in the headphones cuts off. The voltage at TP1 should be $+3.60+0.01$ V at this threshold level.
e. Connect the Digital Voltmeter to TP4 on A23. The signal level at TP4 should also be $+2.0+0.01 \mathrm{~V}$. If necessary, adjust R26 on A23 to obtain this value.
f. Increase the input signal level 1 dB by removing 1 dB from the Step Attenuator. Without changing the SLIDEBACK PEAK control setting, the volt-age at TP1 should remain unchanged, but the voltage at TP4 should rise approximately 0.3 V and the audio tone should be audible in the headphones.
g. The nominal DC voltage levels of the integrated circuits and transistors on A23 as measured to ground with the Digital Voltmeter are listed for reference (values are in volts). Set the FUNCTION switch at SLIDEBACK PEAK and rotate the SLIDEBACK PEAK control fully clockwise.

| AR1: | Pins 2 and 3 | Pin 4 | Pin 6 | Pin 7 |
| :---: | :---: | :---: | :---: | :---: |
|  | +0.7 | -12 | +2.4 | +12 |
| $\begin{aligned} & \mathrm{V}_{\mathrm{E}} \\ & \mathrm{~V}_{\mathrm{B}} \\ & \mathrm{~V}_{\mathrm{C}} \end{aligned}$ | Q1 | Q2 | Q3 | Q4 |
|  | +4.1 | +3.9 | +3.9 | +8.8 |
|  | +4.8 | +4.1 | 0 | +12 |
|  | +7.6 | +11.1 | +12 | -0.4 |
| $\begin{aligned} & \mathrm{V}_{\mathrm{E}} \\ & \mathrm{~V}_{\mathrm{B}} \\ & \mathrm{~V}_{\mathrm{C}} \end{aligned}$ | Q5 | Q6 | Q7 | Q8 |
|  | 0 | 0 | +11.5 | 0 |
|  | -0.5 | 0 | +11.9 | +0.7 |
|  | +12 | +11.5 | +12 | +0.1 |

## 4. 5.4 Alignment of Weighting and Meter Amplifier A21

Perform the preliminary procedures in Paragraph 4.5.1 and proceed as follows:
a. Set the FUNCTION switch to the FIELD INTENSITY position.
b. Connect the Digital Voltmeter to TP1 on weighting and meter amplifier A21. Adjust R21 on A21 to obtain $+3.60 \pm 0.01 \mathrm{~V}$ at TP1.
c. Set the FUNCTION switch at the QUASI-PEAK position.
d. Connect the Digital Voltmeter to TPZ on A21 and adjust RZZ to obtain $+3.60 \pm 0.01 \mathrm{~V}$ at TP2.
e. Set the FUNCTION switch to FIELD INTENSITY.
f. Connect the Digital Voltmeter to the video output of the log IF amplifier (at the BNC T-adapter) and adjust the Signal Generator to obtain $+0.60 \pm 0.01 \mathrm{~V}$ indication on the Digital Voltmeter.
g. Connect the Digital Voltmeter to TP3 on A21. Adjust R11 on A21 to obtain $0.00 \pm 0.01 \mathrm{~V}$ at TP3.
h. Connect the Digital Voltmeter to the video output of the log IF amplifier and adjust the Signal Generator output to obtain $+3.60 \pm 0.01 \mathrm{~V}$.
i. Connect the Digital Voltmeter to TP3 on AZ21 and adjust R13 to obtain $+3.00 \pm 0.01 \mathrm{~V}$ at TP3.

## NOTE

There is interaction between adjustments of R11 and R13. Repeat steps $\mathrm{g}, \mathrm{h}$, and i as necessary to obtain correct voltages at TP3 without further adjustment.
j . To check the mechanical zeroing of the dB meter, set the POWER switch at OFF. If necessary, adjust the mechanical zero of the meter through the access hole on the front panel. Set the POWER switch to ON AC.
k. With $+3.00 \pm 0.01 \mathrm{~V}$ at TP3 of A 21 , observe that the indication on the dB meter is exactly 60 dB . If not, adjust R17 on A21 to obtain 60 dB .
I. Set the FUNCTION switch sequentially to all positions and observe that the signal level at TP3 of A21 is $+3.00 \pm 0.01 \mathrm{~V}$ at each position.
m . Connect a 1 kilohm load resistor to the Y OUTPUT receptacle on the rear panel and measure the output voltage with the Digital Voltmeter. Adjust R19 on A21, if necessary, to obtain $+1.000 \mathrm{~V} \pm 5 \mathrm{mV}$. Remove the 1 kilohm load and observe that the Y output voltage rises to $+2.00 \pm 0.02 \mathrm{~V}$.

### 4.5.5 Alignment of Remote Function Selector A25

Perform the preliminary procedures given in Paragraph 4.5.1 Ind proceed as follows:
a. Set the FUNCTION switch at PEAK/0.3 SEC HOLD. Connect the Digital Voltmeter to TP1 on remote function selector A25.
b. Adjust R5 to obtain $+3.00+0.01 \mathrm{~V}$ at TP1.
c. Connect the Digital Voltmeter to pin $\underline{k}$ of the PROGRAMMER receptacle on the rear panel of the NM-37/57. Observe that the voltage is $+2.00+0.01 \mathrm{~V}$.

### 4.5.6 Alignment of dB Readout and Audio Amplifier A24 on Serial Number 205 and Below

Perform the alignment procedures for weighting and meter amplifier A21 given in Paragraph 4.5.4 and proceed as follows:
a. Set the FUNCTION switch to FIELD INTENSITY and set the ATTENUATOR switch to the -20 dB position. Reduce the output of the Signal Generator to obtain 0 dB on the NM-37/57 dB meter.
b. Using the Digital Voltmeter, check that the voltage at TP1 on A24 is 0.00 V . If not, connect a short from TP1 to ground before proceeding.
c. Connect the Digital Voltmeter to TP2 on A24. Adjust R5 on A24 to obtain - 20 mV at TP2.
d. Set the ATTENUATOR Switch to the positions indicated and adjust the corresponding control on A24 to obtain the correct voltage at TP2:

| ATTENUATOR <br> Switch Position | Control <br> on A24 | Voltage <br> at TP2 |
| :---: | :---: | :---: |
| 0 dB | R3 | 0.0 mV |
| +20 dB | R7 | +20 mV |
| +40 dB | R10 | +40 mV |
| +60 dB | R 12 | +60 mV |

e. Set the ATTENUATOR switch to 0 dB and remove the short from TP1 to ground. Increase the Signal Generator output to obtain full-scale deflection ( 60 dB ) of the dB meter. Adjust R1 on A 24 to obtain +60 mV at TP2.
f. Adjust the Signal Generator for $30 \%$ modulation at 1 kHz on the full-scale input signal. Connect a Ballentine VTVM and Oscilloscope to TP4 on A24.
g. Adjust the AUDIO GAIN control on the front panel to obtain 7V RMS on the VTVM. The waveform on the Oscilloscope should be an undistorted sine wave at a frequency of 1 kHz .
h. The nominal DC voltage levels of the integrated circuits and transistors on A24 as measured to ground with the Digital Voltmeter are listed for reference (values are in volts):

|  | Pins 1, 2, 6, 7, 11, 12 | Pin 3 | Pins 8, 10 | Pin 9 |
| :---: | :---: | :---: | :---: | :---: |
| AR1: | +4.5 | 0 | +5.5 | +9.1 |
| $\begin{aligned} & v_{: E} \\ & v_{: B} \\ & v_{C:} \end{aligned}$ | Q1 and Q2 |  |  |  |
|  | +0.06 |  |  |  |
|  | +0.7 |  |  |  |
|  | +11.9 |  |  |  |

### 4.5.7 Alignment of dB Readout and Audio Amplifier A24 on Serial Number 206 and Above

Perform the alignment procedures for weighting and meter amplifier A21 given in paragraph 4.5.4 and proceed as follows:
a. Set the FUNCTION switch to FIELD INTENSITY and set the ATTENUATOR switch to the -20 dB position. Reduce the output of the Signal Generator to obtain 0 dB on the NM-37/57 dB meter.
b. Connect the digital voltmeter to TP1 and adjust R 4 for $\mathrm{OV} \pm 1 \mathrm{mV}$.
c. Connect the digital voltmeter to TP2 and adjust R14 for $-200 \mathrm{mV} \pm 2 \mathrm{mV}(-198 \mathrm{mV}$ to $-202 \mathrm{mV})$.
d. Apply +12 V to pin $4(0 \mathrm{~dB})$. Check for $0 \mathrm{mV}+2 \mathrm{mV}$ at TP2. Check N the logic level on pin 11 ; the nominal value is +11.3 V .
e. Remove the +12 V from pin 4 and apply it to pin $5(+20 \mathrm{~dB})$. Check for $+200 \mathrm{mV}+2 \mathrm{mV}(+198 \mathrm{mV}$ to +202 mV ) at TP2. Check the logic level on pin 11 ; the nominal value is +11.3 V .
f. Remove the +12 V from pin 5 and apply it to pin $15(+40 \mathrm{~dB})$. Check for $+400 \mathrm{mV} \pm 3 \mathrm{mV}(+397 \mathrm{mV}$ to +403 mV ) at TP2. Check the logic level on pin 11 ; the nominal value is +11.3 V .
g. Remove the +12 V from pin 15 and apply it to pin 16 ( +60 dB ). Check for $+600 \mathrm{mV}+4 \mathrm{mV}(+596 \mathrm{mV}$ to +604 mV ) at TP2. Check the logic level on pin 11 ; the nominal value is +11.3 V .
h. Remove the +12 from pin 16 and apply it to pin 7 . Check for $0 \mathrm{~V}+2 \mathrm{mV}$ at TP2. Check the logic level on pin 11 . The nominal value is +10.6 V .
i. Connect the precision adjustable power supply to pin 3 ( dB input) and apply sequentially $+1,+2$ and +3 V to the dB Input. Check at TP2, sequentially for $+200 \mathrm{mV},+400 \mathrm{mV}$ and +600 mV . These values are $+0.5 \%$.
j. Remove the +12 V from pin 7 and repeat step i. Check at TP2, sequentially, for $0 \mathrm{~V},+200 \mathrm{mV}$ and +400 mV . These values are $\pm 3 \mathrm{mV}$.
k. Apply +12 V to pin $16(+60 \mathrm{~dB})$ and repeat step i. Check at TP2, sequentially, for $+800 \mathrm{mV},+1.0 \mathrm{~V},+1.2 \mathrm{~V}$. These values are $+0.5 \%$. Remove the +12 V from pin 16 ; the adjustable power supply from pin 3 and the digital voltmeter from TP2.
I. Connect the audio generator to pin 14 (Audio Input) and the audio vtvm to TP3. Apply 10 mV at 1 kHz to pin 14 and measure $690 \mathrm{mV}+69 \mathrm{mV}(+621 \mathrm{mV}$ to $+759 \mathrm{mV})$ at TP 3.
m . Vary the frequency of the audio generator from 1 kHz to 10 Hz and then from 1 kHz up to 5 kHz ; the frequency response should be flat within 3 dB .
n. Connect the oscilloscope to TP3 and apply 1 kHz to pin 14. Increase the input signal level until the output signal is undistorted. Measure the maximum available undistorted output level at TP3. It should be no more than 6 V rms. The output power should be approximately 60 mW .
o. Repeat step n at 5 kHz ; the maximum available undistorted output level should be no more than 5.5 V rms. The output power should be approximately 50 mW .

### 4.6 MAINTENANCE AND ALIGNMENT OF IF SECTION

The following test equipment (or equivalent) is required for maintenance and alignment of the IF section of the NM-37/57:
Signal Generator, HP 608 E
Digital Voltmeter, HP 3440A
Step Attenuator (10 dB per step), HP 355D
Oscilloscope, Tektronix 535A
VTVM, Ballentine 861
RF Millivoltmeter, HP 411A
Frequency Counter, CMC 616
Impulse Generator, Singer Model 91263-1
Impulse Generator, Singer Model 93453-1
Sweep Generator, Texscan VS50

Audio Generator, HP 200CD
Sweep Generator, Telonic SM2000 (with Oscillator 3006)
Band Pass Filter, 20.5 MHz, Telonic TBP 20.5-3-4-AA

## NOTE

Before beginning procedures on any of the shielded modules (A1-A18), remove the module from the chassis and connect with extender cable. Remove module cover for access to circuit components.

### 4.6.1 Alignment and Test of Log IF amplifier A41

Refer to Paragraph 4.5.1 and Figure 4-1 and connect the test equipment as directed, except use a 10 dB Step Attenuator (HP 355D) in series with the signal input to the log IF amplifier.
a. Connect a Frequency Counter (CMC 616) to the output of the Signal Generator and adjust the output frequency to 20.500 MHz .
b. Connect an RF Millivoltmeter (HP 411A) to the output of the Signal Generator and adjust output level to obtain 500 millivolts.
c. Set the FUNCTION switch of the NM-37/57 to the FIELD INTENSITY position.

## DC Output Alignment

d. Set the Step Attenuator to 20 dB and observe the DC output voltage of the log IF amplifier A41 on the Digital Voltmeter.
e. Adjust the OFFSET control on A41 to obtain $+3.60+0.01 \mathrm{~V}$.
f. Set the Step Attenuator to 80 dB and adjust the GAIN control on A 41 to obtain +0.01 V .

## NOTE

There is interaction between adjustments of the OFFSET and GAIN controls. Repeat steps d, e, and f as necessary to obtain correct voltages without further adjustment.

## Linearity Check

g. Set the Step Attenuator to the following values and observe that the corresponding DC output voltage of the log IF amplifier is within the tolerance specified:

| Step Attenuator <br> Setting (dB) | Log IF Output <br> $(\mathrm{V})$ | Tolerance <br> $(\mathrm{mV})$ |
| :---: | :---: | :---: |
| 0 | +4.6 | +100 |
| 10 | +4.1 | 1 ioo |
| 20 | +3.6 | +50 |
| 30 | +3.1 | +50 |
| 50 | +2.1 | +50 |
| 60 | +1.6 | +50 |
| 70 | +1.1 | +50 |
| 80 | +0.6 | +50 |

## Noise Output

h. Adjust the Signal Generator output level for $224 \mathrm{mV}(0 \mathrm{dBm})$ and set the Step Attenuator for 0 dB .
i. Disconnect the Digital Voltmeter from the BNC T-adapter connected to J3 of A41 and connect the Ballentine VTVM to the output at J3.
j. Decrease the Signal Generator output from $224 \mathrm{mV}(0 \mathrm{dBm})$ down to 0 mV (no signal) and observe the noise voltage at J 3 on the VTVM. The maximum noise should occur from -80 to -90 dBm input signal level and should not exceed 25 mV RMS.

## Buffered Video Output

k. Disconnect the VTVM from the output at J3 and reconnect the Digital Voltmeter. Adjust the Signal Generator to obtain $+3.60+0.01 \mathrm{~V}$ at J 3 as indicated on the Digital Voltmeter.
I. Connect a 50 ohm load from J 4 on A 41 to ground and measure the output signal level at J 4 with the Digital Voltmeter. The buffered video output voltage should be $+300+6 \mathrm{mV}$.
m . Remove the 50 ohm load. The buffered output at J 4 should rise $6+1 \mathrm{~dB}$, and the output voltage at J 3 should remain unchanged.

## Limited IF Output

n. Connect a 50 ohm load from J5 on A 41 to ground and measure the output signal level at J 5 with the RF Millivoltmeter. The limited IF output should be $400+40 \mathrm{mV}$ RMS.
o. Decrease the input signal level 60 dB by setting the Step Attenuator for 60 dB . The limited IF output voltage at J 5 should not drop more than 3 dB .

### 4.6.2 Alignment and Test of Linear IF Amplifier and BFO A15

Remove module A15 from the chassis and connect with extender cable before proceeding.
a. Remove cables from connectors $\mathrm{J} 1, \mathrm{~J} 3$, and J 4 on A 15 and connect test equipment as shown in Figure 4-2. Terminate J 1 and J 4 with 50 ohm loads. Set FUNCTION switch to FIELD INTENSITY.

## IF Gain and AGC Operation

NOTE
Shield integrated circuit AR1 with the module cover plate during the following procedures.
b. Adjust Signal Generator for 20.5 MHz CW signal at -13 dBm at input J 1 of Al 5 .
c. Adjust C14 on A15 for maximum indication on the RF Millivoltmeter connected to TP1. The voltage at TP1 should be from 1.6 to 2.8 V RMS and the voltage at TP2 should be from +0.6 to +0.9 V DC .
d. Decrease the Signal Generator output to -73 dBm . The voltage at TP1 should be from 0.9 to 1.8 V RMS and at TP2 from -0. 1 to -0.3 V DC.
e. Increase the Signal Generator output to 0 dBm . The voltage at TP1 should be from 2.5 to 3.5 V RMS and at TPZ from +0.8 to +1.1 V DC.


Figure 4-2. Test Equipment Setup for Linear IF Amplifier Test and Alignment

## Linear Video Output

f. Disconnect the voltmeters from TP1 and TP2 and replace the cover on A15.
g. Adjust the Signal Generator for $1 \mathrm{kHz} \mathrm{80} \mathrm{\%}$ modulation (internal) on the 20.5 MHz signal and set the output level at-13 dBm.
h. Readjust C14 on A15 for maximum indication on the VTVM connected to J 4 and for optimum waveshape on the Oscilloscope connected to J3.

## NOTE

Readjustment of C14 is required due to effects of voltmeter probe at TP1 and cover removal in steps a through e.
i. The output voltage at J 4 with the 50 ohm load should be from 100 to 160 mV RMS and the waveform at J3 should be an undistorted 1 kHz sine wave.
j. Decrease the output of the Signal Generator in 10 dB steps to -63 dBm . The sine wave on the Oscilloscope should decrease in amplitude but remain undistorted. At -63 dBm the output at J4 should be from 50 to 100 mV RMS.

## Frequency Response Test

k. Connect an Audio Generator (HP 200 CD) to the Signal Generator external modulation input. Set the Signal Generator for external modulation and adjust the Audio Generator for a $1 \mathrm{kHz}, 2 \mathrm{~V}$ signal. Adjust the modulation to $50 \%$ at 20.5 MHz with an input level to J 1 of A 15 of -20 dBm .
I. The voltage output at J 4 with the 50 ohm load should be $50-80 \mathrm{mV}$ RMS. The waveform at J 3 should be undistorted.
m. Adjust the Audio Generator to decrease the modulation frequency from 1 kHz to 20 Hz in octave steps (reduce frequency to one-half each step). The video output at J 4 should be flat within 1 dB and the sine wave at J3 should remain undistorted.
n. Increase the modulation frequency from 1 kHz to 200 kHz in octave steps (double the frequency each step). The output at J4 should be flat within 3 dB and the sine wave at J3 undistorted.

## BFO Test and Alignment

o. Disconnect the Audio Generator from the Signal Generator. Remove cover from A15 and connect RF Millivoltmeter to TP3. Set the FUNCTION switch to the BFO position.
p. Adjust C31 on A15 to obtain maximum voltage at TP3. The BFO output at TP3 should be $1.0+0$. 2 V RMS.
q. Adjust the frequency of the Signal Generator to exactly 20. 500 MHz as indicated by the Frequency Counter. Adjust the Signal Generator to apply a -20 dBm CW signal to the input of A 15 at J1. Connect the Ballentine VTVM and the Oscilloscope to J3 to monitor the BFO output.
r. The BFO output at J 3 should be a 1 kHz signal with an output level of $50+10 \mathrm{mV}$ RMS.
s. Vary the Signal Generator output from 0 dBm to -80 dBm . The BFO out-put should not change more than +6 dB.

## IF Output

t. Set the FUNCTION switch to FIELD INTENSITY and connect the RF Millivoltmeter across the 50 ohm load at IF output JZ. Adjust the Signal Generator to apply a 50 mV CW signal at 20.5 MHz to J 1 .
u. The IF output at J 2 should be from ZZ to 25 mV RMS.
v. Disconnect the 50 ohm load from JZ and observe that the output increases $6+1 \mathrm{~dB}$.
w. Connect the Oscilloscope to JZ and observe that the IF output is an undistorted sine wave up to 100 mV RMS.
x. The nominal DC voltage levels of the integrated circuit and transistors on A15 as measured to ground with the Digital Voltmeter are listed for reference (values are in volts).

|  | Pin 1 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AR1: | -0.1 | -4.0 | -6 | -4.7 | Pin 2 | Pin 3 |


|  | $\underline{\text { Q1 }}$ | $\underline{\text { Q2 }}$ | $\underline{\text { Q3 }}$ | $\underline{\text { Q5 }}$ | $\underline{\text { Q4 }}$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{V}_{\mathrm{E}:}$ | +2.1 | +2.8 | -0.3 | -8.0 | $\mathrm{VS}:$ | +3 |
| V B: | +2.8 | +3.6 | +0.3 | -7.2 | $\mathrm{VG}:$ | 0 |
| $\mathrm{~V}_{\mathrm{C}:}$ | +7.6 | +11.9 | +9.8 | 0 | $\mathrm{VD}:$ | +12 |

### 4.6.3 Alignment and Test of FM Discriminator A18

Remove module A18 from the chassis and connect with extender cable before proceeding.
a. Remove cables from connectors J 2 and J 4 on FM discriminator A18 and from J1 on log IF amplifier A41. Remove cover from A18.
b. Connect the Digital Voltmeter to pin 6 of integrated circuit AR1 on A18 and adjust R12 to obtain 0 volts. Replace cover on A18.
c. Connect test equipment as shown in Figure 4-3.


EL2RPO53

Figure 4-3. Test Equipment Setup for FM Discriminator Alignment

## Discriminator Alignment

d. Adjust the Sweep Generator for an RF output of 10 mV at 20.5 MHz center frequency and about 1 MHz sweep width. Adjust the Oscilloscope to display the discriminator curve of the FM audio output. Use the Signal Generator as a marker source with frequency monitored by the Counter. Set the Oscilloscope vertical gain for $0.5 \mathrm{~V} / \mathrm{cm}$ and horizontal gain for $0.1 \mathrm{MHz} / \mathrm{cm}$.
e. Adjust the marker frequency to 20.8 MHz and adjust trimmer C9 on A 18 for maximum positive waveform excursion at the marker frequency.
f. Adjust the marker frequency to 20.2 MHz and adjust trimmer C10 on A18 for maximum negative waveform excursion at the marker frequency.

## NOTE

There is interaction between adjustment of C9 and C10. Repeat step e and f until both requirements are met.
g. The correctly aligned discriminator curve is symmetrical with peaks at 20.2 and 20.8 MHz and zero crossover frequency of 20.500 MHz . Nominal peak-to-peak amplitude is 2.2 V .

## FM Video Output

h. Connect a 50 ohm load across the FM video output at J3, and connect the vertical input of the Oscilloscope to J3. The nominal amplitude of the discriminator curve should be 1.2 V peak-to-peak.

## AFC Test and Alignment

i. Disconnect the Sweep Generator and connect the output of the Signal Generator to J1 on log IF amplifier A41. Adjust the Signal Generator for a 10 mV CW signal at 20. $500 \mathrm{M4Hz}$ as monitored by the Frequency Counter.
j. Check the input voltage level at J1 on A18 with an RF Millivoltmeter. The IF input should be 0.4 V RMS.
k. The AFC output voltage at J 4 should be 0.000 V as measured with the Digital Voltmeter. If not, readjust trimmers C9 and C10 to obtain 0.000 V at J4.
I. Adjust the Signal Generator frequency above and below 20. 5 MHz in steps as follows and observe that the AFC voltage at J4 is within $+20 \%$ of the indicated values:

| Signal Generator <br> Frequency (MHz) | AFC Output <br> at J4 (VDC) |
| :---: | :---: |
| 20.0 | -0.9 |
| 20.2 | -1.1 |
| 20.4 | -0.6 |
| 20.5 | 0 |
| 20.6 | +0.6 |
| 20.8 | +1.1 |
| 21.0 | +0.9 |

m. The nominal DC voltage levels of Q1 and AR1 on A18 as measured to ground with the Digital Voltmeter are given for reference (values are in volts):

| AR1: |  | Pins 2 and 3 | Pin 4 | Pin 6 | $\underline{\text { Pin } 7}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0.00+0.01$ | -12 | 0 | +12 |  |
|  |  | Q1 |  |  |  |
| $V_{E}$ : |  | -8.8 |  |  |  |
| $V_{B}$ : |  | -8.1 |  |  |  |
| Vc: |  | -4.1 |  |  |  |

### 4.6.4 Alignment and Test of Bandwidth Selector A14

Remove module A14 from the chassis and connect with extender cable before proceeding.

## Gain Alignment

a. Remove cables from connectors J1 and J2 on A14 and connect test equip- ment as shown in Figure 4-4 Terminate J2 with 50 ohms.


Figure 4-4. Test Equipment Setup for Bandwidth Selector Gain Adjustment
b. Set FUNCTION switch to FIELD INTENSITY and BANDWIDTH switch to .01 MHz .
c. Adjust the Signal Generator for 10 mV input to JI on bandwidth selector A14. Set frequency at 20. 500 MHz as measured by the Frequency Counter.
d. Adjust C6 on A14 to obtain maximum output voltage at J2 as indicated on the RF Millivoltmeter.
e. Adjust R7 on A14 to obtain 125 mV at J2 (22 dB gain).
f. Set the BANDWIDTH switch to 0. 1.MHz and adjust R8 on A14 to obtain 125 mV at J2.
g. Set the BANDWIDTH switch to 1.0 MHz and adjust R9 to obtain 125 mV at J 2 .
h. Reduce the output level of the Signal Generator to 4 mV . Remove the 50 ohm load and RF Millivoltmeter from J2 on A14 and reconnect cables removed in step a to J2.
i. Set the BANDWIDTH switch sequentially to $.01 \mathrm{MHz}, 0.1 \mathrm{MHz}$, and 1.0 MHz positions. The signal level as indicated on the front panel $d B$ meter should be $60+0.2 \mathrm{~dB}$ at each position. If not, readjust $R 7, R 8$, and R9 on A14 as necessary.

## Frequency Response and Bandwidth

j. Remove cable W19 from J3 on log IF amplifier A41 and connect test equip- ment as shown in Figure 4-5.


Figure 4-5. Test Equipment Setup for Bandwidth Selector Alignment and Bandwidth Test
k. Set the BANDWIDTH switch on the NM-37/57 to 1.0 MHz .
I. Set the RF attenuator on the Sweep Generator for 60 dB to obtain a 1.0 mV signal input level to J1 on A14. Use the Signal Generator as a marker source with frequency monitored by the Frequency Counter and adjust the Sweep Generator for a sweep width of 10 MHz at a center frequency of 20.5 MHz . Set the sweep rate for 10 sweeps per second.
m. Adjust the Oscilloscope to display the frequency response of the bandwidth selector output. Set the Oscilloscope horizontal gain for $1 \mathrm{MHz} / \mathrm{cm}$ and vertical gain for $1 \mathrm{~V} / \mathrm{cm}$.
n. Adjust C25, C26, and C27 on A14 as necessary to obtain a 6 dB bandwidth of from 0.9 MHz minimum to 1.3 MHz maximum.
o. Set the BANDWIDTH switch to 0.1 MHz . Decrease the sweep width to 1 M and set the Oscilloscope horizontal gain for $100 \mathrm{kHz} / \mathrm{cm}$.
p. The 6 dB bandwidth should be from 900 kHz minimum to 130 kHz maximum
q. Set the BANDWIDTH switch to .01.Decrease the sweep width to 100 kHz and set the Oscilloscope horizontal gain for $10 \mathrm{kHz} / \mathrm{cm}$.
r. The 6 dB bandwidth should be from 9 kHz minimum to 13 kHz maximum.

## Noise Output

s. Disconnect all test equipment. Terminate the input of A14 at J1 with 50 ohms and reconnect cable W19 to J3 on A41.
$t$. Check the internal noise indication on the $d B$ meter for each bandwidth with the four detector functions. The nominal values in $d B$ are as follows:

| FUNCTION Switch: |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| BANDWIDTH | FIELD | QUASI | DIRECT | SLIDEBACK |
| Switch | INTENSITY | PEAK | PEAK | PEAK |
|  |  |  |  |  |
| $01 \mathrm{MHz}:$ | 0 | 0 | 2 | 2 |
| $0.1 \mathrm{MHz}:$ | 0 | 0 | 2 | 2 |
| 1.0 MHz | 0 | 0 | 5 | 5 |

u. The nominal DC voltage levels of the transistors on A14 as measured to ground with a Digital Voltmeter are given for reference (values are in volts):

|  | $\underline{Q 1}$ | $\underline{Q 2}$ |
| :---: | :---: | :---: |
| $V_{\mathrm{E}}:$ | +8.5 | +8.0 |
| $V_{\mathrm{B}}:$ | +7.7 | +7.4 |
| $V_{C}:$ | -1.8 | 0 |

### 4.6.5 Maintenance of Voltage Controlled IF Attenuator A48

-To gain access to the test points on the A48 circuit board, remove the CALIBRATE control knob and lock nut and remove A48 from the front panel. Remove the two screws that secure the cover on A48 and slide the circuit board out of the cover assembly.

## Gain Control Voltage Check

a. Remove cables W8 and W9 from J1 and J2 of A48.
b. Set the CALIBRATE control to the positions indicated and measure the positive DC voltages at TP1 and TP2 with a Digital Voltmeter (values are given in volts, tolerance is 120 mV ):

|  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | FALIBRATE Control Setting: |  |  |  |  |  |
| TP1: | Full | $\underline{60^{\circ}}$ | $\frac{120^{\circ}}{}$ | $\frac{180^{\circ}}{}$ | $\frac{240^{\circ}}{0}$ | Fully CW |
| TP2: | 0.5 | 0.55 | 0.6 | 0.65 | 0.7 | 0.75 V |
|  | 0.8 | 0.75 | 0.7 | 0.65 | 0.6 | 0.55 V |

## Gain Control Range Check

c. Connect the output of the Signal Generator to J1 on A48.Terminate the output of A48 at J2 with 50 ohms. Adjust the output of the Signal Genera- tor for 100 mV CW at 20.5 MHz .
d. Measure the output voltage across the 50 ohm load at J2 with the RF Milli- voltmeter. Set the CALIBRATE control to the positions indicated and determine that the attenuation in $d B$ is within the tolerance given (values are in $d B$ ):

| CALIBRATE Control Setting: |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fully CCW | $60^{\circ}$ | $120^{\circ}$ | $180^{\circ}$ | $\underline{240}{ }^{\circ}$ | Fully CW |
| Attenuation: | 20.5 | 15.5 | 10 | 6 | 3 | 1.2 |
| Tolerance: | +2 | +1.5 | $\pm 1$ | 0.5 | +0.3 | 0.2 |

## CW Signal Tracking

e. Connect test equipment as showr in Figure 4-6.Adjust the Signal Genera- tor output for 10 mV CW at 20.5 MHz and set the Step Attenuator for 0 dB .


Figure 4-6. Test Equipment Setup for Voltage Controlled IF Attenuator CW Signal Tracking Test
f. Set the BANDWIDTH switch to 0.1 MHz and the FUNCTION switch to FIELD INTENSITY. Adjust the CALIBRATE control to obtain full scale deflection ( 60 dB ) on the dB meter.
g. Set the FUNCTION switch to QUASI-PEAK, to each of the PEAK positions, and to SLIDEBACK PEAK and measure the signal level. The dB meter should indicate $60+0.5 \mathrm{~dB}$ for each function.
h. Decrease the input in 10 dB steps with the Step Attenuator and observe the dB meter indication for each of the four functions at each input level. The tolerance is +2 dB of the nominal levels at $50,40,30,20$, and 10 dB .

## Impulse Signal Tracking

i. Disconnect the Signal Generator and Step Attenuator and connect an Impulse Generator (Singer 93453-1) to the input of the Band Pass Filter. Adjust the Impulse Generator output to $80 \mathrm{~dB} \mathrm{\mu V} / \mathrm{MHz}$ at a PRF of 60 pps .
j. Set the BANDWIDTH switch on the NM-37/57 at 1.0 MHz . Set the FUNC- TION switch to PEAK/0.3 SEC HOLD and SLIDEBACK PEAK. Observe that the measured signal level as indicated on the dB meter is 60 +1 dB for both functions.
k. Decrease the Impulse Generator output in 10 dB steps as follows and observe the dB meter indication for the direct peak and slideback peak functions. The tolerance is $\pm 2 \mathrm{~dB}$ of the nominal levels given:

| Impulse Signal Level | Meter |
| :--- | :---: |
| $(\mathrm{dB} \mu \mathrm{V} / \mathrm{MHz})$ | Indication $(\mathrm{dB})$ |


| 70 | 50 |
| :--- | :--- |
| 60 | 40 |
| 50 | 30 |
| 40 | 20 |

I. Set the BANDWIDTH switch to 0.1 MHz . Adjust the Impulse Generator output to $100 \mathrm{~dB}-\mathrm{V} / \mathrm{MHz}$.
m . Set the FUNCTION switch to PEAK/0. 3 SEC HOLD and SLIDEBACK PEAK. Observe that the measured signal level on the dB meter is $60 \pm 1 \mathrm{~dB}$.

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Decrease the impulse signal as follows and observe the dB meter indication for both functions is within m2 of the nominal levels:

Impulse Signal Level
( $\mathrm{dB} \mu \mathrm{V} / \mathrm{MHz}$ )
90
80
70
60

Meter
Indication (dB)
50
40
30
20
n. Adjust the Impulse Generator for $100 \mathrm{~dB} \mu \mathrm{~V} / \mathrm{MHz}$ output. Set the NM-37/57 BANDWIDTH selector switch to .01 MHz .
o. Set the FUNCTION switch to PEAK/0. 3 SEC HOLD and SLIDEBACK PEAK and measure the signal level. The dB meter should indicate $40+1 \mathrm{~dB}$ for both functions.

### 4.6.6 Alignment and Test of IF Preamplifier A13

Remove module A13 from the chassis and connect with extender cable before proceeding. Disconnect signal cables from A13.

## Frequency and Gain Adjustment

a. Connect the Signal Generator output to J 1 on A 13 and adjust the Signal Generator for 10 mV CW signal at 20.5 MHz as monitored by the Frequency Counter. Set the ATTENUATOR switch on the NM-37/57 to -20 dB .
b. Connect the RF Millivoltmeter to TP1 on A13 (remove cover) and adjust trimmers C3 and C6 for maximum voltage at TP1.The signal level at TP1 should be from 40 to 70 mV RMS.
c. Terminate output at J 3 with 50 ohms and connect the RF Millivoltmeter to J3.Adjust trimmer C10 for maximum voltage at J3.
d. Adjust R7 on A13 to obtain 125 mV at J 3 (22 dB gain).
e. Check and readjust C3, C6, and C10 as necessary for maximum output and repeat step d. The reserve gain available with $R 7$ should be greater than 5 dB but less than 10 dB .

## Bandwidth Check

f. Adjust the Signal Generator for 30 mV input signal to obtain 380 mV at output connector J3.
g. Measure the bandwidth at 3 dB and at 40 dB . The 3 dB bandwidth should be 2 MHz minimum, and the 40 dB bandwidth should be 18 MHz maximum.

## CW Signal Tracking

h. Connect the test equipment as shown in Figure 4-6to J1 of A13. Connect cable W8 between J3 on A13 and J 1 on A48. Adjust the Signal Generator output for 10 mV at 20.5 MHz and set the Step Attenuator for 0 dB .
i. Set the ATTENUATOR switch on the NM-37/57 to 0 dB , the FUNCTION switch to FIELD INTENSITY, and the BANDWIDTH selector to 0.1 MHz . Adjust the CALIBRATE control to obtain full scale deflection ( 60 dB ) on the dB Meter.
j. Set the FUNCTION switch to QUASI-PEAK, to each of the PEAK positions, and to SLIDEBACK PEAK and measure the signal level. The dB meter should indicate $60 \pm 0.5 \mathrm{~dB}$ for each function.
k. Decrease the input in 10 dB steps with the Step Attenuator and observe the dB meter indication for each of the four functions at each input level. The tolerance is +2 dB of the nominal levels at $50,40,30,20$, and 10 dB .
I. Adjust the Signal Generator output for 1 mV and set the ATTENUATOR switch to -20 dB .
m. Repeat steps j and k .

## Impulse Signal Tracking

n. Perform step i of Paragraph 4.6.5 using Impulse Generator 91263-1 in place of Impulse Generator 93453-1.
o. Set the ATTENUATOR switch to 0 dB and perform steps j and k of Paragraph 4.6.5.
p. Adjust the Impulse Generator output for $80 \mathrm{~dB} \mu \mathrm{~V} / \mathrm{MHz}$.
q. Set the FUNCTION switch to PEAK/0. 3 SEC HOLD and SLIDEBACK PEAK. Measure the signal level for each bandwidth in both functions. The tolerance is +2 dB of the nominal levels as follows:

BANDWIDTH Meter Indication
Switch Position
(dB)
$1.0 \mathrm{MHz} \quad 60$
$0.1 \mathrm{MHz} \quad 40$
$.01 \mathrm{MHz} \quad 20$

## Gain Calibration

r. Remove cable W21 from J1 of IF switch All. Connect output of the Signal Generator to J1 of All. Connect cable W5 between J9 of All and J1 of A13.Adjust the Signal Generator output for 10 mV CW at 20.5 MHz .
s. Set the ATTENUATOR switch to 0 dB , BAND switch to Band 1, BAND- WIDTH switch to 0 . 1 MHz , and FUNCTION switch to FIELD INTENSITY.
t. Adjust the CALIBRATE control for full scale deflection ( 60 dB ) on the dB meter.
u. Check that the reserve gain available with the CALIBRATE control is $9+1 \mathrm{~dB}$. If not, readjust R7 on A13. Check that the total range of the CALIBRATE control is $20+2 \mathrm{~dB}$.
v. Repeat step t.

## NOTE

Do not change the setting of the CALIBRATE control for the remainder of the IF section procedures.

## Noise Output Check

w. Remove test equipment and reconnect cable W21 to J1 on IF switch All. Disconnect cable W5 at J1 on A13 and terminate input J1 with 50 ohms.
x. Set the ATTENUATOR switch to -20 dB . Observe the internal noise indicated on the dB meter for each function and bandwidth and compare with the following nominal values in dB :

| FUNCTION Switch: |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BANDWIDTH | FIELD | QUASI- | DIRECT | SLIDEBACK |  |
| Switch | INTENSITY | PEAK | PEAK | PEAK |  |
| .01 MHz | 0 | 1 | 2 | 2 |  |
| 0.1 MHz | 0 | 2 | 6 | 6 |  |
| 1.0 MHz | 6 | 10 | 15 | 15 |  |

y. The nominal DC voltage levels of the transistors on A13 as measured to ground with a Digital Voltmeter are given for reference (values in volts):

|  | Q 1 | Q 2 |
| :---: | :---: | :---: |
| $\mathrm{~V}_{\mathrm{E}}:$ | -10.6 | -8.6 |
| $\mathrm{~V}_{\mathrm{B}}:$ | -10 | -8 |
| $\mathrm{~V}_{\mathrm{C}}:$ | 0 | 0 |

### 4.6.7 Alignment and Test of IF Converter A12

Remove module A12 from the chassis and connect with extender cable before proceeding. Disconnect signal cables from A12.
a. Set the BAND selector on the NM-37/57 to any Band from 4 through 8 to apply -12 V to A 12 circuits.

## Local Oscillator Alignment

b. Connect RF Millivoltmeter to TP1 on A12 and adjust C41 for maximum voltage. The correct signal level at TP1 is from 400 to 500 mV RMS.
c. Connect RF Millivoltmeter to TP2 and adjust C38 and then C34 for maximum voltage. The signal at TP2 should be from 500 to 600 mV .
d. Connect RF Millivoltmeter to TP3 and adjust R18 to obtain 350 mV .

## Band Pass Filter and Output Alignment

e. Connect Signal Generator output to J 1 on A 12 and adjust for 10 mV CW signal at 160 MHz .
f. Connect RF Millivoltmeter to TP4 and adjust trimmers C2, C4, C7, C8, and C10 in that order for maximum voltage. Because of interaction between adjustments, repeat several times until the voltage at TP4 is at maximum, then adjust C9 if necessary to obtain $45+5 \mathrm{mV}$ at TP4.
g. Connect the RF Millivoltmeter to output connector J2 on A13 and terminal J2 with 50 ohms.
h. Adjust C15 for maximum voltage at J2, then adjust R12 to obtain an output of 125 mV across the 50 ohm load.

## Bandwidth Check

i. Monitor the Signal Generator output frequency with the Frequency Counter and measure the 6 dB bandwidth at J2. The 6 dB bandwidth should be $3+0.2 \mathrm{MHz}$. If not, realign C 9 to obtain the correct bandwidth, then repeat step h.

## Converter Gain Adjustment

j. Reconnect cable W 40 to J 1 and cable W 7 to J 2 of A12.Disconnect cable W 27 from J 7 of IF switch Al 1.
k. Connect the Signal Generator via a 10 dB Step Attenuator to J7 on All. Set the Step Attenuator for 0 dB. Set the ATTENUATOR switch on the NM-37/57 to 0 dB , the BAND switch to Band 7, the BANDWIDTH to 0.1 MHz , and the FUNCTION switch to FIELD INTENSITY.

## NOTE

The CALIBRATE control must be set as instructed in steps $r$, $s$, and $t$ of Paragraph 4.6.6 before proceeding. Do not change setting for remainder of A 12 procedures.
I. Adjust the Signal Generator output for 10 mV at 160 MHz . The dB meter should indicate 60 dB . If not, readjust R12 on A12.

## CW Signal Tracking

m. Perform steps $j$ through $m$ oParagraph 4.6.6 to check the CW signal reading accuracy of A12.

## Impulse Signal Tracking

n. Disconnect the Signal Generator and Step Attenuator and connect Impulse Generator 91263-1 to J7 on All. Adjust the Impulse Generator output to $80 \mathrm{~dB} \mu \mathrm{~V} / \mathrm{MHz}$ at a PRF of 60 pps .
o. Set the ATTENUATOR switch to 0 dB and perform steps j and k of Paragraph 4.6.5
p. Perform steps $p$ and $q$ of Paragraph 4.6.6.

## Noise Output Check

q. Remove test equipment and reconnect cable W27 to J7 on All1.
r. Set the ATTENUATOR switch to -20 dB . Observe the internal noise indi- cated on the dB meter for each function and bandwidth and compare with the following nominal values in dB :

| FUNCTION Switch: |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BANDWIDTH | FIELD | QUASI- | DIRECT | SLIDEBACK |  |
| Switch | INTENSITY | PEAK | PEAK | PEAK |  |
| .01 MHz | 0 | 0 | 6 | 6 |  |
| 0.1 MHz | 0 | 6 | 12 | 12 |  |
| 1.0 MHz | 10 | 16 | 22 | 22 |  |

s. The nominal DC voltage levels of the transistors on A12 as measured with a Digital Voltmeter are given for reference (values are in volts):

|  | Q1 | Q2 | Q3 | Q4 |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{E}}:$ | -10.3 | -8.4 | -10.2 | -9.3 |
| $\mathrm{~V}_{\mathrm{B}}:$ | -9.8 | -7.8 | -12.0 | -9.5 |
| $\mathrm{~V}_{\mathrm{C}}:$ | 0 | 0 | 0 | 0 |

### 4.7 MAINTENANCE AND ALIGNMENT OF TUNING CONTROL SECTION

The following test equipment (or equivalent) is required for maintenance and align- ment of the tuning control section of the NM-37/57. Digital Voltmeter, HP 3440A Ohmmeter, Triplett 630

### 4.7.1 Alignment and Test of Tuning Control A29

a. Set the CONTROL MODE switch to LOCAL, AFC switch to OFF, FUNC- TION switch to FIELD INTENSITY, and rotate the TUNE and FINE TUNE controls fully counterclockwise.
b. Measure the DC voltage at TP2 on A29 to ground with the Digital Voltmeter. The voltage should be $0 \mathrm{~V} \pm 10$ mV .
c. Rotate the TUNE control fully clockwise and adjust R1 on A29 to obtain $+10.000 \mathrm{~V} \pm 1 \mathrm{mV}$ at TP2.
d. Rotate the TUNE control fully counterclockwise and the FINE TUNE control fully clockwise. The voltage at TP2 should be $+200 \pm 20 \mathrm{mV}$.
e. Rotate both TUNE and FINE TUNE controls fully clockwise. The voltage at TP2 should be $+10.2 \mathrm{~V}+20 \mathrm{mV}$.
f. Rotate the FINE TUNE control fully counterclockwise and the TUNE con- trol fully clockwise. Adjust R18 on A29 to obtain full scale deflection on the front panel frequency meter.
g. Measure the DC voltage at the $X$ OUTPUT jack on the rear panel with the Digital Voltmeter. The voltage should be $+2.0 \mathrm{~V}+20 \mathrm{mV}$. Connect a 1 kilohm load across the X OUTPUT jack and the voltage should drop to $1.0 \mathrm{~V} \pm 10 \mathrm{mV}$.

### 4.7.2 Alignment and Test of Shaper 1, A26

a. Set the BAND switch to Band 1 and rotate the TUNE and FINE TUNE controls fully counterclockwise.
b. Measure the DC voltage at TP1 on A26 to ground with the Digital Volt- meter. Adjust R31 on A26 to obtain $+1.7 \mathrm{~V}+30 \mathrm{mV}$ at TP1.
c. Rotate the TUNE control fully clockwise and adjust R40 on A26 to obtain $+60 \pm+1 \mathrm{~V}$ at TP1.
d. Rotate the TUNE control fully counterclockwise and repeat step b.

## NOTE

There is interaction between adjustments of R31 and R40. Repeat steps b, c, and d as necessary to obtain correct voltages at TP1 without further adjustment.
e. Leave the BAND switch at Band 1, but use the Band 8 scale of the frequency meter as reference and rotate the TUNE control to the following equally- spaced frequencies. The DC voltage at TP1 on A26 should be within $+2 \%$ of the values indicated:

Frequency Meter
(Band 8)
800
840
880
920
960
1000

A26TP1
(Volts)
+1.7
+4.15
+8.7
+17.2
+31.8
f. The nominal DC voltage levels of the integrated circuits and transistors on A26 as measured with the Digital Voltmeter are given for reference (values are in volts). Rotate the TUNE and FINE TUNE controls fully counterclockwise.

|  |  | Pins 2 and 3 |  | Pin 4 |
| :--- | :--- | :--- | :--- | :--- |
| AR1: | 0 | $\frac{\text { Pin } 6}{+025}$ | $\frac{\text { Pin } 7}{+12}$ |  |
| AR2 thru AR6: | 0 | -12 | +05 | +12 |
| AR7: | 0 | -12 | -1.5 | +12 |
| VE: | $\underline{\text { Q1 }}$ | $\underline{\text { Q2 }}$ | +9 | $\underline{\text { Q3 }}$ |
| VB: | -08 | +90 | $\underline{\text { Q4 }}$ |  |
| VC: | -0.2 | +9.6 | +1.7 | -12 |

### 4.7.3 Alignment and Test of Shaper 2, ,A27

a. Set the BAND switch to Band 4 and rotate the TUNE and FINE TUNE controls fully counterclockwise.
b. Measure the DC voltage at TP1 on A27 to ground with the Digital Voltmeter. Adjust R31 on A27 to obtain +4 . $0 \mathrm{~V} \pm 80 \mathrm{mV}$ at TP1.
c. Rotate the TUNE control fully clockwise and adjust R40 on A 27 to obtain $+60 \pm 1 \mathrm{~V}$ at TP1.
d. Rotate the TUNE control fully counterclockwise and repeat step b.

## NOTE

There is interaction between adjustments of R31 and R40. Repeat steps b through d as necessary to obtain correct voltages at TP1 without further adjustment.
e. Leave the BAND switch at Band 4, but use the Band 8 scale of the frequency meter as reference and rotate the TUNE control to the following equally-spaced frequencies. The DC voltage at TP1 on A27 should be within $+2 \%$ of the values indicated:

Frequency Meter
(Band 8)
800
840
880
920
960
1000

A27TP1
(Volts)
+4. 0
+8.5
+15.2
+24.5
+38.9
+60.0
f. The nominal DC voltage levels of the integrated circuits and transistors on A27 as measured with the Digital Voltmeter are given for reference (values are in volts). Rotate the TUNE and FINE TUNE controls fully counterclockwise.

|  | Pins 2 and 3 | Pin 4 | Pin 6 | Pin 7 |
| :--- | :--- | :--- | :--- | :--- |
| AR1: | 0 | -12 | +0.25 | +12 |
| AR2 thru AR6: | 0 | -12 | +0.5 | +12 |
| AR7: | 0 | -12 | -1.5 | +12 |
|  | Q1 | QZ | Q3 | Q4 |
| $\mathrm{V}_{\mathrm{E}}:$ | -0.8 | +11.0 | +4.0 | -12 |
| $\mathrm{~V}_{\mathrm{B}}:$ | -0.4 | +11.7 | +4.4 | -11.4 |
| $\mathrm{~V}_{\mathrm{C}}:$ | +4.4 | +100 | +100 | +4.0 |

### 4.7.4 Alignment and Test of Internal Sweep A33

a. Set the CONTROL MODE switch to SCAN.
b. Measure the DC voltage at TP1 on A33 to ground with the Digital Volt- meter and adjust R1 on A33 to obtain $0 \mathrm{~V}+10 \mathrm{mV}$ at TP1.
c. Press the SINGLE switch momentarily.
d. Observe that the voltage at TP1 rises from zero to $+10 \mathrm{~V} \pm 10 \mathrm{mV}$ in approximately one minute, and also observe that the frequency meter scans smoothly to full scale. At the end of the one-minute scan period, the voltage at TP1 should drop to zero, and the frequency meter should indicate at the low end of the scale.
e. Adjust R5 as necessary to obtain $+10 \mathrm{~V} \pm 10 \mathrm{mV}$ at TP 1 at the peak of the scan.
f. Connect an Ohmmeter across the RECORDER PENLIFT jack on the rear panel and observe that an open circuit is indicated.
g. Repeat step c and observe that a short circuit is indicated by the Ohm- meter during the one-minute scan period, then an open circuit when the scan is complete.
h. Connect the Digital Voltmeter to TPZ on A33 and observe approximately +11 V . Repeat step c and observe that the voltage at TP2 drops to approximately -10 V during the scan period, then returns to +11 V .
i. The nominal DC voltage levels of the integrated circuits on A33 are given for reference (values are in volts):

|  | $\frac{\text { AR } 1}{}$ | $\frac{\text { AR2 }}{0}$ | $\frac{\text { AR3 }}{+0.5}$ |
| :--- | :---: | :---: | :---: |
| Pin 3: | 0 | 0 | +3.0 |
| Pin 2: | -12 | -12 | -1.3 |
| Pin 4: | 0 | -12 |  |
| Pin 6: | +12 | +12 | +11.3 |
| Pin 7: | +11.96 | +11.96 | +11.96 |
| Pins 1 and 5: |  |  | +11.96 |

### 4.7.5 Alignment and Test of Frequency Readout A34

a. Set the CONTROL MODE switch to REMOTE to deenergize the band select relays ( K 1 through K8) on A34 and to remove tuning voltages from the input to A34 at TP1. Connect a short from TP1 to ground.
b. Connect the Digital Voltmeter to the output of A34 at TP3 and adjust R22 to obtain zero volts at TP3.
c. Remove the short from TP1 to ground and set the CONTROL MODE switch to LOCAL. Rotate the TUNE and FINE TUNE controls fully counterclockwise to obtain zero volts at TPI as measured with the Digital Voltmeter.
d. Set the BAND switch to Bands 1 thru 8 in sequence and measure the DC voltage at TP3 as follows:

| Band <br> Selected | TP3 Output <br> Voltage |
| :--- | :--- |
| 1 | $+300+3 \mathrm{mV}$ |
| 2 | $+550+4 \mathrm{mV}$ |
| 3 | +1.010 V 5 mV |
| 4 | $+1.860 \mathrm{~V}+6 \mathrm{mV}$ |
| 5 | $+2.850 \mathrm{~V}+8 \mathrm{mV}$ |
| 6 | $+4.300 \mathrm{~V}+10 \mathrm{mV}$ |
| 7 | $+6.000 \mathrm{~V}+13 \mathrm{mV}$ |
| 8 | $+8.000 \mathrm{~V}+15 \mathrm{mV}$ |

e. Rotate the TUNE control fully clockwise to obtain $+10,000 \mathrm{~V}+1 \mathrm{mV}$ at TP1. The voltage at TP2 should measure $-9.000 \mathrm{~V}+5 \mathrm{mV}$.
f. Set the BAND switch to Bands 1 thru 8 in sequence and measure the DC voltage at TP3 as follows:

| Band <br> Selected | TP3 Output <br> Voltage |
| :--- | :--- |
| 1 |  |
| 2 | $+570+4 \mathrm{mV}$ |
| 3 | $+1.050 \mathrm{~V} \pm 5 \mathrm{mV}$ |
| 4 | $+1.920 \mathrm{~V}+6 \mathrm{mV}$ |
| 5 | $+2.920 \mathrm{~V} \pm 8 \mathrm{mV}$ |
| 6 | $+4.450 \mathrm{~V} \pm 10 \mathrm{mV}$ |
| 7 | $+6.200 \mathrm{~V}+12 \mathrm{mV}$ |
| 8 | $+8.250 \mathrm{~V}+14 \mathrm{mV}$ |
|  | $+10.000 \mathrm{~V}+16 \mathrm{mV}$ |

### 4.8 MAINTENANCE AND ALIGNMENT OF RF SECTION

The following test equipment (or equivalent) is required for maintenance and align- ment of the RF section of the NM37/57:

Sweep Generator, Wavetek 2001
Oscilloscope, Tektronix 535A
VSWR Bridge, Telonic TRB-3
RF Detector, Wavetek D-152
Attenuator, 10 dB
Band Pass Filter, 20.5 MHz , Telonic TBP 20.5-3-4-AA

### 4.8.1 Alignment of Tuner 1, A1

Remove module Al from the chassis and connect with extender cable. Remove module cover from side of tuner that has least number of screws.

## Local Oscillator Frequency Alignment

a. Connect test equipment as shown in Figure 4-7.
b. Set the NM-37/57 controls as follows:

Control
BAND switch
BANDWIDTH switch
ATTENUATOR switch

Position
$30-57 \mathrm{MHz}$ (Band 1)
1.0 MHz

0 dB

## Control

CONTROL MODE switch
AFC switch
FINE TUNE control
FUNCTION switch

Position
LOCAL
OFF
Fully CCW
FIELD INTENSITY
c. Adjust the Sweep Generator for a sweep range from 30 to 60 MHz at an output level of - 67 dBm and turn on the 1 MHz and 10 MHz markers. Adjust the Oscilloscope vertical and horizontal gain to display the full sweep range.
d. Adjust the TUNE control on the NM-37/57 to obtain an indication of 30 MHz on the frequency meter.
e. Adjust transformer T5 on tuner Al to obtain tuner response coincident with the 30 MHz marker on the sweep display.
f. Adjust the TUNE control to obtain an indication of 57 MHz on the frequency meter.


Figure 4-7. Test Equipment Setup for Local Oscillator Frequency Alignment of Tuners
g. Adjust trimmer C29 on tuner Al to obtain tuner response coincident with the 57 MHz marker on the sweep display.

## NOTE

There is interaction between adjustments of T5 and CZ9. Repeat steps d through g as necessary to obtain proper frequency response without further adjustment.

## IF Circuit Alignment

h. Adjust the Sweep Generator for a CW output at 32 MHz of -67 dBm .
i. Tune the NM-37/57 for maximum indication on the dB meter, then adjust the CALIBRATE control to obtain 40 dB on the meter.
j. Set the BANDWIDTH switch to 0.1 MHz and adjust FINE TUNE to peak the receiver. Adjust transformer T4 to obtain maximum indication on the dB meter.

## IF Trap Alignment

k. Adjust the Sweep Generator for a sweep range from 15 to 25 MHz at -20 dBm . Insert a 20. 5 MHz Band Pass Filter between the RF output of the Sweep Generator and the RF input to the NM-37/57.
I. Repeat step d.
m. Adjust trimmer C13 to obtain maximum IF response as indicated on the Oscilloscope display.

RF Alignment

## NOTE

The tuner RF filter circuits require alignment to obtain acceptable VSWR, gain flatness, sensitivity, and rejection of undesired signal responses. The tuner VSWR and gain flatness across the band are greatly affected by the impedance matching, coupling, and tuning of the preselector circuits. Some compromise in these characteristics may be necessary to obtain satisfactory overall operation.
n. Disconnect cable W33 at J1 on log IF amplifier A41.Connect the RF Detector via a UG-914 adapter to cable W33 as shown in Figure 4-8, and connect the remainder of the test equipment as indicated.
o. Adjust the Sweep Generator for a sweep range from 30 to 60 MHz . Set the Sweep Generator RF output level at 0 dBm to observe VSWR or at -30 dBm to observe gain response. Set the Oscilloscope vertical gain to obtain $5 \mathrm{mV} / \mathrm{cm}$ sensitivity on both channels.
p. Set the NM-37/57 controls as in step a and adjust the CALIBRATE control to obtain a suitable sweep display on the Oscilloscope.

## NOTE

Adjust the Sweep Generator and Oscilloscope controls as necessary to obtain optimum display during the following procedures.
q. Tune the NM-37/57 over the frequency range of the band and observe the VSWR and gain response on the sweep display.


EL2RPO58

Figure 4-8 . Test Equipment Setup for RF Alignment of Tuners

## NOTE

The actual measurement of VSWR should be made at the frequency that coincides with tuner gain response.
r. Adjust the TUNE control to obtain an indication of 30 MHz on the frequency meter.
s. Adjust transformer T1 on tuner A1 to obtain the best VSWR characteristic at the frequency that coincides with the gain response at the low end of the band, then adjust transformers TZ and T 3 to obtain maximum gain. Obtain the lowest VSWR possible without degrading gain flatness.
t. Adjust the TUNE control to obtain an indication of 57 MHz on the frequency meter.
u. Adjust trimmer CZ on tuner Al to obtain the best VSWR at the frequency that coincides with the gain response at the high end of the band, then adjust trimmers C11 and C18 for maximum gain.

## NOTE

Due to interaction between adjustments, repeat steps $r$ through $u$ as necessary to obtain optimum VSWR and flat gain response across the band without further adjustment. Tuner VSWR should not exceed 2.0 to 1 (typical VSWR is 1.3 to 1 ). Nominal tuner gain should be from 20 to 22 dB and flat across the band within +2 dB .
v. Substitute a standard mismatch termination on the VSWR Bridge to obtain an approximate indication of VSWR magnitude and check average gain and gain flatness across the band.

## NOTE

If VSWR and gain characteristics are within specifications, skip to step x .
w. If VSWR and gain are not within specifications, use the criteria established in steps $r$ through $u$ as a guide and try to obtain acceptable characteristics by compromising gain and VSWR as necessary as the receiver is tuned across the band.

## NOTE

Failure to achieve acceptable performance after following these procedures indicates that critical RF circuit component adjustments are necessary. Such adjustments are beyond the scope of this manual.
x. Reinstall the tuner module in the NM-37/57 chassis and recheck VSWR, average gain, and gain flatness across the band.

### 4.8.2 Alignment of Tuners 2 and $3, \mathrm{~A} 2$ and A 3

Follow the instructions given for the alignment of tuner A1 in Paragraph 4.8.1 and substitute the following frequencies in each step as indicated for the specific tuner being aligned:

## NOTE

Omit the IF trap alignment (steps $k, 1$, and $m$ ) for tuners $A 2$ and $A 3$.

| Step | Change |
| :--- | :--- |
| b | Set BAND switch to frequency band of tuner being aligned. |
| $\mathrm{c}, \mathrm{o}$ | Sweep Generator sweep range: |
|  | Tuner A2: 50 to 110 MHz |
|  | Tuner A3: 100 to 200 MHz |
| $\mathrm{d}, \mathrm{e}, \mathrm{h}$, | Tuner A2: 58 MHz |
| $1, \mathrm{r}$ | Tuner A3: 102 MHz |
| $\mathrm{f}, \mathrm{g}, \mathrm{t}$ | Tuner A2: 104 MHz |
|  | Tuner A3: 190 MHz |

### 4.8.3 Alignment of Tuner 4, A4

Remove module A4 from the chassis and connect with extender cable. Remove module cover from side of tuner that has least number of screws.

## Local Oscillator Frequency Alignment

a. Connect test equipment as shown in Figure 4-7.
b. Set the NM-37/57 controls as follows:

Control

| BAND switch | $186-292 \mathrm{MHz}$ (Band 4) |
| :--- | :--- |
| BANDWIDTH switch | 1.0 MHz |
| ATTENUATOR switch | 0 dB |
| CONTROL MODE switch | LOCAL |
| AFC switch | OFF |
| FINE TUNE control | Fully CCW |
| FUNCTION switch | FIELD INTENSITY |

c. Adjust the Sweep Generator for a sweep range from 180 to 300 MHz at an output level of -67 dBm and turn on the 10 MHz and 50 MHz markers. Adjust the Oscilloscope vertical and horizontal gain to display the full sweep range.
d. Adjust the TUNE control on the NM-37/57 to obtain an indication of 290 MHz on the frequency meter.
e. Adjust R6 on tuner A4 to obtain tuner response coincident with the 290 MHz marker on the sweep display.
f. Adjust the TUNE control to obtain an indication of 190 MHz on the frequency meter.
g. Adjust R5 on tuner A4 to obtain tuner response coincident with the 190 MHz marker on the sweep display.

## NOTE

There is interaction between adjustments of R5 and R6. Repeat steps d through g as necessary to obtain proper frequency response without further adjustment.

## TM 11-6625-2827-14\&P/TO 33A1-4-67-1

RF Alignment

## NOTE

The tuner RF filter circuits require alignment to obtain acceptable VSWR, gain flatness, sensitivity, and rejection of undesired signal responses. The tuner VSWR and gain flatness across the band are greatly affected by the impedance matching, coupling, and tuning of the preselector circuits. Some compromise in these characteristics may be necessary to obtain satisfactory overall operation.
h. Disconnect cable W33 at J1 on log IF amplifier A41.Connect the RF Detector via a UG-914 adapter to cable W33 as shown in Figure 4-8 and connect the remainder of the test equipment as indicated.
i Adjust the Sweep Generator for a sweep range from 180 to 300 MHz . Set the Sweep Generator RF output level at 0 dBm to observe VSWR or at -30 dBm to observe gain response. Set the Oscilloscope vertical gain to obtain $5 \mathrm{mV} / \mathrm{cm}$ sensitivity on both channels.
j. Set the NM-37/57 controls as in step a and adjust the CALIBRATE control to obtain a suitable sweep display on the Oscilloscope.

NOTE
Adjust the Sweep Generator and Oscilloscope controls as necessary to obtain optimum display during the following procedures.
k. Tune the NM-37/57 over the frequency range of the band and observe the VSWR and gain response on the sweep display.

## NOTE

The actual measurement of VSWR should be made at the frequency that coincides with tuner gain response.

1. Adjust the TUNE control to obtain an indication of 290 MHz on the frequency meter.
m . Adjust trimmers C1 and C2 on tuner A4 to obtain the best VSWR characteristic at the frequency that coincides with the gain response at the high end of the band, then adjust trimmer C 3 to obtain maximum gain. Obtain the lowest VSWR possible without degrading gain flatness.
n. Adjust the TUNE control to obtain an indication of 190 MHz on the frequency meter.
o. Adjust RF bias controls R1 and R2 on tuner A4 to obtain the best VSWR at the frequency that coincides with the gain response at the low end of the band, then adjust R3 to obtain maximum gain. Adjust trimmers C4 and C5 for maximum gain.
p. Adjust the TUNE control to obtain 240 MHz on the frequency meter.
q. Adjust RF tuning voltage control R4 on tuner A4 until the VSWR response approximately coincides with the gain response near the center of the band.

## NOTE

Due to interaction between adjustments, repeat steps 1 through q as necessary to obtain optimum VSWR and flat gain response across the band without further adjustment. Tuner VSWR should not exceed 2.0 to 1 (typical VSWR is 1.3 to 1 ). Nominal tuner gain should be from 20 to 22 dB and flat across the band within 2 dB .
r. Substitute a standard mismatch termination on the VSWR Bridge to obtain an approximate indication of VSWR magnitude and check average gain and gain flatness across the band.

## NOTE

If VSWR and gain characteristics are within specifications, skip to step $t$.
s. If VSWR and gain are not within specifications, use the criteria established in steps 1 through q as a guide and try to obtain acceptable characteristics by compromising gain and VSWR as necessary as the receiver is tuned across the band. Readjust trimmer C4 for maximum gain at the point of lowest gain in the band.

## NOTE

Failure to achieve acceptable performance after following these procedures indicates that critical RF circuit component adjustments are necessary. Such adjustments are beyond the scope of this manual.
t . If the average gain in Band 4 is higher than the average gain of the other bands, lower the gain by detuning trimmer C5 on tuner A4.Rotate C5 in a clockwise direction to lower the gain, then recheck gain flatness across the band.
u. Reinstall the tuner module in the NM-37/57 chassis and recheck VSWR, average gain, and gain flatness across the band.

### 4.8.4 Alignment of Tuners 5-8, A5-A8

Follow the instructions given for alignment of tuner A4 in Paragraph 4.8.3 and substitute the following frequencies in each step as indicated for the specific tuner being aligned:

| Step | Change |  |
| :---: | :---: | :---: |
| b | Set BAND switch to frequency band of tuner being aligned. |  |
| c, i | Sweep Generator sweep range: <br> Tuner A5: 280 to 450 MHz <br> Tuner A6: 420 to 630 MHz <br> Tuner A7: 590 to 830 MHz <br> Tuner A8: 790 to 1010 MHz |  |
|  | Tuner | Frequency |
| d, e, 1 | $\begin{aligned} & \text { A5 } \\ & \text { A6 } \\ & \text { A7 } \\ & \text { A8 } \end{aligned}$ | $\begin{aligned} & 440 \mathrm{MHz} \\ & 620 \mathrm{MHz} \\ & 820 \mathrm{MHz} \\ & 1000 \mathrm{MHz} \end{aligned}$ |
| f, g, n | $\begin{aligned} & \text { A5 } \\ & \text { A6 } \\ & \text { A7 } \\ & \text { A8 } \end{aligned}$ | $\begin{aligned} & 290 \mathrm{MHz} \\ & 430 \mathrm{MHz} \\ & 600 \mathrm{MHz} \\ & 800 \mathrm{MHz} \end{aligned}$ |
| $p$ | $\begin{aligned} & \text { A5 } \\ & \text { A6 } \\ & \text { A7 } \\ & \text { A8 } \end{aligned}$ | $\begin{aligned} & 360 \mathrm{MHz} \\ & 520 \mathrm{MHz} \\ & 700 \mathrm{MHz} \\ & 900 \mathrm{MHz} \end{aligned}$ |

### 4.8.5 Test and Alignment of Impulse Calibrator A9

Remove module A9 from the chassis and connect with extender cable before proceeding.
a. Set the FUNCTION switch to CALIBRATE.
b. Observe the positive-going pulse waveform at TP1 on A9 with the Oscilloscope. The pulse shape should be as shown in A, Figure 4-9, with peak amplitude from 1.6 to 2.4 V and pulse width from 35 to 45 Used at $50 \%$ amplitude. The pulse repetition frequency should be $450+45 \mathrm{~Hz}$.
c. Observe the negative-going pulse waveform at TP2 on A9 with the Oscilloscope. The pulse should appear as in B, Figure 4-9, with peak amplitude from -4. 0 to -5.6 V , maximum positive overshoot of 1.2 V , and pulse width from 20 to 25 nanoseconds at $50 \% 0$ amplitude.
d. Observe the positive-going pulse waveform at TP3 and compare with C Figure 4-9. The peak amplitude of the pulse should be from 11 to 15 V , and pulse width from 60 to 130 nanoseconds at $50 \%$ amplitude.

(A) TP1

(B) $\mathrm{TP}_{2}$


Figure 4-9. Impulse Calibrator Waveforms
e. Disconnect cable W3 from J1 on A9.Connect the output from J1 of A9 via Step Attenuator (HP 355D) to a Sampling Oscilloscope. Set the Step Attenuator for 20 dB . Compare the output pulse with D, Figure 49.Adjust R18 on A9 to obtain the narrowest pulse possible at maximum pulse amplitude.

## NOTE

Increasing R18 above the optimum value will reduce pulse amplitude without affecting pulse width. Decreasing R18 below the optimum value will widen the pulse without affecting pulse amplitude.
f. Disconnect test equipment from A9 and reconnect cable W3 to J1.
g. Connect the output of Signal Generator (HP 608E) via Step Attenuator (HP 355D) to the RF INPUT receptacle on the NM-37/57. Set the Step Attenuator for 20 dB . Adjust the Signal Generator for a CW signal at 31 MHz at an output level of $-27 \mathrm{dBm}(10 \mathrm{mV})$, yielding a signal level of -47 dBm at the $\mathrm{NM}-37 / 57 \mathrm{input}$.
h. Set the BAND switch to Band 1, BANDWIDTH switch to 0.1 MHz , ATTENUATOR switch to 0 dB , AFC to OFF, CALIBRATE control to mid-position, and FUNCTION switch to QUASI-PEAK.
i. Tune the NM-37/57 for maximum indication on the dB meter, then adjust the CALIBRATE control to obtain exactly 60 dB indication (full-scale deflection).
j. Set the FUNCTION switch to CALIBRATE and observe the calibration figure indicated on the dB meter. Readjust R18 on A9 as necessary to obtain a calibration figure of $30 \pm 0.2 \mathrm{~dB}$ on the meter.
k. The nominal DC voltage levels of the transistors on A9 as measured with the Digital Voltmeter are given for reference (values are in volts):

|  | $\underline{V_{E}}$ | $\underline{V_{B}}$ | $\underline{V_{C}}$ |
| :--- | :--- | :--- | :--- |
| Q1: | $\underline{-} .2$ | 0 | +4.4 |
| Q2: | +3.7 | +4.4 | +4.5 |
| Q3: | +4.5 | +4.4 | +0.04 |
| Q4: | 0 | 0 | +4.5 |
| Q5: | +4.5 | +4.5 | +0.06 |


|  | $\underline{V_{E}}$ | $\underline{V_{B}}$ | $\underline{V_{C}}$ |
| :---: | :---: | :---: | :---: |
| Q6: | 0 | 0 | +4.5 |
| Q7: | +4.5 | +4.5 | 0 |
| Q8: | -0.8 | $-0.8+12$ |  |

### 4.9 DETERMINATION OF CALIBRATION FIGURES FOR ALL FREQUENCY BANDS

Calibration data for the NM-37/57 should be determined at periodic intervals and especially subsequent to any maintenance or repair of the instrument. The calibration figures should be plotted on a calibration chart (Figure 2-8) and kept for reference. Follow the procedure given in the Calibration Data Accuracy Test (Test D) in able 4-1. Record the calibration figures for as many points in each frequency band as desired.

## Section V.

SCHEMATIC DIAGRAMS

## Section VI.

## 6. PARTS LIST

### 6.1 SINGER PARTS LIST

Pages 6-2 and 6-3 contain pictures of the top and bottom of the NM-37/57 chassis. Pages 6-4 through 6-53 contain all of the parts used by Singer by assembly.


Figure 6-1. Location of Main Assemblies (Top View)


Figure 6-2 . Location of Main Assemblies (Bottom View)

MAIN ASSEMBLIES

| Reference <br> Designator | Description | Singer <br> Part No. |
| :---: | :--- | :--- |
| A1 | Tuner 1 | $1-004126-001$ |
| A2 | Tuner 2 | $1-004127-001$ |
| A3 | Tuner 3 | $1-004128-001$ |
| A4 | Tuner 4 | $1-004129-001$ |
| A5 | Tuner 5 | $1-004130-001$ |
| A6 | Tuner 6 | $1-004131-001$ |
| A7 | Tuner 7 | $1-004132-001$ |
| A8 | Tuner 8 | $1-004133-001$ |
| A9 | Impulse Calibrator | $1-004099-001$ |
| A10 | Eight Position RF Switch | $4-003976-001$ |
| A11 | Five Position and Three Position IF | $1-004084-001$ |
|  | Switch |  |
| A12 | 160/Z0. 5 MHz IF Converter | $1-004273-001$ |
| A13 | 20.5 MHz IF Preamplifier | $1-004106-001$ |
| A14 | Bandwidth Selector | $1-004120-001$ |
| A15 | Linear IF and BFO | $1-004228-001$ |
| A16 | DC/DC Converter | $1-00421-001$ |
| A17 | Two Position RF Switch | $4-003962-001$ |
| A18 | FM Discriminator | $1-004272-001$ |
| A19, A20 | (Not Used) |  |
| A21 | Weighting Circuit and Meter Amplifier | $4-004114-005$ |
| A22 | Direct Peak Circuit | $4-004136-005$ |
| A23 | Slideback Peak Circuit | $4-004137-005$ |
| A24 | dB Readout \& Audio Amplifier | $4-004870-002$ |
| A25 | Remote Function Selector | $4-004139-005$ |
| A26 | Shaper 1 | $4-004140-005$ |
| A27 | Shaper 2 $\quad$ (Not Used) |  |
| A28 |  |  |
| A29 | Tuning Control |  |
| A30 | Band Selector | $4-004140-006$ |
| A31 | Voltage Regulator | $4-004143-005$ |
| A32 | Rectifier and Charge Regulator | $4-004727-001$ |
|  |  | $4-004041-005$ |
|  |  |  |

## TM 11-6625-2827-14\&P/TO 33A1-4-67-1

MAIN ASSEMBLIES (Continued)

| Reference Designator | Description | Singer <br> Part No. |
| :---: | :---: | :---: |
| A33 | Internal Sweep | 4-004095-005 |
| A34 | Frequency Readout | 4-004144-005 |
| A35-A40 | (Not Used)- |  |
| A41 | Log IF Amplifier | 1-004492-001 |
| A42 | Power Transformer | 2-403756-001 |
| A43 | (Not Used)- |  |
| A44 | Battery Pack | 4-003771-001 |
| A45 | Turret Attenuator | 1-003741-001 |
| A45* | Rotary Attenuator | 1-404129-001 |
| A46 | dB Meter | 4-403696-001 |
| A47 | Frequency Meter | 4-403695-001 |
| A48 | Voltage Controlled IF Attenuator | 1-004275-001 |

ASSEMBLY A1, TUNER 1


ASSEMBLY A1, TUNER 1 (Continued)

| REFERANCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q2 | Transistor | 1-958018-001 | RCA | 2N5179 | 1 |
| Q3 | Transistor | 1-958018-001 | RCA | 2N5179 | 1 |
| R1 | Resistor, Fixed, 1K | 1-945000-162 | Allen-Bradley | CB1025 | 1 |
| R2 | Resistor, Fixed, 8.2K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R3 | Resistor, Fixed 6.8K | 1-945000-182 | Allen-Bradley | CB6825 | 1 |
| R4 | Resistor, Fixed, 15 | 1-945000-118 | Allen-Bradley | CBI 505 | 1 |
| R5 | Same as RI |  |  |  |  |
| R6 | Resistor, Fixed, 820 | 1-945000-160 | Allen-Bradley | CB8215 |  |
| R7-R9 | Resistor, Fixed 12K | 1-945000-188 | Allen-Bradley | CB1235 | 1 |
| R10 | Same as R1 |  |  |  | 1 |
| R11 | Resistor, Fixed, 15K | 1-945000-190 | Allen-Bradley | CB1535 | 1 |
| R12 | Resistor, Fixed, 1.2K | 1-945000-164 | Allen-Bradley | CB1225 | 1 |
| R13 | Resistor, Fixed, 4.7K | 1-945000-178 | Allen-Bradley | CB4725 | 1 |
| R14 | Resistor, Fixed, 47 | 1-945000-130 | Allen-Bradley | CB4705 | 1 |
| R15 | Same as R1 |  |  |  | 1 |
| R16 | Resistor, Fixed, 39 | 1-945000-128 | Allen-Bradley | CB3905 |  |
| R17 | Resistor, Fixed, 27 | 1-945000-124 | Allen-Bradley | CBZ705 | 1 |
| R18 | Same as R16 |  |  |  | 1 |
| R19 | Same as R1 |  |  |  | 1 |
| R20 | Same as R13 |  |  |  | 1 |
| R21 | Resistor, Fixed, 3.3K | 1-945000-174 | Allen-Bradley | CB3325 |  |
| R22 | Same as R7 |  |  |  | 1 |
| R23 | Resistor, Fixed, 18K | 1-945000-192 | Allen-Bradley | CB1835 | 1 |
| R24 | Resistor, Fixed, 470 | 1-945000-154 | Allen-Bradley | CB4715 | 1 |
| R25 | Resistor, Fixed, 56 | 1-945000-132 | All(n-Bradley | CB5605 | 1 |
| R26 | Resistor, Fixed, 680 | 1-945000-158 | Allen-Bradley | CB6815 | 1 |
| R27 | Same as R12 | 1-945000-158 |  |  | 1 |
| T1 | Transformer | 2-004246-001 | Singer | 2-004246-001 | 1 |
| T2 | Transformer | 2-004244-001 | Singer | 2-004244-001 | 1 |
| T3 | Transformer | 2-004248-001 | Singer | 2-004248-001 | 1 |
| T4 | Transformer | 2-004247-001 | Singer | 2-004247-001 | 1 |
| T5 | Oscillator Coil | 2-004249-001 | Singer | 2-004249-001 | 1 |
|  |  | 6-7 |  |  |  |

ASSEMBLY A2, TUNER 2

| REFERANCE | $\begin{array}{l}\text { DESCRIPTION } \\ \text { DESIGNATOR }\end{array}$ | $\begin{array}{l}\text { SINGER } \\ \text { PART NUMBER }\end{array}$ | MANUFACTURER | MANUFACTURER |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PART NUMBER |  |  |  |  |$]$ QTY

[^0]ASSEMBLY A2, TUNER 2 (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R2 | Resistor, Fixed, 12K | 1-945000-188 | Allen-Bradley | CB1235 |  |
| R3 | Resistor, Fixed, 8.2K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R4 | Resistor, Fixed, 6.8K | 1-945000-182 | Allen-Bradley | CB6825 |  |
| R5 | Resistor, Fixed 10 | 1-945000-114 | Allen-Bradley | CB1005 | 1 |
| R6 | Same as RI |  |  |  |  |
| R7 | Resistor, Fixed, 1K | 1-945000-162 | Allen-Bradley | CB1025 | 1 |
| R8 | Same as R2 |  | Alen Bradey |  | , |
| R9 | Resistor, Fixed, 1K | 1-945000-162 | Allen-Bradley | CB1025 | 1 |
| R10 | Same as R2 |  |  |  | 1 |
| R11 | Resistor, Fixed, 15K | 1-945000-190 | Allen-Bradley | CB1535 | 1 |
| R 12 | Resistor, Fixed, 4.7K | 1-945000-178 | Allen-Bradley | CB4725 | 1 |
| R13 | Same as R1 |  |  |  | 1 |
| R14 | Resistor, Fixed, 47 | 1-945000-130 | Allen-Bradley | CB4705 | 1 |
| R15 | Not used |  |  |  |  |
| R 16 | Resistor, Fixed, 22 | 1-94500-122 | Allen-Bradley | CB2205 | 1 |
| R17 | Resistor, Fixed, 47 | 1-94500-130 | Allen-Bradley | CB4705 | 1 |
| R18 | Same as R16 |  |  |  | 1 |
| R19 | Same as R1 |  |  |  | 1 |
| R20 | Resistor, Fixed, 3.3K | 1-945000-174 | Allen-Bradley | CB3325 | 1 |
| R21 | Resistor, Fixed, 6.8K | 1-945000-182 | Allen-Bradley | CB6825 | 1 |
| R22 | Same as R2 |  |  |  | 1 |
| R23 | Resistor, Fixed, 18K | 1-945000-192 | Allen-Bradley | CB1835 | 1 |
| R24- | Resistor, Fixed, 470 | 1-945000-226 | Allen-Bradley | CB4715 | 1 |
| R25 | Resistor, Fixed, 56 | 1-945000-132 | Allen-Bradley | CB5601 | 1 |
| R26 | Resistor, Fixed, 820 | 1-945000-160 | Allen-Bradley | CB8211 | 1 |
| T1 | Transformer | 2-004252-001 | Singer | 2-004252-001 | 1 |
| T2 | Transformer | 2-004251-001 | Singer | 2-004251-001 | 1 |
| T3 | Transformer | 2-004253-001 | Singer | 2-004253-001 | 1 |
| T4 | Transformer | 2-004247-001 | Singer | 2-004247-001 | 1 |
| T5 | Transformer, Oscillator | 2-004254-001 | Singer | 2-004254-001 | 1 |
|  |  | 6-9 |  |  |  |

ASSEMBLY A3, TUNER 3


ASSEMBLY A3, TUNER 3 (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q1* | Transistor | 1-958064-001 | Amperex | A486 | 1 |
| Q2 | Transistor | 1-958018-001 | RCA | 2N5179 | 1 |
| Q3 | Transistor | 1-926018-001 | RCA | 2N5179 | 1 |
| Q4* | Transistor | 1-958064-001 | Amperex | A486 |  |
| $\begin{aligned} & \mathrm{R} 1,5,11, \\ & 11^{*}, 30,30^{*} \end{aligned}$ | Resistor, Fixed, 1K | 1-945000-162 | Allen-Bradley | CB1025 | 5 |
| R1** | Not used |  |  |  | 1 |
| R2, 16 | Resistor, Fixed, 12K | 1-945000-188 | Allen-Bradley | CB1235 | 2 |
| R3 | Resistor, Fixed, 8.2 K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R3** | Resistor, Fixed, 10K | 1-945086-087 | Allen-Bradley | BB1035 | , |
| R4** | Resistor, Fixed, 6.8K | 1-945000-182 | Allen-Bradley | CB6825 | 1 |
| R4** | Resistor, Fixed, 2.2 K | 1-945000-071 | Allen-Bradley | CB2225 | 1 |
| R5* | Resistor, Fixed, 220 | 1-945086-047 | Allen-Bradley | BB8215 | 1 |
| R6, 23, 25* | Resistor, Fixed, 820 | 1-945000-160 | Allen-Bradley | CB8215 | 3 |
|  | Not used Same as R2 |  |  |  | 2 |
| R9 | Resistor, Fixed, 15K | 1-945000-190 | Allen-Bradley | CB1535 | 1 |
| R10 | Resistor, Fixed, 4.7K | 1-945000-178 | Allen-Bradley | CB4725 |  |
| R12 | Resistor, Fixed, 47 | 1-945000-130 | Allen-Bradley | CB4705 | 1 |
| R13, 15 | Resistor, Fixed, 10 | 1-945000-114 | Allen-Bradley | CB1005 | 2 |
| R14 | Resistor, Fixed, 68 | 1-945000-134 | Allen-Bradley | CB6805 | 1 |
| R17 | Resistor, Fixed, 18K | 1-945000-192 | Allen-Bradley | CB1835 | 1 |
| R18 | Resistor, Fixed, 470 | 1-945000-154 | Allen-Bradley | CB4715 | 1 |
| R19 | Resistor, Fixed, 56 | 1-945000-132 | Allen-Bradley | CB5605 | 1 |
| R20, R21 | Resistor, Fixed, 10K | 1-945000-087 | Allen-Bradley | BB1035 | 2 |
| R22, 24 | Resistor, Fixed, 680 | 1-945000-158 | Allen-Bradley | CB6815 | 2 |
| R23* | Not used |  |  |  | 1 |
| R25 ${ }^{\text {R }}$ * | Resistor, Fixed, 820 | 1-945086-061 | Allen-Bradley | BB8215 | 1 |
| R26*, 29* | Same as R25 |  |  |  | 2 |
| R27* | Resistor, Fixed, 150 | 1-945086-043 | Allen-Bradley | BB1515 | 1 |
| R28* | Resistor, Fixed, 2.7 | 1-945086-001 | Allen-Bradley | BB27G5 | 1 |
| R30 | Same as R5 |  |  |  | 1 |
| T1 | Transformer | 2-004267-001 | Singer | 2-004267-001 | 1 |
| T2 | Transformer | 2-004268-001 | Singer | 2-004268-001 |  |
| T3 | Transformer | 2-004269-001 | Singer | 2-004269-001 | 1 |
| T4 | Transformer | 2-004247-001 | Singer | 2-004247-001 | , |
| T5 | Transformer, Oscillator | 2-004270-001 | Singer | 2-004270-001 | 1 |
| *Serial \#455 and above |  |  |  |  |  |
|  |  | 6-11 |  |  |  |

ASSEMBLY A4, TUNER 4

| $\begin{array}{c}\text { REFERENCE } \\ \text { DESIGNATOR }\end{array}$ | DESCRIPTION | $\begin{array}{c}\text { SINGER } \\ \text { PART NUMBER }\end{array}$ | MANUFACTURER | MANUFACTURER |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PART NUMBER |  |  |  |  |$]$ QTY

ASSEMBLY A4, TUNER 4 (Continued)

| $\begin{array}{c}\text { REFERENCE } \\ \text { DESIGNATOR }\end{array}$ | DESCRIPTION | $\begin{array}{c}\text { SINGER } \\ \text { PART NUMBER }\end{array}$ | MANUFACTURER | MANUFACTURER |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PART NUMBER |  |  |  |  |$]$ QTY

ASSEMBLY A5, TUNER 5

| $\begin{array}{c}\text { REFERENCE } \\ \text { DESIGNATOR }\end{array}$ | DESCRIPTION | $\begin{array}{c}\text { SINGER } \\ \text { PART NUMBER }\end{array}$ | MANUFACTURER | MANUFACTURER |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PART NUMBER |  |  |  |  |$]$ QTY

ASSEMBLY A5, TIIUNER 5 (Continued)

| $\begin{array}{c}\text { REFERENCE } \\ \text { DESIGNATOR }\end{array}$ | DESCRIPTION | $\begin{array}{c}\text { SINGER } \\ \text { PART NUMBER }\end{array}$ | MANUFACTURER | MANUFACTURER |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PART NUMBER |  |  |  |  |$]$ QTY

ASSEMBLY A6, TUNER 6


ASSEMBLY , TUNER 6 (Continued)


ASSEMBLY A7, TUNER 7

| $\begin{array}{c}\text { REFERENCE } \\ \text { DESIGNATOR }\end{array}$ | DESCRIPTION | $\begin{array}{l}\text { SINGER } \\ \text { PART NUMBER }\end{array}$ | MANUFACTURER | MANUFACTURER |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PART NUMBER |  |  |  |  |$]$ QTY

ASSEMBLY A7, TUNER 7 (Continued)

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \\ & \hline \end{aligned}$ | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q1 | Transistor | 1-958070-001 | Hewlett-Packard | 35821 E | 1 |
| Q2 | Transistor | 1-958072-001 | Fairchild | MT1038 | 1 |
| Q3 | Transistor | 1-958018-001 | RCA | 2N5179 | 1 |
| R1-R6 | Resistor, Variable, 20K | 1-945085-001 | Amphenol | 46D7364D | 6 |
| $\begin{aligned} & \text { R7-R10, 13-15, } \\ & 23-25,27 \end{aligned}$ | Resistor, Comp. 10K | 1-945000-186 | Allen-Bradley | CB1035 | 11 |
| R11, 16-18 | Resistor, Comp. 1.5K | 1-945000-166 | Allen-Bradley | CB1525 | 4 |
| R12 | Resistor, Comp. 1K | 1-945000-162 | Allen-Bradley | CB1025 | 1 |
| R19 | Resistor, Comp. 6.8 K | 1-945086-083 | Allen-Bradley | BB6825 | 1 |
| R20, 22 | Resistor, Comp. 10K | 1-945086-087 | Allen-Bradley | BB1035 | 2 |
| R21 | Resistor, Comp. 47 | 1-945086-055 | Allen-Bradley | BB4705 | 1 |
| R26 | Resistor, Comp. 51 | 1-945000-131 | Allen-Bradley | CB5105 | 1 |
| R28 | Resistor, Comp., 220 | 1-945000-146 | Allen-Bradley | CB2215 | 1 |
| R29 | Resistor, Comp., Selected, 10 | 1-945000-114 | Allen-Bradley | CB1005 | 1 |
| R29* | Resistor, Comp., Selected, 68 | 1-945000-134 | Allen-Bradley | CB6805 | 1 |
| T1 | Transformer | 3-004394-001 | Singer | 3-004394-001 | 1 |
| *Serial *339 and ab |  |  |  |  |  |

ASSEMBLY A8, TUNER 8

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \\ & \hline \end{aligned}$ | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1-C3 | Capacitor, Variable, 0.4-3pF | 1-900096-001 | Johanson | 5802 | 3 |
| C4, C5 | Capacitor, Variable, 1-IOpF | 1-900097-001 | Johanson | 5202 | 2 |
| C6 | Capacitor, Ceramic, 470pF | 1-900089-002 | Mucon | 2E470RM | 1 |
| C7-C9 | Capacitor, Feed Thru, 470pF | 1-900045-001 | Allen-Bradley | FA5C-4712 | 3 |
| C10 | Capacitor, Ceramic, 0.47pF | 1-900066-015 | Quality Components | MC-.47+10\% | 1 |
| CII-C13 | Same as C7 |  |  |  | 3 |
| C14 | Same as C6 |  |  |  | 1 |
| C15-C17 | Same as C7 |  |  |  | 3 |
| C18 | Same as C6 |  |  |  | 1 |
| C19-C21 | Same as C7 |  |  |  | 3 |

ASSEMBLY A8, TUNER 8 (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C22 | Not used |  |  |  |  |
| C23 | Capacitor, Mica, 5pF | 1-900098-005 | Elmenco | DM5-CC050K | 1 |
| C24 | Capacitor, Mica, 10pF | 1-900098-009 | Elmenco | EM5-CC100J | 1 |
| C25 | Capacitor, Mica, 50pF | 1-900098-023 | Elmenco | CM5-EC500J | 1 |
| C26, 227 | Sane as C7 |  |  |  | 2 |
| C28 | Same as C6 |  |  |  | 1 |
| C29 | Same as C23 Capacitor, Mica, 39pF | 1-900098-020 | Elmenco | DM5-EC930J | 1 |
| C31 | Not used |  |  |  |  |
| C32 | Same as C6 |  |  |  | 1 |
| ${ }^{\text {C33-C35 }}$ | Same as C7 |  |  |  | 3 |
| C36, C37 | Capacitor, Mica IpF | 1-900098-001 | Elmenco | EM5-CCOIOD | 2 |
| CR1-CR3 | Diode, Varactor | 1-913047-001 | Motorola | MV1864D | 3 |
| CR4, CR5 | Diode Varactor | 1-913049-002 | Hewlett-Packard | 5082-2900 | 2 |
| FL1-FLS* | Bead Ferrite | 1-906013-001 | Ferroxcube | 56-590-65/4B | 8 |
| J1iJ3 | Connector | 1-910139-001 | Sealectro | UG1464/U | 3 |
| L1 | Inductor | 1-103565-001 | Singer | 1-103565-001 | 1 |
| L2 | Inductor | 2-403275-001 | Singer | 2-403275-001 | 1 |
| L3 | Same as L1 |  |  |  | 1 |
| L4 | Choke, RF, 0.22pH | 1-906003-005 | Nytronics | 0-0.22 | 1 |
| L5 | Same as L1 |  |  |  | 1 |
| ${ }^{\text {L6 }}$ | Not used |  |  |  |  |
| $\stackrel{L 7}{ }$ | Choke, RF, 0.33, Inductor, L1.OH | 1-906003-007 | Nytronics Singer | ${ }_{1-403276-001}$ | 1 |
| $\llcorner 9$ | Choke, RF, 1.0pH | 1-906003-013 | Nytronics | DD-1.00 | 1 |
| L10 | Same as L8 |  |  |  | 1 |
| L11 | Inductor | 1-103566-001 | Singer | 1-103566-001 | 1 |
| P1 | Connector | 1-103549-001 | Singer | 1-103549-001 | 1 |
| Q1 ${ }^{\text {Q2 }}$ | Transistor Transistor | $\begin{aligned} & 1-958070-001 \\ & 1-958071-001 \end{aligned}$ | Hewlett-Packard Fairchild | $\xrightarrow{\text { HPA35821E }}$ MT1060A | 1 |
| *SERIAL 1440 AND | above |  |  |  |  |
|  |  | 6-20 |  |  |  |
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ASSEMBLY AS, TUNER 8 (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q3 | Transistor | 1-958018-001 | RCA | 2N5179 | 1 |
| RI-R6 | Resistor, Variable, 20K | 1-945085-001 | Amphenol | 46D7364D | 6 |
| R7, R9, R10 | Resistor, Comp. 10K | 1-945000-186 | Allen-Bradley | CB1035 | 3 |
| R8 | Resistor, Comp. 8.2K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R11 | Resistor, Comp. 1.5K | 1-945000-166 | Allen-Bradley | CB1525 | 1 |
| R12 | Resistor, Comp. 1K | 1-945000-162 | Allen-Bradley | CB1025 | 1 |
| R13-R15 | Same as R7 |  |  |  | 3 |
| R16, R17 | Same as RI1 |  |  |  | 2 |
| R18 | Resistor, Comp. 2. 2 K | 1-945000-170 | Allen-Bradley | CB2225 | 1 |
| R19, R20 | Resistor, Comp. 10K | 1-945086-087 | Allen-Bradley | BB1035 | 2 |
| R21 | Resistor, Comp. 470 | 1-945086-055 | Allen-Bradley | BB4715 | 1 |
| R22 | Same as R19 |  |  |  | 1 |
| R23-R25 | Same as R7 |  |  |  | 3 |
| R26 | Resistor, Comp. 51 | 1-945000-131 | Allen-Bradley | CB5105 | 1 |
| R27 | Same as R8 |  |  |  | 1 |
| R28 | Resistor, Comp. , Selected, 10 | 1-945000-114 | Allen-Bradley | CB1005 | 1 |
| T1 | Transformer | 3-004394-001 | Singer | 3-004394-001 | 1 |

ASSEMBLY A9, IMIPULSE CALIBRATOR
TM 11 -6625-28271 4\&P/TO 33A1 -4-67-1

| $\begin{aligned} & \text { REFERENCE } \\ & \text { DESIGNATOR } \end{aligned}$ | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1-C3 | Capacitor, Electrolytic, 10pF | 1-Q00057-119 | Sprague | 150D160X902OB22 | 3 |
| C4 | Capacitor, Ceramic, 0.15 pF | 1-90000-115 | Ampere | C280AE, 0. 15pF | 1 |
| C5, C6 | Capacitor, Mica, 390pF | 1-q00003-045 | Electromotive | DM15-391F | 2 |
| C7 | Capacitor, Mica, 24pF | 1-900071-007 | Elmenco | DM10-240J | 1 |
| C8-C10 | Capacitor, Ceramic, 0.OlpF | 1-900077-002 | Sprague | TG-S10 | 3 |
| C11 | Capacitor, Mica, 47pF | 1-900003-021 | Electromotive | DM15-470E | 1 |
| C12 | Capacitor (Selected at Test) | 1-900071-xxx | Elmenco | DM10- . XX |  |
| C13, C14 | Capacitor, Feed Thru, 1000pF | 1-9000045-002 | -Allen-Bradley | FA5C-102W | 2 |
| CRI | Diode, 2ener | 1-913054-108 | Motorola | 1N750A | 1 |
| CR2 | Diode | 1-913063-001 | CGE | 1N3716 |  |
| CR3 | Diode, Step-Recovery | 1-913049 004 | Hewlett-Packard | HP5082-0112 | 1 |
| CR4 | Diode, Hot Carrier | 1-913049-002 | Hewlett-Packard | 1IP5082-2900 | 1 |
| CR5 | Same as CR3 |  |  |  |  |

ASSEMBLY A9, IMPULSE CALIBRATOR (Continued)


ASSEMBLY A11, 5 POSITION AND 3 POSITION IF SWITCH CIRCUIT BOARD

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1-C8 | Capacitor, Feed Thru, 1000pF | 1-900045-002 | Allen-Bradley | FA5C-102W | 8 |
| C9-Cl1* | Capacitor, Mica, 8pF | 1-900098-008 | Electromotive | DM5-CCOBOK | 3 |
| C12, C13* | Capacitor, Mica 6pF | 1-900098-006 | Electromotive | DM5-CC060K | 2 |
| CR1-CR8 | Diode | 1-913056-001 | Motorola | 1N456A | 8 |
| K1-K8 | Relay | 1-942017-001 | Triridge | 206-00049 | 8 |

ASSEMBLY A12, 160/20.5 MH2 IF CONVERTER


ASSEMBLY A12, 160/20.5 MH2 IF CONVERTER (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C28 | Capacitor, Mica, 27pF | 1-900071-103 | Elmenco | DM10-270J | 1 |
| ${ }_{\text {C29 }} \mathrm{C} 30-\mathrm{C} 32$ | Not used Part of 22 |  |  |  |  |
| C33 | Capacitor, Mica, 33pF | 1-900071-104 | Elmenco | DM10-330J | 1 |
| C41 | Capacitor, Variable, 1-7pF | 1-900094-031 | Erie | 563-023 | 1 |
| C47* | Capacitor, Mica, 18pF | 1-900098-012 | Elmenco | DM5-180J | 1 |
| L1, L2 | Coil, Toroid, 0.06pH | 2-004335-001 | Singer | 2-004335-001 | 2 |
| L3-L6 | Inductor, 2.2 pH | 1-906016-017 | Lenox-Fugle | DR 2.2 | 4 |
| L7, L8 | Part of 21 |  |  |  |  |
| L9 , 11, | Inductor, 10pH | 1-906016-025 | Lenox-Fugle | DR 10 | 1 |
| $\begin{aligned} & \text { L10, 11, 17, } \\ & 18 \end{aligned}$ | Inductor, $0.33 y \mathrm{H}$ | 1-906016-007 | Lenox-Fugle | DR. 33 | 4 |
| L12, L13 | Part of 22 |  |  |  |  |
| L14 | Inductor, 0.15uH | 1-906016-003 | Lenox-Fugle | DR. 15 | 1 |
| L15, L16 | Inductor, 3.3pH | 1-906016-019 | Lenox-Fugle | DR 3.5 | 2 |
| L19, L20 | Inductor, 1 pH | 1-906016-013 | Lenox-Fugle | DR 1.0 | 2 |
| L21** | Inductor, 0.03pH | 2-004335-002 | Singer | 2-004335-002 | 1 |
| L22* | Inductor, 0.10 pH | 1-906003-001 | Nytronics | DDO. 10 | 1 |
| Q1-Q4 | Transistor | 1-958024-004 | RCA | 2 N 3932 | 4 |
| R1 | Resistor, Comp. 12K | 1-945000-188 | Allen-Bradley | CB1235 | 1 |
| R2 | Resistor, Carp. 2.7K | 1-945000-172 | Allen-Bradley | CB2725 | 1 |
| R3 | Resistor, Comp. IK | 1-945000-162 | Allen-Bradley | CbO1025 | 1 |
| R4 | Resistor, Camp. 33 | 1-945000-126 | Allen-Bradley | CB3305 | 1 |
| R5 | Resistor, Comp. 3.3K | 1-945000-174 | Allen-Bradley | CB3325 | 1 |
| R6, 8 | Resistor, Camp. 56 | 1-945000-132 | Allen-Bradley | CB5605 | 2 |
| R7 | Resistor, Comp. 510 | 1-945000-155 | Allen-Bradley | CB5115 | 1 |

*Serial t431 and above

ASSEMBLY A12, 160/20.5 MH2 IF CONVERTER (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R9 | Same as R7 |  |  |  | 1 |
| R10 | Resistor, Comp. 8.2K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R11 | Resistor, Comp. 4.7K | 1-945000-178 |  | CB4725 | 1 |
| R12 | Resistor, Variable, 100 | 1-945081-004 | Bourn | 3009P-1-101 | 1 |
| R13 | Resistor, Comp. 680 | 1-945000-158 | Allen-Bradley | CB6815 | 1 |
| R14 | Same as R5 |  |  |  | 1 |
| RIS, R16 | Resistor, Comp. 10 | 1-945000-114 | Allen-Bradley | CB1005 | 1 |
| R17 | Resistor, Comp. 150 | 1-945000-142 | Allen-Bradley | CB1515 | 1 |
| R1 | Resistor, Variable, 11K | 1-945081-007 | Bourn | 3009P--102 | 1 |
| R19 | Same as R4 |  |  |  | 1 |
| R20, R2I | Same as R17 |  |  |  | 2 |
| R22 | Same as R3 |  |  |  | 1 |
| R23 | Same as R2 |  |  |  | 1 |
| R24 | Resistor, Comp. 10K | 1-945000-186 | Allen-Bradley | CB1035 | 1 |
| Y1 | Crystal 69.75 MH 2 | 1-912004-001 | Pie2o | 4201-69.75 | 1 |
| 21, 27 | Filter | 1-00445-001 | Singer | 1-00445-001 | 2 |

ASSEMBLY A13, 20. 5 MH2 IF PREAMPLIFIER

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| , C2 | Capacitor, Ceramic, .001tF | 1-900076-001 | Erie | 5835-000 Y5UO-1032 | 2 |
| C3 | Capacitor, Variable, 8-35pF | 1-900095-104 | Johanson | 539-002-142D | 1 |
| C4 | Capacitor, Mica, 3pF | 1-900071-001 | Elmenco | DM10-030D | 1 |
| C5 | Capacitor, Mica, 56pF | 1-900071-105 | Elmenco | DM10-560J | 1 |
| C6 | Same as C3 |  |  |  | 1 |
| C7 | Capacitor, Mica, 18pF | 1-900071-107 | Elmenco | DM10-180J | 1 |
| C8, C9 | Same as C1 |  |  |  | 2 |
| C10 | Same as C3 |  |  |  | 1 |
| C11 | Capacitor, Mica, 180pF | 1-900071-106 | Elmenco | DM10-181 F | 1 |
| C12-C16 | Capacitor, Feed Thru, 1000pF | 1-900045-002 | Allen-Bradley | FA5C-102W | 5 |
| CR1-CR3 | Diode | 1-913056-001 | Motorola | 1N456A | 3 |
| K1-K3 | Relay | 1-942019-001 | Triridge | 206-00052 | 3 |

ASSEMBLY AI 3, 205 MTI2 IF PREAMIPLIIFIER (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1-L3 | Inductor,2. 22 H | 1-9-6016-017 | Lenox-Fugle | DR 2.2 | 3 |
| L4 | Inductor, 8.21uH | 1-906016-024 | Lenox-Fugle | DR 8.2 | 1 |
| L5, L6 | Inductor,6.8,F | 1-906016-023 | Lenox-Fugle | DR 6.8 | 2 |
| Q1, Q2 | Transistor | 1-958024-004 | RCA | 2N3932 |  |
| RI | Resistor, Film, 49.9 | 1-945027-068 | Corning | RN55-D-49R9F | 1 |
| R2 | Resistor, Comp. 12 K | 1-945000-188 | Allen-Bradley | CB1235 | 1 |
| R3 | Resistor, Comp. 2.7 K | 1-945000-172 | Allen-Bradley | CB2725 | 1 |
| R4 | Resistor, Comp. 560 | 1-945000-156 | Allen-Bradley | CB5615 | 1 |
| R5 | Resistor, Comp. 47 | 1-945000-130 | Allen-Bradley | CB4705 | 1 |
| R6 | Resistor, Comp. 3. 3K | 1-945000-174 | Allen-Bradley | CB3325 | 1 |
| R7 | Resistor, Variable, 500 | i-945081-006 | Bourn | 3009P-1-501 | 1 |
| R8 | Resistor, Comp. 8. 2 K | 1-945000-184 | Allen-Bradley | CB8225 |  |
| R9 | Resistor, Comp. 4.7K | 1-945000-178 | Allen-Bradley | CB4725 | 1 |
| R10 | Resistor, Comp. 680 | 1-945000-158 | Allen-Bradley | CB6815 | 1 |
| R11 | Same as R5 |  |  |  |  |
| R12 | Same as R6 |  |  |  | 1 |
| R13, R14 | Resistor, Film, 61.9 | 1-945027-077 | Corning | RN'55-D-61R9F | 2 |
| R15 | Resistor, Film, 249 | 1-945027-135 | Corning | RN55-D-2490F | 1 |
| TPI, TP2 | Terminal | 19-64109-001 | Lerco | 3535B | 2 |

ASSEMBLY A14, BANDSELECTOR

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER $\square$ | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{C} 1-\mathrm{C} 5 \\ & \mathrm{C} 6 \end{aligned}$ | Capacitor, Ceramic, .01.F Capacitor, Variable, 8-35pF | $\begin{aligned} & 1-900077-002 \\ & 1-900095-104 \end{aligned}$ | Sprague Johanson | $\begin{aligned} & \text { TGSO1 } \\ & 539-000-5 Y U 0- \\ & 1032 \end{aligned}$ | 5 |
| C7 | Capacitor, Mica, 200pF | 1-900071-016 | Elmenco | DM10 |  |
| C8, C9 | Capacitor, Ceramic, . 011 iF | 1-900077-02 | Spraque | TGSO1 | 2 |
| C10 | Capacitor, Feed Thru, 1000pF | 1-900045-002 | Allen-Bradley | FA5C-102W I |  |
| CII-C13 | Capacitor, Electrolstlc, IJIF | 1-900057-146 | Sprague | 150D105X0035A2 3 |  |
| C14-C19 | Not used |  |  |  |  |
| C20-C27 | Part of 723 |  |  |  |  |
| C28-C30 | Same as C10 | 3 |  |  |  |

ASSEMBLY A14, BANDWIDTII SEI.ECTOR (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| K1-K6 | Relay | 1-942017-001 | Triridge | 206-00049 | 6 |
| L1-L3 | Choke, 10pH | 1-906016-025 | Lenox-Fugle | DR 10 | 3 |
| L4 | Inductor, 2. 2H | 1-906016-017 | Lenox-Fugle | DR2. 2 | 1 |
| L5 | Inductor, 1.2plH | 1-906016-014 | Lenox-Fugle | DR 1.2 | 1 |
| L6-L8 | Same as LI |  |  |  | 3 |
| L9 | Not used |  |  |  |  |
| L10-L12 | Part of 23 |  |  |  |  |
| L13 | Not used |  |  |  |  |
| L14-L17 | Inductor, Selected | 1-906033-XXX | Lenox-Fugle |  | 2 |
| Q1, Q2 | Transistor Resistor, Comp. 51 | 1-958024-004 | RCA Allen-Bradley | 2N'3932 | 2 |
| R1 | Resistor, Comp. 51 Resistor, Comp. 8. 2 K | 1-945000-131 $1-945000-184$ | Allen-Bradley Allen-Bradley | CB5105 CB8225 | 1 |
| R3 | Resistor, Comp. 4.7K | 1-945000-178 | Allen-Bradley | CB4725 | 1 |
| R4 | Resistor, Comp. 10 | 1-945000-114 | Allen-Bradley | CB1005 | 1 |
| R5 | Resistor, Comp. 1 K | 1-945000-162 | Allen-Bradley | CB1025 | 1 |
| R6 | Resistor, Comp. 510 | 1-945000-155 | Allen- Bradley | CB5115 | 1 |
| R7-R9 | Resistor, Variable 500 | 1-945081-006 | Bourn | 3009P-1-501 | 3 |
| R10 | Same as R2 ${ }_{\text {Resistor, Comp. } 5.6 \mathrm{~K}}$ | 1-945000-180 | Allen-Bradley | CB5625 | 1 |
| R12 | Resistor, Comp. 33 | 1-945000-126 | Allen-Bradley | CB3305 | 1 |
| R13 | Same as R5 |  |  |  |  |
| R14 | Resistor, Conp. 3.3K | 1-945000-174 | Allen Bradley | CB3325 | 1 |
| 21 | Filter, Crystal 20.5 MH 2 , | 2-403209-001 | Singer | 2-403209-001 | 1 |
| 22 | Filter, Crystal $20.5 \mathrm{NMH2}$, | 2-403208-001 | Singer | 2-403208-001 | 1 |
| 23 | Filter Assembly, 1 NIH2 | 3-004118-001 | Singer | 3-004118-001 | 1 |
|  |  | 6-27 |  |  |  |

ASSEMBLY A15A1, LINEAR IF CIRCUIT BOMRD


ASSAMBLY A1 5AI, LINEAR IF CIRCUIT BOARD (Continued)

| REFERENCE <br> DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L9 | Inductor, 2.7yH | 1-906014-012 | Delevan | 1537.22 | 1 |
| P1 | Connector | 2-103549-001 | Singer | 2-103549-001 |  |
| Q1, Q2 | Transistor | 1-958018-001 | RCA | 2N5179 | 2 |
| Q3 ${ }^{\text {a }}$ | Transistor | 1-958056-001 | Texas Instr. | 2N5449 | 1 |
| R1 | Resistor, Comp. 27K | 1-945000-196 | Allen-Bradley | CB2735 |  |
| R2 | Resistor, Comp. 470 | 1-945000-154 | Allen-Bradley | CB4715 |  |
| R3 | Resistor, Comp. 1.8K | 1-945000-168 | Allen-Bradley | CB1825 | 1 |
| R4 | Not used. |  |  |  |  |
| R5 | Resistor, Comp. 22K | 1-945000-194 | Allen-Bradley | CB2235 | 1 |
| R6 | Resistor, Comp. 6.8 K | 1-945000-182 | Allen-Bradley | CB6825 | 1 |
| R7 | Resistor, Comp. 1K | 1-945000-162 | Allen-Bradley | CBIO2S | 1 |
| R8 | Resistor, Comp. 2. 2 K | 1-945000-170 | Allen-Bradley | CB2225 | 1 |
| R9 | Resistor, Comp. 18K | 1-945000-192 | Allen-Bradley | CB1835 | 1 |
| R10 | Resistor, Comp. 8. 2 K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R11 | Same as R7 |  |  |  | 1 |
| R12 | Resistor, Comp. 4.7K | 1-945000-178 | Allen-Bradley | CB4725 | 1 |
| R13 | Resistor, Comp. 15K | 1-945000-190 | Allen-Bradley | CB1535 | 1 |
| R14 | Resistor, Comp. 1.5Meg. | 1-945000-238 | Allen-Bradley | CB1555 | 1 |
| ${ }^{\text {R15 }}$ | Resistor, Comp. 10K | 1-945000-186 | Allen-Bradley | CB1035 | 1 |
| R16 | Resistor, Comp. 560 | 1-945000-156 | Allen-Bradley | CB5615 | 1 |
| R17 | Same as R3 ${ }_{\text {Resistor, Comp. } 56}$ | 1-945000-132 | Allen-Bradley | CB5605 | 1 |
| R19-R22 | Not used | 1-945000-132 | Alen-Bradey | CB5605 | 1 |
| R23 | Resistor, Comp. 100 | 1-945000-138 | Allen-Bradley | CB1015 | 1 |
| $\begin{aligned} & \text { R24-R28 } \\ & \text { R29 } \end{aligned}$ | Not used Same as R7 |  |  |  | 1 |
|  |  | 6-29 |  |  |  |

ASSEMBLY A15A2, BFO AND IF BUFFER CIRCUIT BOQRD

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1-C19 | Not used | - |  |  |  |
| C20 | Capacitor, Mica, 5pF | 1-90003-004 | Electromotive | nM15-050C |  |
| C21 | Capacitor, Mica 50pF | 1-900003-022 | Electromotive | DM15-500 |  |
| C22, C23 | Capacitor, Ceramic, 0.01pF | 1-900077-002 | Sprague | TSG10 |  |
| C24 | Capacitor, Electrolytic, 1pF | 1-900057-146 | Sprague | 150D105x0035A2 |  |
| C25 | Capacitor, Feed Thru, 1000pF | 1-900045-002 | Allen-Bradley | FA5C-102W |  |
| ${ }_{\text {C26 }} \mathrm{C} 310$ | Not used |  |  |  |  |
| C31 | Capacitor, Ceramic, 9-35pF | 1-900093-008 | Erie | 538-002-94R |  |
| C32 | Same as C22 |  |  |  |  |
| C33 | Not used | - |  |  |  |
| C35 | Capacitor, Mica, 3pF | 1-900003-003 | Electromotive | DM15 |  |
| C36, C37 | Not used |  |  |  |  |
| C38 | Capacitor, Mica, 10pF | 1-900003-0008 | Electromotive | DM15 |  |
| ${ }_{\text {L5 }}^{\text {L1-L4 }}$ | Not used Inductor, $2.2, \mathrm{H}$ | 1-906016-017 | Lenox-Fugle | DR 2.2 |  |
| L6 | Inductor, 6.8 BH | 1-906016-023 | Lenox-Fugle | DR 6.8 |  |
| Q1-Q3 | Not used |  |  |  |  |
| Q4 | Transistor Transistor | - $\begin{aligned} & \text { 1-958069-001 } \\ & 1-958018-001\end{aligned}$ | Texas Instr. | 2N5248 2N5179 |  |
| R1-R18 | Not used |  |  |  |  |
| R19 | Resistor, Comp. 10Meg | 1-945000-258 | Allen-Bradley | CB1065 |  |
| R20 | Resistor, Comp. 2.2K | 1-945000-170 | Allen-Bradley | CB2225 |  |
| R21 | Resistor, Comp. 5.6K | $1-945000-180$ $1-95500-162$ | Allen-Bradley | CB5625 |  |
| R22 | Resistor, Comp. 1 K Not used | 1-945000-162 | Allen-Bradley | CB1025 |  |
| R24 | Resistor, Comp. 5.6K | 1-945000-180 | Allen-Bradley | CB5625 |  |
| R25 | Resistor, Comp. 8.2K | 1-945000-184 | Allen-Bradley | CB8225 |  |
| R26 | Resistor, Comp. 680 | 1-945000-158 | Allen-Bradley | CB6815 |  |
| R27 | Resistor, Comp. 330 | 1-945000-129 | Allen-Bradley | CB3315 |  |
| R28 | Resistor, Comp. 43 | 1-945000-129 | Allen-Bradley | CB4305 |  |
| Y1 | Crystal, 20.501 MH 2 | 1-912005-001 | Pie2o | 4221-20.501 |  |
|  |  | 6-30 |  |  |  |

ASSEMBLY A16, DC TO DC CONVERTER

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1, C2 | Capacitor, Electrolytic, 10SF | 1-900057-152 | Sprague | 150D106X0035R2 | 2 |
| C3, C4 | Capacitor, Electrolytic, 4. 7iF | 1-900057-150 | Sprague | 1500D475X0035B2 | 2 |
| C5 | Capacitor, Electrolytic, 101F | 1-900057-119 | Sprague | 150D106X9020B2 | 1 |
| C6, C7 | Capacitor, Electrolytic, 1F | 1-900057-146 | Sprague | 150D105X0035A2 | 2 |
| C8, C 9 | Capacitor, Ceramic, 2200pF | 1-900131-029 | Arco | 3MCY-C-222K | 2 |
| C10, C11 | Capacitor, Mica, 1000pF | 1-900003-056 | Electromotive | DM15-102F | 2 |
| C12, C13 | Capacitor, Mylar, 1 F | 1-900001-125 | Amperex | C2BOAE, 1pF | 2 |
| C14 | Same as C3 |  |  |  | 1 |
| C15-C17 | Capacitor, Feed Thru, 1000pF1- | 00045-002 | Allen-Bradley | FA5C-102W | 3 |
| CIB | Capacitor, Ceramic, 0.005,uF | 1-900012-004 | Erie | 80125 U 5022 | 1 |
| CR1 | Diode, 2ener | 1-913054-111 | Motorola | 1 N735A | 1 |
| CR2 | Diode, Bridge Rectifier | 1-913046-001 | Motorola | MDA-920-4A |  |
| LI, L2 | Inductor, 1 MH | 1-906016-049 | Lenox-Fugle | DR 1000 | 2 |
| L3 | Inductor, 100MH | 1-906016-061 | Lenox-Fugle | DR 10, 000 | 1 |
| Q11 | Transistor | 1-958040-001 | Motorola | 2 N 3053 | 1 |
| Q2, Q3 | Transistor | 1-948056-001 | Texas Instr. | 2N5449 | 2 |
| Q4, Q5 | Transistor | 1-948065-001 | Motorola | MJ420 | 2 |
| R1 | Resistor, Comp. 2. 2 K | 1-945001-170 | Allen-Bradley | EB2225 | 1 |
| R2, R3 | Resistor, Comp. B. 2 K | 1-945000-184 | Allen-Bradley | CB8225 | 2 |
| R4 | Resistor, Variable, 500 | 1-945081-006 | Bourn | 3009P-1-501 | 1 |
| R5 | Resistor, Comp. 2. 7 K | 1-945000-172 | Allen-Bradley | CB2725 | 1 |
| R6, R7 | Resistor, Comp. 10 | 1-945000-114 | Allen-Bradley | CB1005 | 2 |
| R8 | Resistor, Comp. 10K | 1-945000-186 | Allen-Bradley | CB1035 | 1 |
| R9 | Not used |  |  |  |  |
| R10-R12 | Resistor, Comp. 390 | 1-945000-152 | Allen-Bradley | CB3915 | 3 |
| R13 | Resistor, Comp. 100K | 1-945000-210 | Allen-Bradley | CB1045 | 1 |
| T1 | Transformer | 3-004210-001 | Singer | 3-004210-001 | 1 |
| TP1-TP3 | Terminal | 1-964109-001 | Lerco | 3535B | 3 |
|  |  | 6-31 |  |  |  |
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ASSEMBLY A18, FM DISCRIMINATOR


ASSEMBLY 12l, WEIGHITING CIRCUIT AND METTER AMPLIFIER

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ARI-AR3 | Integrated Circuit | 1-926036-002 | Fairchild | UA741C | 3 |
| C1 | Capacitor, Mylar, 3pF | 1-900091-107 | Electro Cube | 625 BIA 305 J | 1 |
| C2 | Capacitor, Mylar, .47pF | 1-900001-121 | Amperex | ,C280AE, 0.47 F | 1 |
| C3, C4 | Capacitor, Electrolytic, 100F | 1-900039-004 | Gen. Inst. Corp. | '984-16 | 2 |
| CR1, CR2 | Diode | 1-913055-001 | Hewlett-Packard | ¥iP5082-2800 | 2 |
| R1 | Resistor, Comp. 1 K | 1-945000-162 | Allen-Bradley | CB1025 | 1 |
| R2, R3 | Resistor, Comp. 62K | 1-945000-205 | Allen-Bradley | CB6235 |  |
| R4 | Resistor, Film, 12. IK | 1-945088-297 | Corning | RN55-D-1212F | 1 |
| R5 | Same as RI |  |  |  | 1 |
| R6 | Resistor, Comp. 120 | 1-945000-140 | Allen-Bradley | CB1215 | 1 |
| R7, R8 | Resistor, Comp12 Meg | 1-945000-236 | Allen-Bradley | CB1265 | 1 |
| R9 | Same as R4 |  |  |  | 1 |
| R10 | Resistor, Film, 12. IK | 1-945027-297 | Corning | RN55-D-1212F | 1 |
| ${ }^{1} 11$ | Resistor, Variable, 100K | 1-945081-013 | Bourn | 3009P-1-104 | 1 |
| ${ }^{\mathrm{R} 12}$ | Resistor. Comp. 220K | 1-945000-218 | Allen-Bradley | CB2245 | 1 |
| R13 | Resistor, Variable, 2K | 1-945081-008 | Bourn | 3009P-1-202 | 1 |
| R14 | Resistor, Comp. 11 K | 1-945000-187 | Allen-Bradley | CB1135 | 1 |
| R15 R16 | Same as R10 ${ }_{\text {Resistor }}$ Comp 1.8 K | 1-945000-168 | Allen-Bradley | CB1825 | 1 |
| R17 | Resistor, Variable, 500 | 1-945081-006 | Bourn | 3009P-1-501 | 1 |
| R18 | Resistor, Comp. 1. 22 K | 1-945000-164 | Allen-Bradley | CB1225 | 1 |
| R19 | Same as R17 |  |  |  | 1 |
| $\begin{aligned} & \text { R20 } \\ & \text { R21, R22 } \end{aligned}$ | Resistor, Comp.3K Resistor, Variable,10K | $\begin{aligned} & 1-945000-173 \\ & 1-945081-010 \end{aligned}$ | Allen-Bradley Bourn | $\begin{aligned} & \text { CB3025 } \\ & 3009 P-1-103 \end{aligned}$ | 1 |
|  |  |  |  |  |  |
|  |  | 6-33 |  |  |  |
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ASSEMBLY A22, DIRECT PEAK CIRCUIT


ASSEMBLY A22, DIRECT PEAK ASSEMBLY (Continued)

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \\ & \hline \end{aligned}$ | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R11 | Resistor, Comp. 33 | 1-945000-126 | Allen-Bradley | CB2605 | 1 |
| R12 | Same as R3 |  |  |  | 1 |
| R13 | Resistor, Film, 12.1K | 1-945088-297 | Corning | RN55-D-1212F | 1 |
| R14 | Not used |  |  |  |  |
| R15 | Resistor, Variable, 500 | 1-945081-006 | Bourn | 3009P-1-501 | 1 |
| R16 | Resistor, Variable, 50 | 1-945081-003 | Bourn | 3009P-1-500 | 1 |
| R17 | Resistor, Comp. 56K | 1-945000-204 | Allen-Bradley | CB5635 | 1 |
| R18 | Resistor, Comp. 39 | 1-945000-128 | Allen-Bradley | CB3905 | 1 |
| R19 | Resistor, Comp. 9.1K(Selected at Test) | 1-945000-185 | Allen-Bradley | CB9125 | 1 |
| R20 | Same as R17 (Selected at Test) |  |  | 1 |  |
| R21 | Resistor, Comp. 470K (Selected1 at Test) | 945000-226 | Allen-Bradley | CB4745 | 1 |
| $\begin{aligned} & \text { R22 } \\ & \text { R23 } \end{aligned}$ | Resistor, Comp. 22 K Same as R17 | 1-945000-194 | Allen-Bradley | CB2235 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |

ASSEMBLY A23, SLIDEBACK PEAK CIRCUIT

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR1 | Integrated Circuit | 1-926036-002 | Fairchild | UA741C | 1 |
| C1 | Capacitor, Ceramic, .002F'F | 1-900012-013 | Erie | $871000 \times 5$ FO- 202 K | 1 |
| C2 | Capacitor, Mica, 500cF | 1-900003-048 | Electromotive | DM15-501F | 1 |
| C3 | Capacitor, Electrolytic, 2. 22F1 | 1-900057-111 | Sprague | 150D225X9020A2 | 1 |
| C4, C5 | Capacitor, Mylar, .015 F | 1-900001-103 | Amperex | C280AE, 0.015 F | 2 |
| C6 | Capacitor, Mylar, . liF | 1-900001-113 | Amperex | C280AE, O0. 1FIF | 1 |
| C7 | Capacitor, Mylar, .47pF | 1-900001-121 | Amperex | C280AE, 0.47BF | 1 |
| C8, $\mathrm{C9}$ | Capacitor, Electrolytic, 100001 | 1-900039-004 | Gen. Instr. Corp. | 984-1653 | 1 |
| CR1 | Diode, 2ener | 1-913054-115 | Motorola | 1N757A | 1 |
| CR2 | Diode, Stabistor | 1-913057-001 | Texas Instr. | G129 | 1 |
| CR3 | Diode | 1-913056-001 | Motorola | 1N456A | 1 |
| Q1 | Transistor | 1-958056-001 | Texas Instr. | 2N5449 | 1 |
| Q2, Q3 | Transistor, Set | 1-403190-001 | Singer | 1-403190-001 | 1 |
| Q4 | Transistor | 1-958053-001 | Fairchild | 2 N 4258 | 1 |
| Q5, Q6 | Same as Q1 |  |  |  | 2 |
| Q7, Q8 | Transistor Resistor Comp. 12 K | 1-958000-001 $1-945000-188$ | Motorola Allen-Bradley | $2 N 3904$ CB1235 | ${ }_{1}^{2}$ |
| R1 | Resistor, Comp. 12K | 1-945000-188 | Allen-Bradey |  |  |

ASSEMBLY A23, SLIDEBACK PEAK CIRCUIT (Continued)

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \end{aligned}$ | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R2 | Resistor, Comp. 1K | 1-945000-162 | Allen-Bradley | CBIO25 |  |
| R3 | Resistor, Comp. 100K | 1-945000-210 | Allen-Bradley | CB1045 | 1 |
| R4 | Same as R2 |  |  |  |  |
| R5 | Resistor, Film, 12. IK | 1-945088-297 | Corning | RN55-D-21212F | 1 |
| R6 | Resistor, Comp. 220 | 1-945000-146 | Allen-Bradley | CB2215 |  |
| R7 | Resistor, Comp. 2. 2K | 1-945000-170 | Allen-Bradley | CB2225 |  |
| R8 | Resistor, Comp. 3.9K | 1-945000-176 | Allen-Bradley | CB3925 | 1 |
| R9, R10 | Same as R2 |  |  |  | 2 |
| R11 | Resistor, Comp I Meg | 1-945000-234 | Allen-Bradley | CB1055 | 1 |
| R12 | Resistor, Comp. 2.2 Meg | 1-945000-242 | Allen-Bradley | CB2255 | 1 |
| R13 | Same as RI |  |  |  |  |
| R14, R15 | Resistor, Comp. 4.7 K | 1-945000-178 | Allen-Bradley | CB4725 | 2 |
| R16, R17 | Resistor, Comp. 68K | 1-945000-206 | Allen-Bradley | CB6835 | 2 |
| $R 18$ | Same as R14 |  |  |  |  |
| R19 | Resistor, Comp. 100K | 1-945000-186 | Allen-Bradley | CB1035 | 1 |
| R20 | Same as R2 |  |  |  |  |
| R21 | Resistor, Comp. 220K | 1-945000-218 | Allen-Bradley | CB2245 |  |
| R22 | Resistor, Comp. 22K | 1-945000-194 | Allen-Bradley | CB2235 |  |
| R23 | Same as R19 |  |  |  | 1 |
| R24 | Same as R22 |  |  |  | 1 |
| R25 | Same as R19 |  |  |  | 1 |
| R26 | Resistor, Variable, 50K | 1-945081-012 | Bourn | 3009P-1-503 |  |

ASSEMBLY A24, dB READOUT AND AUDIO AMPLIFIER

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \\ & \hline \end{aligned}$ | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1, C2 | Capacitor, Electrolytic, 100F | 1-900039-004 | Gen.Instr.Corp. | 984-1653 | 2 |
| C3 | Capacitor, Electrolytic, 0.22pF | 1-900001-117 | Amperex | C280AE, 0. 24F | 1 |
| CR1 | Not used |  |  |  |  |
| CR2-CR5 | Diode | 1-913007-001 | G.E. | IN4148 | 4 |
| CR6-CR10 | Diode | 1-913058-002 | Sylvania | 1N277 | 5 |

ASSEMBLY A24, dB READOUT AND AUDIO AMPLIFIER (Continued)


ASSEMBLY A25, REMOTE FUNCTION SELECTOR

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR1 | Integrated Circuit | 1-926036-002 | Fairchild | UA741C |  |
| C1 | Capacitor, Electrolytic, 1.O01F | 1-900057-146 | Sprague | 150D150X0035A2 | 1 |
| C2, C3 | Capacitor, Electrolytic, 100F | 1-900039-004 | Gen. Instr. Corp. | 984-1653 |  |
| CR1-CR8 | Diode | 1-913058-002 | Sylvania | 1N377 | 8 |
| CR9-CR11 | Diode | 1-913056-001 | Motorola | 1N456A | 3 |
| CR12-CR14 | Same as CRI |  |  |  | 3 |
| CR15 | Diode | 1-913057-001 | Texas Instr | G129 | 1 |
| K1-K3 | Relay, Reed | 1-942018-001 | Triridge | 206-00050 | 3 |
| R1-R3 | Resistor, Film 178K | 1-945027-409 | Corning | RN55-D-1783F | 3 |
| R4 | Resistor, Comp. 2.7K | 1-945000-172 | Allen-Bradley | CB2725 |  |
| R5 | Resistor, Variable, 20K | 1-945081-011 | Bourn | 3009P-1-203 |  |
| R6 | Same as RI |  |  |  | 1 |
| R7 | Resistor, Film, 1.5K | 1-945027-210 | Corning | RN55-D-1501F | 1 |
| R8 | Resistor, Film, 3.01K | 1-945027-239 | Corning | RN55-D-3011F | 1 |

ASSEMBLY A26, SHAPER 1

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR1-AR7 | Integrated Circuit | 1-926036-002 | Fairchild | UA741C | 7 |
| C1, C2 | CapaCitor, Electrolytic, 50fIF | 1-900039-008 | Gen. Instr. Corp. | 984-1655 | 2 |
| C3 | Capacitor, Mica, 100pF | 1-900003-030 | Electromotive | DMI5-IOIF | 1 |
| C4 | Capacitor, Mylar, . 22F | 1-900001-117 | Amperex | C280AE, 0. 224F | 1 |
| C5 | Same as C3 |  |  |  |  |
| C6 | Capacitor, Mylar, .O220IF | 1-900001-105 | Amperex | C280AE, 0.0221F | 1 |
| CR1-CR12 | Diode | 1-913059-001 | Texas Instr. | 1N626 | 12 |
| CR13 | Diode, 2ener | 1-913054-113 | Motorola | 1N755A | 1 |
| Q1, Q2 | Transistor | 1-958066-001 | Motorola | 2N4068 | 2 |
| Q3, Q4 | Transistor | 1-958065-001 | Motorola | MJ420 | 2 |
| R1-R6 | Resistor, Film, 15K | 1-945027-306 | Corning | RN55-D-1502F | 6 |
| R7 | Resistor, Film, 13K | 1-945027-300 | Corning | RN55-D-1302F | 1 |

ASSEMBLY A26, SHAPER 1 (Continued)
$\left.\begin{array}{l|l|l|l|l|l}\hline \text { REFERENCE } & \text { DESCRIPTION } & \text { SINGER } & \text { MANUFACTURER } & \text { MANUFFACTURER } \\ \text { DESIGNATOR } & & \text { QTY } \\ & & & & \text { PART NUMBER } & \\ \text { RART NUMBER }\end{array}\right]$

ASSEMBLY A27, SHAPER 2

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR1-AR7 | Integrated Circuit | 1-926036-002 | Fairchild | UA741C | 7 |
| C1, C2 | Capacitor, Electric, 50 F | 1-900039-008 | Gen. Instr. Corp. | 984-1655 | 2 |
| C3, 5 | Capacitor, Mica, 100 pF | 1-900003-030 | Electromotive | DM15-101F | 2 |
| C4 | Capacitor, Mylar, 22 F | 1-900001-117 | Amperex | C280AE, 0.22 F | 1 |
| C6 | Capacitor, Mylar, . 022 F | 1-900001-105 | Amperex | C280AE, 0.22 F | 1 |
| CR1-CR12 | Diode | 1-913059-001 | Texas Instr. | 1 N626 | 12 |
| CR13 | Diode, 2ener | 1-913054-113 | Motorola | 1 N 755 A | 1 |
| Q1, Q2 | Transistor | 1-958066-001 | Motorola | 2N4068 | 2 |
| Q3, Q4 | Transistor | 1-958065-001 | Motorola | M 4420 | 2 |
| R1-R6 | Resistor, Film, 15K | 1-945027-306 | Corning | FRN55-D-1502F | 6 |
| R7 | Resistor, Film, 13.3K | 1-945027-301 | Corring | RN55-D-1332F | 1 |
| R8 | Resistor, Film, 16.2K | 1-945207-309 | Corning | RN55-D-1622F | 1 |
| R9 | Resistor, Film, 20K | 1-945207-318 | Corning | RN55-D-2002F | 1 |
| R10 | Resistor, Film, 26.1 K Resistor Fim, a | $1-945207-329$ $1-945207-346$ | Corning | RN55-D-2612F | 1 |
| R12 | Resistor, Resistor, Film, Film 80.6K | 1-945027-376 | Corring | RN55-D-8062F | 1 |
| R13 | Resistor, Film, 33.2 K | 1-945027-339 | Corning | RN55-3322F | 1 |
| R13* | Resistor, Film, 31.6K | 1-945027-337 | Corning | RN55-D-3162F | 1 |
| R14 | Resistor, Film, 76.8 K | 1-945027-374 | Corning | RN55-D-7682F | 1 |
| R14* | Resistor, Film, 105K | 1-945027-387 | Corning | RN55-D-1053F | 1 |
| R15 | Resistor, Film, 127K | 1-945027-395 | Corning | RN55-D-1273F | 1 |
| R15* | Resistor, Film, 100K | 1-945027-385 | Corning | RN55-D-1003F | 1 |
| ${ }^{\text {R16 }}$ | Resistor, Film, 110 K | 1-944027-389 | Corring | RN55-D-1103F | 1 |
|  | Resistor, Film, 86.6K | 1-945027-379 | Corring | RN55-D-8662F | 2 |
| R17* | Resistor, Film, 78.7K | 1-944027-375 | Corring | RN55-D-7872F | 1 |
| R18 ${ }_{\text {R18* }}$ | Resistor, Film, 88.7 K Resistor, Film, 127 K | 1-945027-380 $1-945027-395$ | Corning | RN55-D-8872F | 1 |
| R19 | Resistor, Film, 113K | 1-945027-390 | Corning | RN55-D-1133F | 1 |
| R20 | Resistor, Film, 56.2 K | 1-945027-361 | Corning | RN55-D-5622F | 1 |
| R21 | Resistor, Film, 36.5 K | 1-945027-343 | Corning | RN55-D-3652F | 1 |
| R22 | Resistor, Film, 27.4 K | 1-945027-331 | Corning | RN55-D-2742F | 1 |
| R23 | Resistor, Film, 21.5K | 1-945027-321 | Corning | RN55-D-2152F | 1 |
| R24 | Resistor, Film, 200k | 1-945027-414 | Corning | RN55-D-2003F | 1 |
| R25 R26 | Resistor, Comp., 6.8K | 1-945000-182 | Allen-Bradley | CB6825 | 1 |
| R26 R27 | Resistor, Comp., 7.5K | 1-945000-183 | Allen-Bradley | CB7525 | 1 |
| R27 | Resistor, Comp., 8.2K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| * SERIAL \#522 AND | Above |  |  |  |  |
|  |  | 6-40 |  |  |  |

ASSEMBLY A27, SHAPER 2 (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R28 | Resistor, Comp., 9. 1K | 1-945000-185 | Allen-Bradley | CB9125 | 1 |
| R29 | Resistor, Comp., 10K | 1-945000-186 | Allen-Bradley | CB1035 | 1 |
| R30 | Resistor, Comp., 122K | 1-945000-188 | Allen-Bradley | CB1235 I |  |
| R31 | Resistor, Variable, 50K | 1-945081-012 | Bourn | 3009P-1-503 | 1 |
| R32 | Same as R29 |  |  |  | 1 |
| R33 | Same as R26 |  |  |  | 1 |
| R34, R35 | Same as R29 |  |  |  | 1 |
| R36 | Resistor, Comp., 330K | 1-945000-222 | Allen-Bradley | CB3345 | 1 |
| R37 | Same as R25 |  |  |  | 1 |
| R38 | Same as R36 |  |  |  | 1 |
| R39 | Resistor, Film, 73.2K | 1-945027-372 | Corning | RN55-D-7372F | 1 |
| R40 | Resistor, Variable, 5K | 1-945081-009 | Bourn | 3009P-1-502 | 1 |
| R41 | Resistor, Comp., 150 | 1-945000-142 | Allen-Bradley | CB 515 | 1 |

ASSEMBLY A29, TUNING CONTROL


ASSEMBLY A29, TUNING CONTROL (Continued)

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \\ & \hline \end{aligned}$ | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R10 | Same as R3 |  |  |  | 1 |
| R11 | Resistor, Comp., 22K | 1-945000-194 | Allen-Bradley | CB2235 | 1 |
| R12 | Resistor, Film, 4.99K | 1-945027-260 | Corning | RN55--4991F | 1 |
| R13 | Resistor, Film, 1.24K | 1-945027-202 | Corning | RN55-D-1241F | 1 |
| R14 | Resistor, Comp., 220 | 1-945000-146 | Allen-Bradley | CB2215 | 1 |
| R15, R16 | Resistor, Comp., 10 | 1-945000-114 | Allen-Bradley | CB1005 | 2 |
| R17 | Sane as R2 |  |  |  | 1 |
| R18 | Resistor, Variable, 10K | 1-945081-010 | Bourn | 3009P-1-103 | 1 |
| R19 | Resistor, Comp., 1.8M | 1-945000-240 | Allen-Bradley | CB1855 | 1 |

ASSEMBLY A30, BAND SELECTOR

| REFERENCE | DESCRIPTION | SINGER <br> DESIGNATOR | MANUFACTURER | MANUFACTURER <br> PART NUMBER | QTY |
| :--- | :---: | :--- | :--- | :--- | :---: |
|  |  |  |  |  |  |
| CR1-CR8 | Diode | $1-913058-002$ | Sylvania | 1N277 | 8 |
| CR9-R16 | Diode | $1-913056-001$ | Motorola | 1N456A | 8 |
| K1-K8 | Relay | $1-942018-001$ | Triridge | 206-00071 | 8 |
|  |  |  |  |  |  |

ASSEMBLY A31, VOLTAGE REGULATOR

| REFERENCE <br> DESIGNATOR | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER <br> PART NUMBER | QTY |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |
| AR1, AR2 | Integrated Circuit | $1-926040-001$ | Bell \& Ibwell | 20-007C | 2 |
| C1, C2 | Capacitor, Electrolytic, 2gF | $1-900057-154$ | Sprague | 150D226X0035R2 | 2 |
| C3, C4 | Capacitor, Electrolytic, 150,F | $1-900057-191$ | Sprague | 150D157X9015S2 | 2 |
| C5, C6 | Capacitor, Mylar, 022wF | $1-900001-005$ | Amperex | C280AE, 0.022\&4F | 2 |
| C7 | Capacitor, Mica, 470pF | $1-900003-047$ | Electromotive | DM15-471F | 1 |
| C8 | Capacitor, Electrolytic, IpF | $1-900057-146$ | Sprague | 150D105X0035A2 | 1 |
| C9, C10 | Capacitor, Ceramic, .01F | $1-900077-002$ | Sprague | TGS10 | 2 |
| CR1 | Diode, 2ener | $1-913054-108$ | Motorola | 1N750A | 1 |
| CR2 | Diode, 2ener | $1-913054-110$ | Motorola | 1N752A | 1 |
| CR3 | Diode, 2ener | $1-913060-001$ | Motorola | 1N827A | 1 |
|  |  |  |  |  |  |

ASSEMBLY A31, VOLTAGE RECGUIATOR (Continued)

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \\ & \hline \end{aligned}$ | DESCRIPTION | $\begin{gathered} \text { SINGER } \\ \text { PART NUMBER } \end{gathered}$ | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q11 | Transistor | 1-958039-001 | Motorola | 2N3055 |  |
| Q2 | Transistor | 1-958012-009 | Motorola | 2N4901 | 1 |
| Q3 | Transistor | 1-958040-001 | Motorola | 2N3053 | 1 |
| Q4 | Transistor | 1-958023-002 | RCA | 2N4037 |  |
| Q5, Q6 | Transistor | 1-958000-001 | Motorola | 2N3904 | 2 |
| Q7 | Same as Q3 |  |  |  |  |
| Q8 | Same as Q4 |  |  |  |  |
| R1 R2 | Resistor, Comp., 2.2 K | 1-945001-170 | Allen-Bradley | EB2225 | 2 |
| R3, R4 | Resistor, Comp., 100 | 1-945000-138 | Allen-Bradley | CB1015 | 2 |
| R5, R6 | Resistor, W/W, 1 | 1-945079-001 | Dale | RS-2A | 2 |
| R7, R8 | Resistor, Comp. , 10K | 1-945000-186 | Allen-Bradley | CB1035 | 2 |
| R9 | Resistor, Comp. , 2.7K | 1-945000-172 | Allen-Bradley | CB2725 | 1 |
| R10 | Not used |  |  |  |  |
| R11 | Resistor, Film, 768 | 1-945016-182 | Corning | RN60-D-7680F | 1 |
| R12-R15 | Resistor, Film, 2.67 K | 1-945016-234 | Corning | RN60-D-2671F | 4 |
| R16 | Resistor, Film, 2.87 K | 1-945016-237 | Corning | RN60-D-2871F | 1 |
| R17 | Resistor, Film, 8.06K | 1-945016-280 | Corning | RN60-D-8061F | 1 |
| R18 | Resistor, Variable, 500 | 1-945081-006 | Bourn | 3009P-1-501 | , |
| R19 | Resistor, Variable, 100 | 1-945081-004 | Bourn | 3009P-1-101 | 1 |

ASSEMBLY A32, RECTIFIER AND CHARGE REGULATOR


ASSEMBLY A32, RECTIFIER AND CHARGE REGULATOR (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R3, R4 | Resistor, Comp., 2. 2 K | 1-945002-170 | Allen-Bradley | GB2225 | 2 |
| R5, R6 | Resistor. Comp. 2220 | 1-945001-146 | Allen-Bradley | EB2215 | 2 |
| R7, RB | Resistor, W/W, 25 | 1-945080-101 | Dale | RH 10 | 2 |
| R9, R10 | Resistor, Variable, 25 | 1-945074-002 | Ohmite | 210-1009 | 2 |
| R11, R12 | Resistor, Comp., 39 | 1-945002-128 | Allen-Bradley | GB3905 | 2 |
| R13 | Resistor, Comp., 4.3K | 1-945000-177 | Allen-Bradley | CB4325 | 1 |
| R14 | Resistor, Variable, 2 K | 1-945081-008 | Bourn | 3009P-1-202 | 1 |
| ASSEMBLY A33, INTERNAL SWEEP |  |  |  |  |  |
| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| AR1-AR3 | Integrated Circuit | 1-926036-002 | Fairchild | UA741C | 3 |
| C1 | Capacitor, Electrolytic, 1001F | 1-900039-004 | Gen. Instr. Corp. | 984-1653 | 1 |
| C2 | Capacitor, Ceramic, . OOiF | 1-900001-130 | Amperex | C280AE, 0. 001,F | 1 |
| C3 | Capacitor, Ceramic, . 00220 F | 1-900001-134 | Amperex | C280AE, $0.002+\mathrm{F}$ | 1 |
| C4, C5 | Capacitor, Electrolytic, 1leF | 1-900057-146 | Sprague | 150D105X0035A2 | 2 |
| CR1 | Diode | 1-913056-001 | Motorola | IN456A | 1 |
| CR2 | Diode | 1-913058-002 | Sylvania | IN277 | 1 |
| CR3 | Same as CRI |  |  |  | 1 |
| K1 | Relay, Reed | 1-942020-001 | Triridge | 206-00070 | 1 |
| R1 | Potentiometer, 10K | 1-945081-010 | Bourn | 3009P-1-103 | 1 |
| R2 | Resistor, Comp., 1.8 Meg | 1-945000-240 | Allen-Bradley | CB1855 | 1 |
| R3 | Resistor, Comp., IOOK | 1-945000-210 | Allen-Bradley | CB1045 | 1 |
| R4 | Resistor, Comp., 39K Same as RI | 1-945000-200 | Allen-Bradley | CB3935 | 1 |
| R6 | Same as R3 |  |  |  | 1 |
| R7 | Resistor, Comp., 33K | 1-945000-198 | Allen-Bradley | CB3335 | 1 |
| R8, R9 | Resistor, Comp., 47K | 1-945000'202 | Allen-Bradley | CB4735 | 2 |
| R10 | Resistor, Comp., 470K | 1-945000-226 | Allen-Bradley | CB4745 | 1 |
| R11 | Same as R8 |  |  |  | 1 |
| R12 | Resistor, Comp., 390K | 1-945000-224 | Allen-Bradley | CB3945 | 1 |
| R13 | Resistor, Comp. , 270K | 1-945000-220 | Allen-Bradley | CB2745 | 1 |
| R14 | Resistor, Comp., 220 | 1-945000-146 | Allen-Bradley | CB2215 | 1 |
|  |  | 6-44 |  |  |  |

ASSEMBI Y A34, FREQUENCY READOUT


ASSEMBLY A41, LOG IF AMPLIFIER

| $\begin{array}{l}\text { REFERENCE } \\ \text { DESIGNATOR }\end{array}$ | DESCRIPTION | $\begin{array}{l}\text { SINGER } \\ \text { PART NUMBER }\end{array}$ | MANUFACTURER | MANUFACTURER |
| :--- | :--- | :--- | :--- | :--- | :--- |
| PART NUMBER |  |  |  |  |$]$ QTY

ASSEMBLY A41, LOG IF AMPLIFIER (Continued)

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \\ & \hline \end{aligned}$ | DESCRIPTION | SINGER <br> PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C39 | Same as C2 |  |  |  | 1 |
| C40, C41 | Capacitor, Electric | 1-90039-001 | Gen. Intsr. Corp. | 984-2203 | 2 |
| C42, C 43 | Same as C2 |  |  |  | 2 |
| C44 | Capacitor, Mica, 100pF | 1-900003-030 | Electromotive | DM15-101F | 1 |
| C44* | Not Used |  |  |  |  |
| C45 | Capacitor, Mica, 180pF | 1-900003-036 | Electromotive | DM15-181F | 1 |
| C46, C47 .001pF | Capacitor, Feed-thru, | 1-900038-001 | Allen-Bradley | FB2B-1034 | 2 |
| C47* | Same as C4 |  |  |  |  |
| J1 | Connector, BNC | 1-910132-002 | Kings | UG-1094/U | 1 |
| J2 | Not Used |  |  | - |  |
| J3-J5 | Same as J1 |  |  |  | 3 |
| L1 | Coil, Variable | 2-403341-001 | Singer | 2-403341-001 | 1 |
| $\begin{aligned} & \mathrm{L} 2,4,8, \\ & 10,12 \end{aligned}$ | Choke, RF, 33pH | 1-906022-001 | Nytronics | 13-33-10 | 6 |
| $\begin{aligned} & \llcorner 3,5,7, \\ & 9,11 \end{aligned}$ | Choke, RF, 2.2pH | 1-906022-002 | Nytronics | 10-2.2-10 | 5 |
| L13, L14 | Same as L3 |  |  |  | 2 |
| L15 | Choke, RF, 10pH L16 | $\begin{aligned} & \text { 1-906022-005 } \\ & \text { Choke, RF } 1.2 \mathrm{pH} \end{aligned}$ | Nytronics 1-9060220004 | 13-10-10 Nytronics | 1 |
| 10-1.2-10 | ${ }_{1} 17$ | Choke, RF, 2.7pH | 1-906022-003 | Nytronics |  |
| 10-2.7-10 | 1 |  |  |  |  |
| Q1-Q4 <br> NPN Silicon | Transistor, Dual | 1-958077-001 | Motorola | MD918 | 4 |
| $\begin{aligned} & \text { Q5 } \\ & \text { Q6-Q8 } \end{aligned}$ | Transistor Same as Q1 | 1-958078-001 | Texas Instr. | 2N4997 | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ |
| Q9, Q10 | Transistor | 1-958000-102 | Motorola | 2N3906 | 2 |
| Q11 | Transistor | 1-958000-001 | Motorola | 2N3904-5 | 1 |
| R1-R7 | Resistor, Variable, 2.5K | 1-945008-105 | Singer | 1-945008-105 | 7 |
| R8 | Potentiometer, 500 | 1-945096-002 | CTS | M176WL501A | 1 |
| R9 | Potentiometer, 200 | 1-945096-001 | CTS | M176WL201A | 1 |
| $\begin{aligned} & \text { R10, 16, 20, 22, } \\ & 26,28,32,39, \end{aligned}$ | Resistor, Comp., 510 | 1-945000-155 | Allen-Bradley | CB5115 | 12 |
| $\begin{aligned} & \text { R11, 17, 23, 29, } \\ & 33,36,42,48 \end{aligned}$ | Resistor, Comp., 1K | 1-945000-162 Allen- | Bradley | CB1025 | 8 |
| *SERIAL \#473 AND | ABOVE |  |  |  |  |
|  |  | 6-47 |  |  |  |

ASSEMBLY A41, LOG IF AMPLIFIER (Continued)

| $\begin{aligned} & \hline \text { REFERENCE } \\ & \text { DESIGNATOR } \end{aligned}$ | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R11* | Resistor, Film, 866 | 1-945027-182 | Allen-Bradley | CC 1/4-8660F | 1 |
| $\begin{aligned} & \text { R12, 18, 24, 30, } \\ & 37,43,49 \end{aligned}$ | Resistor, Comp., 20 | 1-945000-121 | Allen-Bradley | CB2005 | 7 |
| $\begin{aligned} & \text { R13, } 19,25,31 \text {, } \\ & 38,44,50 \text {, } \end{aligned}$ | Resistor, Comp., 33 | 1-945000-126 | Allen-Bradley | CB3305 | 7 |
| R14 | Same as R10 |  |  |  | 7 |
| $\begin{aligned} & \text { R14**,20*, } 26^{*}, \\ & 32^{\star}, 39^{*}, 45^{\star}, 51 \end{aligned}$ | Resistor, Comp., 270 | 1-945000-148 | Allen-Bradley | CB2715 | 7 |
| $\begin{aligned} & \text { R15, 21, 27, } 34, \\ & 40,46,52 \end{aligned}$ | Resistor, Comp., 100K | 1-945000-210 | Allen-Bradley | CB1045 | 7 |
| R17 | Same as R11 |  |  |  | 6 |
| $\begin{aligned} & \text { R17*, } 23^{*}, 29^{\star} \\ & 36^{\star}, 42^{*}, 48^{*} \end{aligned}$ | Resistor, Film, 1K | 1-945027-193 | Allen-Bradley | CC 1/4-100IF | 1 |
| R53 | Resistor, Comp., 8. 2 K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R54 | Resistor, Comrp., 15K | 1-945000-190 | Allen-Bradley | CB1535 | 1 |
| R55 | Resistor, Comp., 330 | 1-945000-150 | Allen-Bradley | CB3315 | 1 |
| R56 | Resistor, Comp., 560 | 1-945000-156 | Allen-Bradley | CB5615 | 1 |
| R57 | Resistor, Comp., 6.8 K | 1-945000-182 | Allen-Bradley | CB6825 | 1 |
| R58 | Resistor, Comp., 2.2K | 1-945000-170 | Allen-Bradley | CB2225 | 1 |
| R59 | Resistor, Comp., 220 | 1-945000-146 | Allen-Bradley | CB2215 | 1 |
| R60 | Resistor, Comp., 330 | 1-945000-150 | Allen-Bradley | EB3315 | 1 |
| R61 | Resistor, Comp., 150 | 1-945001-142 | Allen-Bradley | EB1515 | 1 |
| R62 | Resistor, Comp., 82 | 1-945000-136 | Allen-Bradley | CB8205 | 1 |
| R63 | Resistor, Film, 332 | 1-945016-147 | Corning | RN60-D-3320F | 1 |
| R64 | Resistor, Film, 60.4 | 1-945016-076 | Corning | RN60-D-60R4F | 1 |
| R65 | Resistor, Comp., 820 | 1-945000-160 | Allen-Bradley | CB8215 | 1 |
| * SERIAL \#473 | ND ABOVE |  |  |  |  |


| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BT1, BT2 CB1, CB2 | Battery <br> Circuit Breaker, 2 Arp | $\begin{aligned} & \text { 2-403172-001 } \\ & 1-024008-007 \\ & \hline \end{aligned}$ | Singer <br> Littlefuse | $\begin{aligned} & \text { 2-403172-001 } \\ & 815002 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \\ & \hline \end{aligned}$ |

ASSEMBLY A48, VOLTAGE CONTROLLED IF ATTENUATOR

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR1 | Integrated Circuit | 1-926041-001 | Fairchild | UA4747 | 1 |
| C1, C2 | Capacito, Electrolytic, $50 \mu \mathrm{~F}$ | 1-900039-008 | Gen. Instr. Corp. | 984-1655 | 2 |
| C3-C7, C12 | Capacitor, Ceramic, $0.01 \mu \mathrm{~F}$ | 1-900077-002 | Sprague | TGS10 | 5 |
| C8-C11 | Capacitor, Feed Thru, 1000pF | 1-900045-002 | Allen-Bradley | TA5C-102W | 4 |
| CR1, CR2 | Diode | 1-913049-005 | Hewlett-Packard | HP5082-3039 | 2 |
| L1-L3 | Inductor, $8.2 \mu \mathrm{H}$ | 1-906016-024 | Lenox-Fugle | DR8.2 | 3 |
| R1 | Resistor, Variable, 1K | 1-945078-005 | Allen-Bradley | JA1N048P502AA | 1 |
| R2, R3 | Resistor, Film, 2K | 1-945027-222 | Corning | RN55-D-20D1F | 2 |
| R2, R3** | Resistor, Film, 1.78K | 1-945027-217 | Corning | RN55-D-1781F |  |
| R4 | Resistor, Film, 178K | 1-945027-409 | Corning | RN55-D-1783F | 1 |
| R5 | Resistor, Film, 10K | 1-945027-289 | Corning | RN55-D-1002F | 1 |
| R6, R7 | Resistor, Film, 19.1K | 1-945027-316 | Corning | RN55-D-1912F | 2 |
| R8, R9 | Resistor, Film, 95.3K | 1-945027-383 | Corning | RN55-D-9532F | 2 |
| R10 | Resistor, Comp., 8.2K | 1-945000-184 | Allen-Bradley | CB8225 | 1 |
| R11 | Resistor, Film, 10.5K | 1-945027-291 | Corning | RN55-D-1052F | 1 |
| R12, R13 | Resistor, Film, 49.9 | 1-945027-068 | Corning | RN55-D-49R9F | 2 |
| C12* | Not Used |  |  |  |  |
| C13, C14* | Capacitor, Ceramic, $0.01 \mu \mathrm{~F}$ | 1-90077-002 | Sprague | TGS10 |  |

* SERIAL \#325 AND ABOVE
** SERIAL \#340 AND ABOVE


## CHASSIS PARTS

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Attenuator, Pad, 13dB | 1-972004-013 | Texcan | FP-50 | 1 |
|  | Bail | 1-964118-005 | Buckeye | MP40016-5 | 1 |
|  | Bandpass Filter, 160 MHz | 2-403210-001 | Singer | 2-403210-001 | 1 |
|  | Board, Meter Assembly | 1-004288-001 | Singer | 1-004288-001 | 1 |
|  | Cable, AC Power | 1-910166-001 | Belden | KH 7375 | 1 |
|  | Capacitor, Blocking | 3-004387-001 | Singer | 3-004387-001 | 1 |
|  | Connector, Amphenol, 5 Socket | 1-910032-010 | Amphenol | 126-223 | 1 |
|  | Connector, Amphenol, 9 Socket | 1-910157-208 | Amphenol | 126 | 1 |
|  | Connector | 1-910167-001 | TT Cannon | DEM-98 | 16 |
|  | Connector, PC Board | 1-910155-002 | Viking | VH18/1AB | 11 |
|  | $\begin{aligned} & \text { Connector, PC Board (A25, } \\ & \text { A29, A30) } \end{aligned}$ | 1-910155-001 | Viking | 2VH18/1AN | 3 |
|  | Extender | 4-004224-005 | Singer | 4-004224-005 | 1 |
|  | Extractor, Circuit Board | 2-103537-001 | Singer | 2-103537-001 | 1 |
|  | Filter, Low Pass, 1 GHz | 2-403362-001 | Lark | LSF1000-4HG | 1 |
|  | Foot, Front Left | 1-964117-001 | Buckeye | PP40012-1 | 1 |
|  | Foot, Front Right | 1-964117-002 | Buckeye | PP40021-2 | 1 |
|  | Foot, Polyethylene | 1-964119-001 | 1W1/Cortland |  | 2 |
|  | Knob, AFC | 1-935024-001 | Buckeye | RSS-70TSL-2 | 1 |
|  | Knob, Attenuator (dB) | 2-403258-002 | Singer | 2-403258-002 | 1 |
|  | Knob, Attenuator | 1-935030-001 | Singer | 1-935030-001 | 1 |
|  | Knob, Audio (Black) | 1-935024-001 | Buckeye | RSS-70TSL-2 | 1 |
|  | Knob, Audio (Red) | 1-935024-001 | Buckeye | RSS-50L-1 | 1 |
|  | Knob, Band (MHz) | 1-935024-001 | Buckeye | RSS-70TSL-2 | 1 |
|  | Knob, Bandwidth (MHz) | 1-935024-001 | Buckeye | RSS-50L-1 | 1 |
|  | Knob, Calibrate | 1-935025-001 | Buckeye | RSSN-70-2 | 1 |
|  | Knob, Control Mode | 1-035023-001 | Buckeye | RSSN-70TSL-2 | 1 |
|  | Knob, Fine Tube | 1-935024-001 | Buckeye | RSS-50L-1 | 1 |
|  | Knob, Function | 1-935023-001 | Buckeye | RSSN-70TSL-2 | 1 |
|  | Knob, Power | 1-935023-001 | Buckeye | RSSN-70TSL-2 | 1 |
|  | Knob, Slideback Peak | 1-935002-002 | Buckeye | RSS-70-2 | , |
|  | Knob, Tune | 1-935021-001 | Buckeye | RSSN-125SP-2 | 1 |
| AD1 | Adapter | 1-910175-001 | Sealectro | 50-073-0000 | 1 |
| AD2 | Adapter, Tee | 1-910162-001 | Sealectro | 50-085-000 | 1 |

CHASSIS PARTS (Continued)

| REFERENCE DESIGNATOR | DESCRIPTION | SINGER PART NUM | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1-C7 | Capacitor, Feed Thru, 1000pF | 1-900038-001 | Allen-Bradley | FB2B-102W | 7 |
| C8, C9 | Capacitor, Electrolytic, $2600 \mu \mathrm{~F}$ | 1-900102-037 | Sprague | 36D262G050AB2A | 2 |
| C10, C11 | Capacitor, Electrolytic, 1500 F | 1-900040-006 | Gen. Instr. Corp. | 977-92 | 2 |
| C12, C26 | Capacitor, Electrolytic, $50 \mu \mathrm{~F}$ | 1-900040-005 | Gen. Instr. Corp. | 977-207 | 2 |
| C13 | Same as C10 |  |  |  | 1 |
| C14, C23 | Same as C1 |  |  |  | 11 |
| C24, C25 | Capacitor, Feed Thru, 470pF | 1-900079-001 | Allen-Bradley | FW5N-1501 | 2 |
| C27-C32 | Capacitor, Ceramic, $0.01 \mu \mathrm{~F}$ | 1-900077-002 | Sprague | TGS10 |  |
| CR1-CR8 | Diode | 1-913058-002 | Sylvania | 1N277 | 8 |
| F1, F2 | Fuse | 1-924000-014 | Bussman | MDL-25V,0.5A | 2 |
| FH1, FH2 | Fuseholder | 1-924007-001 | Littlefuse | 341001 | 2 |
| J1 | Connector, Jack, BNC (part of the Blocking Capacitor) |  |  |  |  |
| J2 | Connector, Jack, BNC (part of W39) |  |  |  |  |
| J3 | Connector, Jack, BNC (part of W36) |  |  |  |  |
| J4 | Connector, Jack, BNC (part of W31) |  |  |  |  |
| J5 | Connector, Jack 3 Pins | 1-910165-001 | Switchcraft | EAC-301 | 1 |
| J6 | Connector, Jack, BNC | 1-910132-001 | Kings | UG-1094A/U | 1 |
| J7 | Connector, Jack, Phone | 2-004364-001 | Singer | 2-004364-001 | 1 |
| J8 | Connector, Jack, Phone | 2-004477-001 | Singer | 2-004477-001 | 1 |
| J9 | Connector, 41 Pins | 1-910161-001 | Bendix | 21-203220-41P | 1 |
| J10 | Connector, Jack, BNC (part of W35) |  |  |  |  |
| J11 | Connector, Jack, BNC | 1-910132-001 | Kings | UG-1094A/U | 1 |
| J12 | Connector, Jack, Phone | 2-004363-001 | Singer | 2-004363-001 | 1 |
| J13 | Connector, Jack, 5 Pins | 1-910157-003 | Anphenol | 126-216 |  |
| J14 | Connector, Box Mounting | 1-901206-001 | ITT Cannon | KPSE02E10-6S | 1 |
| L1 | Choke, RF | 1-906003-049 | Nytronics | DD-1000 | 1 |
| R1 | Resistor, Variable, 1K | 1-945102-004 | Beckman | 7216R1KL. 25 | 1 |
| R2 | Part of S6 | - | - | - | - |
| R3 | Resistor, Variable, 10K | 1-945078-108 | Allen-Bradley | JA1N048P1034A | 1 |
| R4 | Part of S7 | - | Corning | RN55-D-9530F | - |

CHASSIS PARTS (Continued)

| REFERANCE DESIGNATOR | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R5 | Resistor, Film 953 | 1-945027-191 | Corning | RN55-D-9530F | 1 |
| R6 | Resistor, Comp., 47 | 1-945001-130 | Allen-Bradley | EB4705 | 1 |
| R7 | Resistor, Comp.,1K | 1-945001-162 | Allen-Bradley | EB1025 | 1 |
| S1 | Switch | 4-403214-001 | Singer | 4-403214-001 | 1 |
| S2, S3 | Switch | 4-043212-001 | Singer | 4-03212-001 | 1 |
| S4 | Switch (Part of A45) | - | - | - | - |
| S5 | Switch | 4-043213-001 | Singer | 4-403213-001 | 1 |
| S6, R2 | Switch and Variable Resistor | 1-403215-002 | Singer | 1-403215-002 | 1 |
| S7, R4 | Switch and Variable Resistor | 1-403215-001 | Singer | 1-403215-001 | 1 |
| S8 | Switch | 1-951035-001 | Switchcraft | 923 | 1 |
| S9 | Switch | 4-403244-001 | Singer | 4-403244-001 | 1 |
|  |  | 4-403217-001 | Singer | 4-403217-001 | 1 |
|  |  | 1-951034-002 | CTS | Series 212 | 1 |
| S10 | Switch, Slider | 1-951029-001 | Switchcraft | 46256LF | 1 |
| S11 | Switch | 1-951036-007 | C\&K Components | 7203 | 1 |
| W1 | Cable, RF Input | 2-004389-001 | Singer | 2-004389-001 | 1 |
| W1** | Cable, RF Input | 2-005509-001 | Singer | 2-005509-001 | 1 |
| W2 | Cable, Rigid | 2-004391-001 | Singer | 2-004391-001 | 1 |
| W2** | Cable, Rigid | 2-005510-001 | Singer | 2-005510-001 | 1 |
| W3 | Cable, 15 inches | 2-004284-006 | Singer | 2-004284-003 | 1 |
| W4 | Cable, 6 inches | 2-004282-001 | Singer | 2-004282-001 | 1 |
| W5 | Cable, 8 inches | 2-004286-003 | Singer | 2-004286-003 | 1 |
| W6 | Cable, 10 inches | 2-004282-002 | Singer | 2-004282-002 | 1 |
| W7 | Cable, 7 inches | 2-004286-002 | Singer | 2-004286-002 | 1 |
| W8, w9 | Cable, 21 inches | 2-004285-003 | Singer | 2-004285-003 | 2 |
| W9*** | Cable, | 2-004285-004 | Singer | 2-004285-004 | 1 |
| W10 | Cable, Extension | 2-003434-001 | Singer | 2-003434-001 | 1 |
| W11, W12 | Cable, 14 inches | 2-004286-004 | Singer | 2-004286-004 | 4 |
| W12*** | Cable | 2-004286-007 | Singer | 2-004286-007 | 1 |
| W13 <br> Low-Pass Filter | Cable, 14 inch, with | 3-004555-001 | Singer | 3-004555-001 | 1 |

[^1]CHASSIS PARTS (Continued)

| $\begin{aligned} & \hline \text { REFERANCE } \\ & \text { DESIGNATOR } \end{aligned}$ | DESCRIPTION | SINGER PART NUMBER | MANUFACTURER | MANUFACTURER PART NUMBER | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| W13* | Cable, 14 inch | 2-004286-008 | Singer | 2-004286-008 | 1 |
| W14 | Same as W11 | 1 |  |  |  |
| W14*** | Cable | 2-004286-009 | Singer | 2-004286-009 | 1 |
| W15-W18 | Cable, 14 inches | 2-004285-001 | Singer | 2-004285-001 | 4 |
| W16*** | Cable | 2-004285-005 | Singer | 2-004285-005 | 1 |
| W17*** | Cable | 2-004285-006 | Singer | 2-004285-006 | 1 |
| W18*** | Cable | 2-004285-007 | Singer | 2-004285-007 | 1 |
| W19 | Cable | 2-004392-001 | Singer | 2-004392-001 | 1 |
| W20 | Cable | 2-004393-001 | Singer | 2-004393-001 | 1 |
| W21, W22 | Cable, 8 inches | 2-004287-003 | Singer | 2-004287-003 | 2 |
| W22*** | Cable | 2-004287-005 | Singer | 2-004287-005 | 1 |
| W23 | Cable, $61 / 2$ inches | 2-004287-002 | Singer | 2-004287-002 | 1 |
| W24, W25 | Cable, 5 inches | 2-004287-001 | Singer | 2-004287-001 | 2 |
| W25*** | Cable | 2-004287-004 | Singer | 2-004287-004 | 1 |
| W26 | Same as W5 | - | - | - | 1 |
| W26*** | Cable | 2-004286-006 | Singer | 2-004286-006 | 1 |
| W27, W28 | Cable, 6 inches | 2-004286-001 | Singer | 2-004286-001 | 2 |
| W28*** | Cable | 2-004286-005 | Singer | 2-004286-005 | 1 |
| W29 | Cable | 2-004393-002 | Singer | 2-004393-002 | 1 |
| W30 | Cable | 2-004393-003 | Singer | 2-004393-003 | 1 |
| W31 | Cable, 12 inches | 2-004284-002 | Singer | 2-004284-002 | 1 |
| W32 | Cable, 6 inches | 2-004285-001 | Singer | 2-004285-001 | 1 |
| W33 | Cable, 15 inches | 2-004713-001 | Singer | 2-004713-001 | 1 |
| W34 | Not used |  |  |  |  |
| W35 | Cable, 8 inches | 2-004284-001 | Singer | 2-004284-001 | 1 |
| W36 | Cable, 8 inches | 2-004283-001 | Singer | 2-004283-001 | 1 |
| W37 | Cable, 18 inches | 2-004282-004 | Singer | 2-004282-004 | 1 |
| W38 | Not used |  |  |  |  |
| W39 | Cable, 15 inchs | 2-004282-003 | Singer | 2-004284-003 | 1 |
| W40*** | Cable, 15 inches | 2-004863-001 | Singer | 2-004863-001 | 1 |

[^2]
### 6.2 PART NUMBER-NATIONAL STOCK NUMBER CROSS REFERENCE INDEX

National Stock Numbers (NSN) that are missing from the Part Number-National Stock Number Cross Reference Index have been applied for and will be added to this TM by future Change/Revision when they are entered in the Army Master Data File (AMDF). Until the NSNs are established and published, submit exception requisitions to: Commander, US Army Communications-Electronics Command and Fort Monmouth, ATTN: AMSEL-MM, Fort Monmouth, New Jersey 077035007 for the part required to support your equipment.

| PART NUMBER NATIONAL STOCK NUMBER CROSS REFERENCE INDEX |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PART NUMBER | FSCM | NATIONAL STOCK NUMBER | PART NUMBER | FSCM | NATIONAL STOCK NUMBER |
| BB1035 | 01121 | 5905-00-492-7607 | CB2735 | 01121 | 5905-00-911-3815 |
| BB4705 | 01121 | 5905-00-900-1138 | CB2745 | 01121 | 5905-00-911-3819 |
| BB4715 | 01121 | 5905-00-912-1834 | CB3025 | 01121 | 5905-00-577-9453 |
| CB1005 | 01121 | 5905-00-960-0099 | CB3305 | 01121 | 5905-00-915-3152 |
| CB1015 | 01121 | 5905-00-102-5294 | CB3315 | 01121 | 5905-00-114-0710 |
| CB1025 | 01121 | 5905-00-097-9533 | CB3325 | 01121 | 5905-00-909-3967 |
| CB1045 | 01121 | 5905-00-959-1202 | CB3345 | 01121 | 5905-00-485-4545 |
| CB1055 | 01121 | 5905-00-116-8554 | CB3905 | 01121 | 5905-00-498-6059 |
| CB1135 | 01121 | 5905-00-989-3753 | CB3915 | 01121 | 5905-00-907-4118 |
| CB1215 | 01121 | 5905-00-119-8812 | CB3925 | 01121 | 5905-00-141-0743 |
| CB1225 | 01121 | 5905-00-919-5713 | CB3935 | 01121 | 5905-00-907-4119 |
| CB1235 | 01121 | 5905-00-106-1278 | CB3945 | 01121 | 5905-00-115-3562 |
| CB1505 | 01121 | 5905-00-905-6277 | CB4305 | 01121 | 5905-00-400-8999 |
| CB1515 | 01121 | 5905-00-119-8811 | CB4325 | 01121 | 5905-00-909-3796 |
| CB1525 | 01121 | 5905-00-990-5559 | CB4705 | 01121 | 5905-00-104-8368 |
| CB1535 | 01121 | 5905-00-904-5689 | CB4715 | 01121 | 5905-00-911-3752 |
| CB1555 | 01121 | 5905-00-111-1684 | CB4725 | 01121 | 5905-00-911-3753 |
| CB1825 | 01121 | 5905-00-905-6279 | CB4735 | 01121 | 5905-00-960-0126 |
| CB1835 | 01121 | 5905-00-911-3801 | CB4745 | 01121 | 5905-00-909-3815 |
| CB1855 | 01121 | 5905-00-800-8068 | CB4765 | 01121 | 5905-00-905-6631 |
| CB2005 | 01121 | 5905-00-135-3972 | CB5105 | 01121 | 5905-00-909-3834 |
| CB2205 | 01121 | 5905-00-989-2843 | CB5115 | 01121 | 5905-00-116-2394 |
| CB2215 | 01121 | 5905-00-683-2240 | CB5601 | 01121 | 5905-00-755-0797 |
| CB2225 | 01121 | 5905-00-436-9299 | CB5605 | 01121 | 5905-00-133-0440 |
| CB2235 | 01121 | 5905-00-911-3810 | CB5615 | 01121 | 5905-00-105-7768 |
| CB2245 | 01121 | 5905-00-105-7765 | CB5625 | 01121 | 5905-00-909-3862 |
| CB2255 | 01121 | 5905-00-402-4256 | CB5635 | 01121 | 5905-00-913-9415 |
| CB2705 | 01121 | 5905-00-113-4860 | CB6235 | 01121 | 5905-00-972-0039 |
| CB2725 | 01121 | 5905-00-111-4727 | CB6805 | 01121 | 5905-00-911-3758 |


| PART NUMBER • NATIONAL STOCK NUMBER CROSS REFERENCE INDEX |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PART NUMBER | FSCM | NATIONAL STOCK NUMBER | PART NUMBER | FSCM | NATIONAL STOCK NUMBER |
| CB6815 | 01121 | 5905-00-911-3763 | G130 | 01295 | 5905-00-454-6241 |
| CB6825 | 01121 | 5905-00-577-9455 | HP5082-2800 | 28480 | 5961-00-252-1309 |
| CB6835 | 01121 | 5905-00-716-4852 | JA35J1 | 15801 | 5905-00-892-6925 |
| CB6845 | 01121 | 5905-00-104-8357 | MDA9421 | 04713 | 5961-00-011-6774 |
| CB7525 | 01121 | 5905-00-911-3779 | MD918 | 04713 | 5961-00-105-0982 |
| CB8205 | 01121 | 5905-00-104-8363 | MJ420 | 04713 | 5961-00-494-4929 |
| CB8211 | 01121 | 5905-00-119-8768 | MV1862D | 04713 | 5961-01-065-8076 |
| CB8215 | 01121 | 5905-00-918-6522 | SG22 | 03877 | 5961-00-581-9700 |
| CB8225 | 01121 | 5905-00-104-8358 | TE1211 | 56289 | 5910-00-827-1209 |
| CB8235 | 01121 | 5905-00-916-7267 |  |  |  |
| CB9125 | 01121 | 5905-00-359-4133 | TGS10 | 56289 | 5910-00-810-4849 |
| CB9135 | 01121 | 5905-00-904-5672 | TGS20 | 56289 | 5910-00-603-5906 |
| DM15C200J | 72136 | 5910-00-723-5267 | 1N3716 | 03508 | 5961-00-947-7275 |
| DM15C240J | 72136 | 5910-00-686-6171 | 1 N4001 | 04713 | 5961-00-921-3781 |
| DM15E270J | 72136 | 5910-00-725-7420 | 1 N 4004 | 04713 | 5961-00-106-6991 |
| DM15E330J | 72136 | 5910-00-957-2054 | 1N5148A | 04713 | 5961-00-110-0919 |
| DM15E560J | 72136 | 5910-00-8051137 | 1 N627 | 01295 | 5961-00-577-6181 |
| DM15F101J | 72136 | 5910-00-649-2914 | 1N750A | 04713 | 5961-00-071-9254 |
| DM15F621F | 72136 | 5910-00-7550011 | 1N751A | 04713 | 5961-00-114-1833 |
| DM15F621J | 72138 | 5910-00-543-9305 | 1N752A | 04713 | 5961-00-995-2310 |
| DM15F681F | 72136 | 5910-00-712-8688 | 1N755A | 04713 | 5961-00-068-2000 |
| DM15F820F | 72136 | 5910-00-727-2291 | 1 1 916B | 01295 | 5961-00-904-5355 |
| EB1025 | 01121 | 5905-00-907-4125 | 150D105X0035A2 | 56289 | 5910-00-726-5003 |
| EB1515 | 01121 | 5905-00-055-6140 | 150D106X0015B2 | 56289 | 5910-00-113-5475 |
| EB2215 | 01121 | 5905-00-104-3850 | 150D106X0035R2 | 56289 | 5910-00-236-8766 |
| EB2225 | 01121 | 5905-00-141-1163 | 150D106X9020B2 | 56289 | 5910-00-936-1522 |
| EB3315 | 01121 | 5905-00-192-3971 | 150D157X9015S2 | 56289 | 5910-00-717-6628 |
| EB4715 | 01121 | 5905-00-111-4858 | 150D225X9020A2 | 56289 | 5910-00-177-2581 |
| FA5C-4712 | 01121 | 5910-00-958-8401 | 150D226X0015B2 | 56289 | 5910-00-807-7253 |
| G129 | 01295 | 5961-00-103-7420 | 150D226X0035R2 | 56289 | 5910-00-752-4249 |


| PART NUMBER - NATIONAL STOCK NUMBER CROSS REFERENCE INDEX |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PART NUMBER | FSCM | NATIONAL STOCK NUMBER | PART NUMBER | FSCM | NATIONAL STOCK NUMBER |
| 150D336X9010B2 <br> 150D475X0035B2 <br> 150D476X9020R2 <br> 2N2646 <br> 2N3053 <br> 2N3055 <br> 2N3646 <br> 2N3904 <br> 2N3905 <br> 2N3906 <br> 2N4221 <br> 2N4258 <br> 2N4901 <br> 2N5248 <br> 2N5449 <br> 275-1-201 <br> 275-1-501 <br> 3009P-1-500 <br> 341001 <br> 35821E <br> 36D262G050AB2A <br> 46256LF <br> 5C023105X0250B3 <br> 50-073-0000 <br> 50-085-0000 <br> 5082-2900 <br> 5202 | 56289 56289 03508 04713 07263 04713 04713 04713 07263 04713 01295 80294 80294 28480 56289 82389 91293 98291 98291 28480 91293 | 5910-00-722-4117 5910-00-007-2004 5961-00-912-1177 5961-00-985-9073 5961-00-985-9074 $59611-00-062-3133$ $5961-00-892-8706$ 5961-00-847-9782 5961-00-931-0372 $5961-00-104-5855$ $5961-00-217-7849$ 5961-00-780-8368 5961-00-488-7376 5961-00-137-4383 5905-00-752-7116 $5905-00-660-6067$ $5905-01-005-9596$ 5920-00-568-0926 $5961-01-012-6688$ $5910-00-401-2838$ $5910-00-401-2838$ $5930-00-059-1390$ 5910-00-933-4887 5910-00-152-8196 5985-00-972-3149 $5961-00-110-7491$ $5910-00-105-7660$ | $\begin{aligned} & \text { 625B1A105J } \\ & 6604 \\ & 7203 \\ & 56-590-65 / 4 B \\ & \text { BB1515 } \\ & \text { BB27GS } \\ & \text { CB2715 } \end{aligned}$ | $\begin{aligned} & 14752 \\ & 72825 \\ & 09335 \\ & 02114 \\ & 01121 \\ & 01121 \\ & 01121 \end{aligned}$ | 5910-00-182-8198 5940-00-259-7929 5930-00-110-0495 5938-00-491-6515 5905-00-470-0369 5905-00-494-5891 5905-00-577-9678 |

## 6-57 (6-58 blank)

## APPENDIX A.

## REFERENCES

DA Pam 310-1 Consolidated Index of Army Publications and Blank Forms.

DA Pam 738-750
TM 750-244-2
The Army Maintenance Management System (TAMMS).
Procedures for Destruction of Electronics Materiel to Prevent Enemy Use (Electronics Command).
A-1/(A-2 blank)

## APPENDIX B.

## Battery Supplementary Information

## B-1 The Nickel-Cadmium (NiCd) Battery

The NiCd battery has the following qualities:
a. May be recharged hundreds of times.
b. Nearly constant discharge potential during its normal operating cycle.
c. Excellent charge retention.
d. Good low temperature characteristics.
e. Rugged, sealed construction; can take much abuse.
f. May stand for long periods of time in either charged or discharged state without any adverse effects.

## B-2 NiCd Battery Discharge Characteristics

The discharge voltage is quite flat and should remain within the range of 1.20 volts to 1.25 volts per cell for approximately $80 \%$ of its normal operating range ( 1.25 volts to 1.10 volts). Cells should not be discharged under load to extremely low voltage. Recharging should be started when cell voltage reaches 1.10 volts under load. The low end of the battery meter scale operating range is based on the 1.1 volt point. The cell voltage under normal load drops very rapidly with time when below the 1.1 volt output level.

## B-3 Normal Battery Cycle Life

The life of the cell or battery is based on the drain and nature of its discharge cycles. If the battery is only partially discharged ( $1 / 2$ to $3 / 4$ of its capacity) on each cycle, then the number of cycles possible before the battery's usefulness is ended is extended.

Where discharges completely exhaust a cell, the cycle life can be considerably less. Where the recommended cut-off of 1.1 volts is observed hundreds of cycles should be obtained. Also, when cells are operated according to recommended procedure, termination of cell life will not be sudden. Rather, a gradual decline in capacity will result, allowing replacement on an orderly schedule.

## APPENDIX B. (Continued)

## B-4 Battery Life

The battery is capable of operating the equipment for 8 hours from a fully charged condition to the point at which the battery meter indicates below the low end of the operating range. It has been found that if the battery has been operated throughout a large number of charge/discharge cycles (all within the $50 \%$ to $100 \%$ of full-charge range) the battery capacity apparently decreases by $10 \%$ or $15 \%$. However, this loss is normally regained after 3 or 4 sequential cycles from full-charge to the lower operating range point on the battery meter scale.

## B-5 Temperature Characteristics

NiCd batteries are not recommended for use beyond the range of $-15^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}\left(+5^{\circ} \mathrm{F}\right.$ to $\left.+122^{\circ} \mathrm{F}\right)$. The following tabulation indicates the effect of temperature on the service life of NiCd batteries discharged at a "10 Hour Rate."

| Discharge Temperature | Approximate Percent of <br> $+21.1^{\circ} \mathrm{C}$ <br> $\left(+70^{\circ} \mathrm{F}\right)$ Capacity |  |
| :---: | :---: | :---: |
| $+45.0^{\circ} \mathrm{C}$ | $\left(+113^{\circ} \mathrm{F}\right)$ | 93 |
| $+211^{\circ} \mathrm{C}$ | $\left(+70^{\circ} \mathrm{F}\right)$ | 100 |
| $+4.4^{\circ} \mathrm{C}$ | $\left(+40^{\circ} \mathrm{F}\right)$ | 93 |
| $-2.2^{\circ} \mathrm{C}$ | $\left(+28^{\circ} \mathrm{F}\right)$ | 88 |
| $-20.0^{\circ} \mathrm{C}$ | $\left(-44^{\circ} \mathrm{F}\right)$ | 60 |

## B-6 Retention of Charge

When a fully charged battery is allowed to stand idle it will gradually lose its charge. This loss is hastened considerably by high temperatures. The following table illustrates this.

| Storage | $+55^{\circ} \mathrm{C}\left(+131^{\circ} \mathrm{F}\right)$ | $+51.8^{\circ} \mathrm{C}$ <br> and $100 \%$ R.H. | $\left.+125^{\circ} \mathrm{F}\right)$ <br> Dry | $+45^{\circ} \mathrm{C}$ <br> $\left(+113^{\circ} \mathrm{F}\right)$ <br> Dry | $+21.1^{\circ} \mathrm{C}$ <br> $\left(+70^{\circ} \mathrm{F}\right)$ |
| :--- | :---: | :---: | :---: | :---: | :---: |

Cells which are allowed to stand idle are not harmed by the gradual self-discharge that occurs.

## B-2

## APPENDIX B. (Continued)

## B-7 Cell Reversal

There is a phenomenon which may occur during discharge of battery packs containing series-connected NiCd cells. This is known as "cell reversal" and it may seriously affect the performance of the battery.

Reverse charging of a cell can occur during the discharge of a series string without outward indication. Individual cells do not have identical capacities. The cell in a series string that has the least capacity will dissipate all of its energy before the other cells.

Consider the case of a 25 -volt battery consisting of 20 cells of 1.25 V each. The end of discharge would be 20.0 volts. We would normally assume any voltage between these two to be satisfactory. If one of the cells dissipates its energy and is down to 0 volts, it is possible that the other 19 cells will still have a total voltage of 22.8 volts, which would appear satisfactory.

However, this one cell will now be driven into reverse polarity and is being charged in a reverse direction. In the case of a 5 -cell, 6.25 volt battery, the loss of one cell is immediately apparent, since the battery voltage will drop to 4.8 volts, which is below the normal 5.0 volt endpoint. Thus, it can be seen that the greater the number of cells in a series string, the more difficult it becomes to distinguish a difference in performance due to the loss of the contribution voltage of a single cell.

Reverse charging of a cell, if driven far enough, could cause permanent damage. However, a certain amount of protection against reversal is built into the cell and short reversals do not seem to have any deleterious effect. The effect of cell reversal during discharge of a series string depends upon the number of times it occurs, as well as the number of cells in series and the length of time on reverse charge. Another problem is that once the cell loses some of its capacity the effect will snowball; the cell will go into reverse charge sooner with each battery chargedischarge cycle.

Generally the cells are fairly well balanced in production batteries, and deep cell reversal is uncommon. However, for further protection, there are several equipment operational steps that can be used to minimize the possibility of cell reversal and to correct the condition if it occurs.
a. Operate the instrument on ac power whenever practical, expecially when in use over extended periods of time.
b. When operating the instrument from the battery, check the condition of the battery periodically; more often when the battery is several hours into the discharge cycle.

## B-3

## APPENDIX B. (Continued)

c. Never operate the equipment on the battery when the battery voltage indicates below the operating range on the front panel meter.
d. Never forget to turn off the equipment when it is operating on the battery.
e. "Charge balancing" of the battery should be performed every month or every 15 charge/discharge cycles, whichever occurs first. Charge balancing is to deliberately charge the battery $50 \%$ longer than the normallyrecommended time for fully charging the battery. Overcharging the batteries for any length of time will not damage the battery cells.
f. When cell reversal is suspected (as indicated by an abnormally low battery test voltage for a known battery charge condition), perform battery charge balancing immediately. If this does not correct the condition, then one or more cells may be permanently damaged and the battery should be replaced.

## APPENDIX C.

## MAINTENANCE ALLOCATION

## SECTION I. INTRODUCTION

## C-1. General

This appendix provides a summary of the maintenance operations for the EMI FIELD INTENSITY METER NM-37/57. It authorizes categories of maintenance for specific maintenance functions on repairable items and components and the tools and equipment required to perform each function. This appendix may be used as an aid in planning maintenance operations.

## C-2. Maintenance Function

a. Inspect. To determine the serviceability of an item by comparing its physical, mechanical and/or electrical characteristics with established standards through examination.
b. Test. To verify serviceability and to detect incipient failure by measuring the mechanical or electrical characteristics of an item and comparing those characteristics with prescribed standards.
c. Service. Operations required periodically to keep an item in proper operating condition, i.e., to clean (decontaminate), to preserve, to drain, to paint, or to replenish fuel, lubricants, hydraulic fluids, or compressed air supplies.
d. Adjust. To maintain, within prescribed limits, by bringing into proper or exact position, or by setting the operating characteristics to the specific parameters.
e. Align. To adjust specified variable elements of an item to bring about optimum or desired performance.
f. Calibrate. To determine and cause corrections to be made or to be adjusted on instruments or test measuring and diagnostic equipments used in precision measurement. Consists of comparisons of two instruments, one of which is a certified standard of known accuracy, to detect and adjust any discrepancy in the accuracy of the instrument being compared.
g. Install. The act of emplacing, seating or fixing into position an item, part, module (component or assembly) in a manner to allow the proper functioning of the equipment or system.
h. Replace. The act of substituting a serviceable like type part, subassembly or module (component or assembly) for an unserviceable counterpart.
i. Repair. The application of maintenance services (inspect, test, service, adjust, align, calibrate, replace) or other maintenance actions (welding, grinding, riveting, straightening, facing, remachining or resurfacing) to restore serviceability to an item by correcting specific damage, fault, malfunction, or failure in part, subassembly, module (component or assembly), end item or system.
j. Overhaul. That maintenance effort (service/action) necessary to restore an item to a completely serviceable/operational condition as prescribed by maintenance standards (i.e., DMWR) in appropriate technical publications. Overhaul is normally the highest degree of maintenance performed by the Army. Overhaul does not normally return an item to like new condition.
k. Rebuild. Consists of those services/actions necessary for the restoration of unserviceable equipment to a like new condition in accordance with original manufacturing standards. Rebuild is the highest degree of materiel maintenance applied to Army equipment. The rebuild operation includes the act of returning to zero those age measurements (hours, miles, etc.) considered in classifying Army equipments/components.

## C-3. Column Entries

a. Column 1, Group Number. Column 1 lists group numbers, the purpose of which is to identify components, assemblies, subassemblies, and modules with the next higher assembly.
b. Column 2, Component/Assembly. Column 2 contains the noun names of components, assemblies, subassemblies and modules for which maintenance is authorized.
c. Column 3, Maintenance Functions. Column 3 lists the functions to be performed on the item listed in column 2. When items are listed without maintenance functions, it is solely for the purpose of having the group numbers in the MAC and RPSTL coincide.
d. Column 4, Maintenance Category. Column 4 specifies, by the listing of a work time figure in the appropriate subcolumn(s), the lowest level of maintenance authorized to perform the function listed in column 3. This figure represents the active time required to perform the maintenance function at the indicated category of maintenance. If the number or complexity of the tasks within the listed maintenance function vary at different maintenance categories, appropriate work time figures will be shown for each category. The number of task-hours specified by the work
time figure represents the average time required to restore an item (assembly, subassembly, component, module, end item or system to a serviceable condition under typical field operating conditions. This time includes preparation time, troubleshooting time, and quality assurance/quality control time in addition to the time required to perform the specific tasks identified for the maintenance functions authorized in the maintenance allocation chart. Subcolumns of column 4 are as follows:

C - Operator/Crew
O - Organizational
F - Direct Support
H - General Support
D - Depot
e. Column 5, Tools and Equipment. Column 5 specifies by code, those common tool sets (not individual tools) and special tools, test and support equipment required to perform the designated function.
f. Column 6, Remarks. Column 6 contains an alphabetic code which leads to the remark in section IV, Remarks, which is pertinent to the item opposite the particular code.

## C-4. Tools and Test Equipment Requirements (Section III)

a. Tool or Test Equipment Reference Code. The numbers in this column coincide with the numbers used in the tools and equipment column of the MAC. The numbers indicate the applicable tool or test equipment for the maintenance functions.
b. Maintenance Category. The codes in this column indicate the maintenance category allocated the tool or test equipment.
c. Nomenclature. This column lists the noun name and nomenclature of the tools and test equipment required to perform the maintenance functions.
d. National/NATO Stock Number. This column lists the National/NATO stock number of the specific tool or test equipment.
e. Tool Number. This column lists the manufacturer's part number of the tool followed by the Federal Supply code for manufacturer's (5-digit) in parenthese.

## C-5. Remarks (Section IV)

a. Reference Code. This code refers to the appropriate item in the Section II, Column 6.
b. Remarks. This column provides the required explanatory information necessary to clarify items appearing in section II.

## C-3 (C-4 blank)

## SECTION II. MAINTENANCE ALLOCATION CHART - Continued <br> FOR

ELECTROMAGNETIC INTERFERENCE/FIELD INTENSITY METER NM-37/57


## SECTION II. MAINTENANCE ALLOCATION CHART - Continued <br> FOR

ELECTROMAGNETIC INTERFERENCE/FIELD INTENSITY METER NM-37/57

| (1) Group number | (2) |  | (3) Maint. function | (4) <br> Maint. category |  |  |  | (5) <br> Tool/ equipmen | (6) <br> Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Component/assembly |  |  |  |  |  |  |  |  |
|  |  |  | C | 0 | H | D |  |  |
| 0012 | 16020.5 MHz IF Converter | (A12) |  | $\begin{aligned} & \text { Inspect } \\ & \text { Test } \\ & \text { Replace } \\ & \text { Repair } \end{aligned}$ |  | 0.5 | 0.8 <br> 0.3 <br> 0.8 |  | $\begin{array}{\|l\|l\|} \hline 19 \\ 19 \text { thru } 18 \\ 18 \text { trur } \\ 1800 \\ 18 \text { thur } 20 \end{array}$ |  |
| 0013 | 20.5 MHZ IF PREAMPLFIER | (A13) | $\begin{aligned} & \text { Inspect } \\ & \text { Thest } \\ & \text { Respace } \\ & \text { Repaif } \end{aligned}$ |  | 0.5 | 0.8 0.3 0.8 0.8 |  |  18 thru 20 |  |
| 0014 | BANDWIDTH SELECTOR | (A14) | $\begin{aligned} & \text { Inspect } \\ & \substack{\text { Teset } \\ \text { Replace } \\ \text { Renair }} \end{aligned}$ |  | 0.5 | 0.8 <br> 0.3 <br> 0.8 |  |  |  |
| 0015 | LINEARIfand bfo | (A15) | $\begin{aligned} & \text { Inspect } \\ & \text { T Test } \\ & \text { Replace } \\ & \text { Repair } \end{aligned}$ |  | 0.5 | 0.8 0.3 0.8 |  |  |  |
| 0016 | DCIIC Converter | (A16) | $\begin{aligned} & \text { Inspect } \\ & \begin{array}{c} \text { Testat } \\ \text { Reppee e } \\ \text { Repair } \end{array} \end{aligned}$ |  | 0.3 | 0.5 0.5 0.8 |  |  |  |
| 0017 | TWO POSITION RF SWLITCH | (A17) | $\begin{aligned} & \text { Inspect } \\ & \substack{\text { Testat } \\ \text { Replace } \\ \text { Repair }} \end{aligned}$ |  | 0.5 | 0.8 0.3 0.8 |  | $\begin{array}{\|l\|l\|} \hline 19 \\ 19 \text { thru } 18 \\ 18 \text { trun } \\ 18 \text { thru } \\ 180 \end{array}$ |  |
| 0018 | FM DISCRIIINator | (A18) | $\begin{aligned} & \text { Inspect } \\ & \text { T Test } \\ & \text { Replace } \\ & \text { Repair } \end{aligned}$ |  | 0.5 | 0.8 0.3 0.8 |  |  |  |
| 0019 | WEIGHTING CIRCUIT AND METER AMPLIFIER | (A21) | $\begin{aligned} & \text { Inspect } \\ & \text { Sester } \\ & \text { Repalace } \\ & \text { Repair } \end{aligned}$ |  | 0.5 | 0.8 0.5 0.8 |  |  |  |
| 0020 | direct peak circuit | (A22) | $\begin{aligned} & \text { Inspect } \\ & \begin{array}{l} \text { Test } \\ \text { Replace e } \\ \text { Repair } \end{array} \\ & \text { Ren } \end{aligned}$ |  | 0.5 | 0.8 0.5 0.8 |  |  |  |
| 0021 | SLIdeback peak circuit | (A23) | $\begin{gathered} \text { Inspect } \\ \substack{\text { Teptace } \\ \text { Replace } \\ \text { Repair }} \end{gathered}$ |  | 0.5 | 0.8 0.5 0.8 |  | $\begin{aligned} & 19 \\ & 1,2,4,9,17 \\ & 1 \begin{array}{l} 18,9720 \\ 188 \text { thru } 20 \end{array} \end{aligned}$ |  |
| 0022 | dB READOUT AND AUDIO AMPLIFIER | (A24) | $\begin{aligned} & \text { Inspect } \\ & \begin{array}{c} \text { Instat } \\ \text { Replace } \\ \text { Repair } \end{array} \\ & \hline \end{aligned}$ |  | 0.5 | 0.8 0.5 0.8 |  |  |  |
| 0023 | Remote function selector | ( (225) | $\begin{gathered} \text { Inspect } \\ \begin{array}{c} \text { Tent } \\ \text { Replace } \\ \text { Repair } \end{array} \\ \hline \end{gathered}$ |  | 0.5 | 0.8 0.5 0.8 |  |  |  |

## SECTION II. MAINTENANCE ALLOCATION CHART - Continued <br> FOR

ELECTROMAGNETIC INTERFERENCE/FIELD INTENSITY METER NM-37/57

| (1) <br> Group number | Component/assembly |  | (3) <br> Maint. function | (4) <br> category |  |  |  |  | (5) <br> Tool/ equipment | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | C | 0 | F | H | D |  |  |
| 0024 | SHAPER 1 | (A26) |  | Inspect <br> Test <br> Replace <br> Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.3 \\ & 0.5 \end{aligned}$ |  | 19 <br> 2, 14 <br> 18 thru 20 <br> 18 thru 20 |  |
| 0025 | SHAPER 2 | (A27) | Inspect Test Replace Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.3 \\ & 0.5 \end{aligned}$ |  | $\begin{aligned} & 19 \\ & 2,14 \\ & 18 \text { thru } 20 \\ & 18 \text { thru } 20 \end{aligned}$ |  |
| 0026 | TUNING CONTROL | (A29) | Inspect Test Replace Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.3 \\ & 0.5 \end{aligned}$ |  | 19 <br> 2, 14 <br> 18 thru 20 <br> 18 thru 20 |  |
| 0027 | BAND SELECTOR | (A30) | Inspect Test Replace Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.3 \\ & 0.5 \end{aligned}$ |  | 19 <br> 2, 14 <br> 18 thru 20 <br> 18 thru 20 |  |
| 0028 | VOLTAGE SELECTOR | (A31) | Inspect <br> Test <br> Replace <br> Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.5 \\ & 0.8 \end{aligned}$ |  | $\begin{aligned} & 19 \\ & 1,2,5,6 \\ & 18 \text { thru } 20 \\ & 18 \text { thru } 20 \end{aligned}$ |  |
| 0029 | RECTIFIER AND CHANGE REGULATOR | (А32) | Inspect <br> Test <br> Replace <br> Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.5 \\ & 0.8 \end{aligned}$ |  | $\begin{aligned} & 19 \\ & 1,2,5,6 \\ & 18 \text { thru } 20 \\ & 18 \text { thru } 20 \end{aligned}$ |  |
| 0030 | INTERNAL SWEEP | (A33) | Inspect <br> Test <br> Replace <br> Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.3 \\ & 0.5 \end{aligned}$ |  | 19 <br> 2, 14 <br> 18 thru 20 <br> 18 thru 20 |  |
| 0031 | FREQUENCY READOUT | (A34) | Inspect Test Replace Repair |  | 0.3 |  | $\begin{aligned} & 0.5 \\ & 0.3 \\ & 0.5 \end{aligned}$ |  | 19 <br> 2, 14 <br> 18 thru 20 <br> 18 thru 20 |  |
| 0032 | LOG IF AMPLIFIER | (A41) | Inspect <br> Test <br> Replace <br> Repair |  | 0.5 |  | $\begin{aligned} & 0.8 \\ & 0.3 \\ & 0.8 \end{aligned}$ |  | $19$ <br> 1 thru 18 <br> 18 thru 20 <br> 18 thru 20 |  |
| 0033 | POWER TRANSFORMER | (A42) | Inspect <br> Test <br> Replace <br> Repair |  | 0.5 |  | $\begin{aligned} & 0.8 \\ & 0.3 \\ & 0.8 \end{aligned}$ |  | $\begin{aligned} & 19 \\ & 1 \text { thru } 18 \\ & 18 \text { thru } 20 \\ & 18 \text { thru } 20 \end{aligned}$ |  |
| 0034 | BATTERY PACK | (A44) | Inspect Test Replace Repair |  | 0.5 |  | $\begin{aligned} & 0.8 \\ & 0.3 \\ & 0.8 \end{aligned}$ |  | $19$ <br> 1 thru 18 <br> 18 thru 20 <br> 18 thru 20 |  |
| 0035 | TURRET ATTENUATOR | (A45) | Inspect Test Replace Repair |  | 0.5 |  | 0.8 0.3 0.8 |  | $\begin{aligned} & 19 \\ & 1 \text { thru } 18 \\ & 18 \text { thru } 20 \\ & 18 \text { thru } 20 \end{aligned}$ |  |

## SECTION II. MAINTENANCE ALLOCATION CHART - Continued <br> FOR

ELECTROMAGNETIC INTERFERENCE/FIELD INTENSITY METER NM-37/57


SECTION III . TOOL AND TEST EQUIPMENT REQUIREMENTS FOR
ELECTROMAGNETIC INTERFERENCE/FIELD INTENSITY METER NM-37/57

| $\begin{gathered} \hline \text { TOOL OR TEST } \\ \text { EQUIPMENT } \\ \text { REF CODE } \\ \hline \end{gathered}$ | MAINTENANCE CATEGORY | NOMENCLATURE | NATIONAL/NATO STOCK NUMBER | TOOL NUMBER |
| :---: | :---: | :---: | :---: | :---: |
| 1 | H, D | OSCILLOSCOPE (TEK 5440) | 6625-01-034-3269 |  |
| 2 | H, D | DC DIGITAL VOLTMETER (HP 3490A/W) | 6625-01-010-9255 |  |
| 3 | H, D | RF MILLIVOLTMETER (HP 410C) AN/LSM- 77 AN/USM-77 | 6625-00-969-4105 |  |
| 4 | H, D | 10 dB ATTENUATOR (HP 355C) | 6625-00-866-9462 |  |
| 5 | H, D | AC VOLTMETER (HP 3490A) | 6625-01-01C-9255 |  |
| 6 | H, D | CLIP-ON MILLIAMMETER (HP 428B) ME-488/U | 6625-00-816-9324 |  |
| 7 | H, D | FREQUENCY COUNTER (HP 5345A) | 6625-00-531-4752 |  |
| 8 | H, D | SIGNAL GENERATOR (HP 612A) AN/URM-56) SG-340A/G | 6625-00-542-1292 |  |
| 9 | H, D | SIGNAL GENERATOR (HP 608E) AN/USM-44B | 6625-00-176-5708 |  |
| 10 | H, D | CAPACITANCE BRIDGE ZM-74/U HP-4800A | 6625-00-167-9861 |  |
| 11 | H, D | SWEEP GENERATOR (WAVETEK MODEL 2001) | 4931-00-165-3954 |  |
| 12 | H, D | AUDIO GENERATOR HP 200CD | 6625-00-518-4659 |  |
| 13 | H, D | SWEEP GENERATOR (TELONIC SM 2000) WITH OSCILLATOR 3006 | 6625-00-828-7135 |  |
| 14 | H, D | OHMMETER, TRIPLETT 630 | 6625-00-578-5849 |  |
| 15 | H, D | BAND PASS FILTER (KRUHN-HITE) | 5915-00-499-6676 |  |
| 16 | H, D | IMPULSE GENERATOR (SINGER IG 115) | 6625-00-937-6123 |  |
| 17 | H, D | VTM (HP 28480) | 6625-00-802-7350 |  |
| 18 | D | ELECTROMAGNETIC INTERFERENCE/FIELD INTENSITY METER NM-37/57 | 6625-00-161-4176 |  |
| 19 | H, D | TOOL KIT 101/G | 5180-00-064-5178 |  |
| 20 | 0 | COMMON TOOLS NECESSARY TO THE PERFORMANCE OF THE MAINTENANCE FUNCTION ARE AVAILABLE TO MAINTENANCE PERSONNEL FOR THE MAINTENANCE CATEGORY LISTED. |  |  |

C-9 (C-10 blank)

By Order of the Secretaries of the Army and the Air Force:

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Figure 5-1. Tuner 1 (A1), Schematic Diagram 4-501131-001 (D)


NOTES: UNLESS OTHERWISE SPECIFIED

1. ALL RESISTORS ARE IN OHMS $\pm 5 \%$, \% WAT
2. ALL FEEDTHRU CAPACITORS ARE . OOO 3 MFD $\pm 20 \%$
3. COMPONENTS MARED
4. ALL REONHRU CAPACITORS ARE. 003 MFD $\pm 20 \%$.



NOTES: UNLESS OTHERWISE SPECIFIED

1. ALL RES ISTORS ARE IN OHMS $\pm 5 \%, 1 / 4$ WATT.
2. ALL FEEDTHRU CAPACITORS ARE .003 MFD $\pm 20 \%$.
3.COMPONENTS MARKED WITH * MAY BE CHANGEDAT TEST.

| HIGHEST REF DESIGNATIONS USED |
| :--- |
| Q3 J3\|C26 [L3 T5| R24 CR9 |
| REF DESIGNATIONS NOT USED |
| C1 C21 C22 |



Figure 5-4. Tuner 4 (A4) Schematic Diagram
4-501134-001 (c)


Figure 5-5. Tuner 5 (A5) Schematic Diagram 4-501135-011 (C)



Figure 5-7. Tuner 7 (A7),
Schematic Diagram
4-501137-001 (C)


Figure 5-8. Tuner 8 (A8), 5-10
Schematic Diagram
4-501138-001 (B)


Figure 5-9. Impulse Calibrator (A9),
Schematic Diagram
4-501139-001 (C)


Figure 5-10. 8-Position RF Switch (A10),
Schematic Diagram
3-501199-001


Figure 5-11. 5-Position and 3-Position IF Switch (A11), Schematic Diagram

4-501140-001


Figure 5-12. 160/20.5 MHz IF Converter,
(A12), Schematic Diagram
4-501141-001 (D)

 ALL Capacitions ape in ictora Reot $\pm 5 \%$.


SERIAL NUMBER NOTES:

1. ADO C 4718 BETWEEN JUNCTION OF 2. CHANE Cli47 TO C1 39.



5 ALL RELAYS ARE SPDT RA 30141121


##  <br> 

Figure 5-13. 20.5 MHz IF Preamplifier
(A13), Schematic Diagram
4-501130-001 (B)


Figure 5-14. Bandwidth selector (A14),
Schematic Diagram
4-501142-001 (D)


NOTES: UNLESS OTHERWISE SPECIFIED 1. ALL RESITORS ARE IN OHMS $\pm 5 \%$, \% W .
serial number notes:
476AND ABOVE

1. CHANGE CR-1 FROM IN277 TO 2900


Figure 5-15. Linear IF Amplifier and


Figure 5-16. $D C / D C$ Converter (A16),


Figure 5-17. 2-Position RF Switch (A17), Schematic Diagram 3-501198-001 (A)


Figure 5-18. FM Discriminator (A18), Schematic Diagram4-501144-001 (C)

(3) to be matched pair per 1.403547-001 4 ALL DIODES ARE hP-2800.
3 ARI, AR2, AR 3. ARE FAIRCHILD Ya74IC.
2 All CPACITORS ARE $\pm 10 \%$, 250voc.
1 al resistors are in Ohms, $\pm 5 \%, 1 / 4$ watt.

notes uncss otwermer spearikd


Figure 5-20. Direct Peak Circuit (A22), Schematic Diagram 4-501145-001 (F)


Fighest ref desiciantions used

bef designations not used
R14



Figure 5-21. Slideback Peak Circuit(A23), Schematic Diagram 4-501146-001 (C)
meter amp (3)

5. ALL RESISTORS MARKED WITH *:0.18, $1 / 4 \mathrm{WW}: 10 \mathrm{PPM} / \mathrm{O}$ TC
all other resistors: $5 \times .1 / 4 \mathrm{~W}$

- ALL INTEGRATED CIRCUITS: 741 C
- all diodes marked with *:
all other diodes: in4i48
- all relays: electrol ra30131121 or eouivalent
. Partial ref designations are shown.
or complete designation prefix
with unit no. or subassembly designation (s
NOTES: UNLESS OTHERWISE SPECIFIED
Figure 5-22. DB Readout and Audio Amplifier (A24), Schematic Diagram 2-501384-001

[2] U1 REFERS TO NM $17 / 27$
Figure 5-23. Remote Function Selector (A25), Schematic Diagram 4-501148-001 (B)


NOTES: UNLESS OTHERWISE SPECLIFED

2. ALL RESGRTESE CIRE INTS ARE FARCH


Figure 5-24. Shaper 1 (A26) Schematic Diagram 4-501149-001 (B)


Figure 5-25. Shaper 2 (A27), Schematic Diagram 4-501150-001 (A)


Figure 5-26. Tuning Control (A29), Schematic Diagram 4-501151-001 (A)


Figure 5-27. Band Selector (A30), Schematic Diagram 4-501152-001 (A)


NOTES: UNLESS OTHERWISE SPECIIFIED
(1) FOR MODEL NM-37/57 JUMPER POINT B TO POINT C \& AND E TO
POINT ETO POINT FONLY

FOR MODEL NM- $7 / 57$ \& JUMPER,POINT A TO POINT C \& POINT D TO
POINT FONLY FOR MODEL NM-
POINT FONLY.

| Highest ref designations used |  |  |
| :---: | :---: | :---: |
| CR15 K8 | F |  |
| REF DESIGNATIONS NOT USED |  |  |

NOTES: UNLESS OTHERWISE SPECIFIED

1. ALL CAPACITORS ARE IN MICROFARADS $\pm 20 \%$. 2. ALL RESISTORS ARE IN OHMS, $\pm 1 \%$, $1 / \mathrm{WW}$.
2. INTEGRATED CIRCUITS AR1 $\&$ AR2 ARE BEL HOWEL $20-007 C$.

| Highest ref designations used |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| AR2 | C8 | CR3 | O8 | R20 |
| REF DESIGNATIONS NOT USED |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  | R10 |



Figure 5-28. Voltage Regulator (A31), Schematic Diagram 4-501124-001 (B)


Figure 5-29. Rectifier - Charge Regulator (A32), Schematic Diagram 4-501125-001


Figure 5-30. Internal Sweep (A33), Schematic Diagram 4-501126-001 (C)


Figure 5-31. Frequency Readout (A34), Schematic Diagram 4-501153-001


Figure 5-32. Log IF Amplifier (A41) Schematic Diagram 4-50120-001 (A)


Figure 5-33. Voltage Controlled IF Attenuator (A48), Schematic Diagram 4-501156-001 (A)



Figure 5-35. WIRING DIAGRAM, NM-37/57, 9-501206-001 (K) (SHT. 1 OF 2)


FIGURE 5-35. WIRING DIAGRAM,NM-37/57 9-501206-001 (K) (SHT. 2 OF 2)



[^0]:    *Serial \#339 and above

[^1]:    ** SERIAL \#476 AND ABOVE
    *** SERIAL \#526 AND ABOVE

[^2]:    * SERIAL \#455 AND ABOVE
    ** SERIAL \#526 AND ABOVE

